

Prevention of Significant Deterioration (PSD) Air Permit Application for Plant OX Modernization/Debottleneck Project

BP Amoco Chemical Company – Cooper River Plant Wando, South Carolina

April 2013, Revised March 2014

Non-confidential



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TRC Environmental Corporation | BP Amoco Chemical Company - Cooper River Plant PSD Air Permit Application
OX Modernization/Debottleneck Project

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Background 1.1

BP Amoco Chemical Company - Cooper River Plant (BP CR) currently owns and operates a chemical manufacturing facility in Wando, South Carolina that produces purified terephthalic acid (PTA). The BP CR plant, wholly owned and operated by BP, is located on a 6,000-acre site in Berkeley County, South Carolina on the east bank of the Cooper River, about 16 miles upstream of the Atlantic Ocean. The facility location is as follows:

BP Amoco Chemical Company - Cooper River Plant 1306 Amoco Drive Wando, South Carolina 29492

The BP CR Plant falls under the Standard Industrial Classification (SIC) Code 2869. The product PTA is a white, inert powder used to make polyester fibers, bottles, and films. The major raw materials in the production of PTA are paraxylene (PX), acetic acid (HAC), and hydrogen. Plant operation consists of the following five major processes:

- Oxidation (OX) units for production of crude terephthalic acid (TA)
- 2. PTA units for purification of crude TA into PTA
- 3. Product loading/shipping
- 4. **Utilities**
- 5. Wastewater treatment.

Crude TA is produced in the OX units by the air oxidation of PX in an HAC solution and the presence of a catalyst at high temperature and pressure. The crude TA is crystallized and separated from the mother liquor and dried. Catalyst and mother liquor recycle are routinely operated at very high rates as a result of waste minimization and economic initiatives at the plant.

Crude TA is purified in the PTA units in an aqueous solution by hydrogenation in the presence of a catalyst. The purified product is crystallized, separated, dried, and shipped. Reject product from the silo baghouse, or loading shaker screens is routinely rerun, as an alternative to sending it to the wastewater treatment unit. TA solids in the wastewater treatment plant (WWTP) influent are settled out, recovered, and can be sold as a product, BACA (byproduct aromatic carboxylic acid).

1.2 Purpose and Scope

BP CR has retained TRC Environmental Corporation (TRC) to assist in the preparation of an air construction permit application package for the proposed revisions at the BP CR facility. BP CR is currently a Title V source and a major source for both hazardous air pollutants (HAPs) and Prevention of Significant Deterioration (PSD). BP CR is proposing revisions to the #1 OX and #2 OX units to debottleneck these units so they are able to operate at their design production on a consistent basis. Minor revisions to the #1 and #2 PTA are also proposed that will not impact their capacity but will reduce their production costs. This project will be a phased construction with the initial work on the #1 OX and PTA units beginning in late 2014 and the revised units expected to start-up in mid to late 2016. The work on the #2 OX and PTA units is expected to begin in early 2017 and the revised units startup to occur by early 2019.

This project will result in an actual annual hourly (TA and PTA) production rate closer to the unit design rate. This project will not result in any increase in the maximum hourly emissions, the maximum hourly production rate, the maximum annual potential emission rates, or the maximum annual potential production rates above those used in previous permit applications. The project will modify the cooling tower systems to provide additional cooling capacity. This project will not revise any of the other auxiliary facilities but will require slightly more boiler steam, increase PX flow through the Tank Farm, and increase the PTA production into the product silos and loading that can all be provided without any changes to these systems. The project is referred to as the OX Modernization/Debottleneck Project.

These revisions will be completed over the next 5 years as unit shutdowns allow the tie-ins to be completed.

A PSD applicability analysis has been performed for the project recognizing that the area is in attainment for all pollutants. The PSD applicability analysis for this project recognizes the impact of the revisions on both OX and PTA units and the additional steam production, wastewater treatment, and shipping volumes necessary to accommodate these changes. The project PSD applicability analysis demonstrates that a significant net emissions increase will occur for carbon monoxide (CO) and volatile organic compounds (VOCs); therefore the project is subject to review under the PSD permitting program for those pollutants. Other pollutants were evaluated and determined to have increases that are projected to be less than PSD significance thresholds so they will only be subject to the normal air construction permitting. The Federal Land Manager (FLM) responsible for the Romaine Wilderness area, which is a federal Class 1 Wilderness about 30 miles from the site, was contacted to determine the FLM's interest in the PSD application. After providing the FLM with the emissions impacts from the project, the FLM replied by email (see Appendix F) that they were not requesting that a Class I Air Quality Related Value (AQRV) analysis be included in the PSD permit application. BP CR is required to file a permit application

with South Carolina Department of Health and Environmental Control (SC DHEC) to obtain approval to commence construction on the project via the issuance of an air construction permit. To satisfy this requirement, this permit application has been prepared in accordance with SC DHEC guidelines for air construction permitting including the required PSD permitting elements for CO and VOC. This application contains the following items:

n	Section 1	Introduction
n	Section 2	Project Description
n	Section 3	Regulatory Assessment
n	Section 4	Best Available Control Technology Analysis for Volatile Organic Compound Emissions and Carbon Monoxide
n	Section 5	Air Quality Analysis
n	Section 6	Additional Impacts Analysis
n	Appendix A	SC DHEC Permit Application Forms
n	Appendix B	Emissions Data and Calculations
n	Appendix C	RBLC Search Results
n	Appendix D	BACT Analysis Cost Information

1.3 Facility Location and Contact

All correspondence regarding this permit application should be sent to:

Mr. Brent Pace, P.E.
Environmental Engineer
BP Cooper River Plant
1306 Amoco Drive
Wando, SC 29492
Brent.Pace@bp.com
843.881.5182

and

Mr. Michael Doerner TRC Environmental Corporation 30 Patewood Drive, Suite 300 Greenville, SC 29615 mdoerner@trcsolutions.com 864.234.9481

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Existing Process Description 2.1

The BP CR processes consist of the two OX units, the two PTA units, and the shipping and loading area. The OX areas are where the process actually begins producing TA. In the PTA units, the TA is purified to produce PTA and sent to shipping and loading where it is stored in one of several silos and loaded into shipping containers. A simplified flow of the overall process is shown in Figure 2-1.1. Simplified process diagrams of the existing processes are shown in Figure 2-1.2 through Figure 2-1.5.

In the OX unit, a BP proprietary process is used for the catalytic liquid phase air oxidation of PX to produce TA. HAC, PX, and catalyst solution are mixed in a feed mix drum. The feed mix from the drum and air from the process air compressor are continuously fed to the reactors. Exothermic heat of reaction is removed by condensing the boiling reaction solvent. A portion of this condensate is withdrawn to control the water concentration in the reactor and the remainder is refluxed back to the reactor.

Reactor effluent is depressurized and cooled to filtering conditions in a series of crystallizers to form the solid TA crystals. Air is fed to the first crystallizer for additional reaction. The crystallizer temperatures are controlled by allowing a portion of the reaction solvent to flash off. The crystallizer vent streams are sent to the dehydration tower (DHT) or the High Pressure Absorber (HPA) for recovery of valuable materials. The DHT also removes water formed in the reaction. The crystallizer precipitate TA is recovered by filtration and finally dried. The dried TA solids are conveyed to the OX intermediate storage silos (TA) silos and stored for additional processing in the PTA unit.

The off-gas from the OX reactors is combined with the DHT overhead gases that have been compressed in the low pressure vent gas treatment (LPVGT) equipment. The combined gases pass through a recovery device, the HPA, before being sent to a control device, the high pressure vent gas treatment system (HPVGTS) in which CO, VOC, and HAP are nearly totally destroyed and then the gas is emitted to the atmosphere. The HPVGTS reactor contains catalyst bricks that are routinely changed out based on their activity and mechanical condition. Further processing in the OX unit is required to recover and purify HAC from the reactor outlet, crystallizer solvent withdrawal streams, and also from the un-recycled mother liquor stream. OX byproducts are separated from the HAC in a *confidential* evaporation process and then purged.

The PTA unit is also a continuous operation. Crude TA is fed from the OX intermediate storage silos to the feed slurry drum to produce the slurry of TA crystals and water. The slurry is heated to dissolve the TA and then the slurry enters the hydrogenation reactor where it reacts to convert the impurities into a form that can be separated from the product. The PTA reactor catalyst is routinely changed out based on its activity and mechanical condition. After reaction, the solution goes through a cycle of lowering the pressure and cooling to crystallize the PTA. A portion of the aromatic acids in the mother liquor are recovered by cooling and filtering the mother liquor; the aromatic acids are recycled back to the OX reaction unit.

The crystallized PTA is recovered from the mother liquor by separation in the filtration section of the unit. The final product is dried and transferred to the PTA day silos and then to the PTA product storage silos.

The #1 and #2 Cooling Towers supply non-contact cooling water to the respective #1 OX/PTA and #2 OX/PTA units. The Cooling Tower particulate matter (PM) emissions are Title V insignificant activities.

2.2 **Project Description**

The BP CR Modernization/Debottleneck project will be revising the OX and PTA units to remove limitations that prevent the OX units from operating at their unit design rates and reduce the OX and PTA unit operating costs. These revisions will include improvements to the reaction environment, additional air capacity, optimization of the recovery systems, improved DHT operation, improved energy recovery, removal of several emission points, dense phase conveying and additional cooling tower capacity. Simplified process diagrams of the future processes are shown in Figures 2-2.1 to 2-2.4.

The changes to the existing OX unit process description include the following items:

- PX would bypass the feed mix drum and be sent directly to the reactor.
- The first crystallizer vent stream for both units will only be sent to the HPA for recovery of valuable materials.
- The LPVGT will be removed so the DHT overhead vent stream will be routed to the Low Pressure Absorber (LPA) before being exhausted
- The DHT operation will be converted to an azeotropic distillation process and an additional tower will be added to recover the azeotropic chemical
- The two-stage evaporation process to remove byproducts and the catalyst recovery process will be removed

BP CR proposes to complete the unit revisions over the next 5 years as unit shutdowns allow the tie-ins to be completed and the equipment to be installed.

The major equipment revisions included in the proposed project are the following items on the units:

#1 OX unit 1.

- Replacement of four reactors (BR-301 A-D) with a single more efficient reactor (BR-301)
- Replacement of reactor overhead condenser system
- Replacing the air compressor rotor to reduce energy consumption
- Direct PX injection to reactor
- Additional reactor overhead recovery capacity by replacing equipment with an improved design
- Route 1st crystallizer (BD-401) vent to reactor off-gas recovery system
- Maintain power recovery in off-gas expander by lowering upstream pressure drop
- Azeotropic distillation on DHT (azeotropic distillation refers to the technique of adding another component to generate a new, lower-boiling azeotrope that is heterogeneous [e.g., producing two, immiscible liquid phases].)
- Revised DHT overhead recovery system to a two-stage system by:
 - § Routing existing DHT Scrubber (BT-702) vent to LPA (BT-603)
 - § Revise LPA packing
 - Convert DHT Scrubber to a one-stage acid scrubber
- Revised HPA (T-401) internals
- Dense phase conveying by changing system piping and rotary locks to allow conveying solids with less carrier gas
- Additional filtration capacity
- Removal of the LPVGT compressor (BC-710)
- Removal of the solvent stripper (BT-605)
- Removal of the residue evaporator (BM-606) and catalyst recovery unit (BD-625/631/632/BE-645)
- Removal of PX Stripper (BT-740)
- Addition of a steam turbine to generate power from excess low pressure steam

2. #1 PTA unit

- Revisions to crystallizer vent scrubber (CM-301) to improve energy recovery
- Addition of 5th crystallizer (CD-30x)
- Dense phase conveying by changing system piping and rotary locks to allow conveying solids with less carrier gas

3. #2 OX unit

- Direct PX injection to reactor
- Rerating the process air compressors for additional capacity
- Replacement of reactor overhead condenser
- Azeotropic distillation on DHT (*azeotropic distillation* refers to the technique of adding another component to generate a new, lower-boiling azeotrope that is heterogeneous [*e.g.*, producing two, immiscible liquid phases].)
- Modified packing or trays in DHT (DT-403), HPA (DT-111), LPA (DT-302), Dryer
 Scrubber (DT-301) and HPVGTS Scrubber (DT-1821).
- Routing DHT vent to revised LPA system
- Dense phase conveying by changing system piping and rotary locks to allow conveying solids with less carrier gas
- Removal of the LPVGT compressor (DC-304)
- Removal of a portion of the solvent stripper (DT-402) system
- Removal of the residue evaporator (DM-403) and catalyst recovery unit (DD-412/413/414/DE-416)
- Removal of PX Stripper (DT-404)
- Addition of a steam turbine to generate power from excess steam

4. #2 PTA Unit

- Revisions to crystallizer vent scrubber (DM-601) to improve energy recovery
- Revision of piping system from PTA Feed Drum (DD-500) to the Sundyne pumps.
- Addition of a 4th Sundyne pump
- Dense phase conveying
- Replacement of dryer (DM-703)
- Dense phase conveying by changing system piping and rotary locks to allow conveying solids with less carrier gas

Cooling Towers

- Additional #1 Cooling Tower capacity
- Additional #2 Cooling Tower capacity

The project will also include smaller items that will occur on all the units in the following general categories:

- Additional and/or improved automation, multivariable control schemes, and on-line analyzers to increase unit reliability and improve process control.
- Replacement of process equipment and piping that are negatively impacting maintenance costs and unit reliability.
- Replacement of obsolete or end-of-life equipment.
- Replacement of exchangers and vessels to improve metallurgy, reduce corrosion, and reduce maintenance costs.

2.3 **Unit Emissions**

Emissions calculations for the units and a summary of the facility-wide emissions are included in Appendix B (Tables B-1 through B-11) of this application to determine PSD applicability. A summary of the PSD analysis in Appendix B is shown in Table 2.3.1 indicating that the only pollutants with increases above the baseline actual emissions greater than the PSD significance thresholds are CO and VOC. The unit's potential-to-emit (PTE) emissions are based on 8,760 hours per year of operation at their design capacities. The emissions include the impact of the incremental boiler steam production emissions, and the increased tank farm and shipping and loading emissions due to additional PTA production. The boilers have excess capacity available within their previously permitted limits and can provide the steam without making any revisions to the boilers. Both the Tank Farm and the Shipping and Loading areas have the capacity available to handle the increased flows without requiring any modifications. The addition of the azeotropic distillation to the OX units will add new pollutants (n-butyl acetate and butanol) to the emissions from the units.

The emissions calculations in Appendix B provide the various emissions estimates requested in the applications forms. The PSD emission calculations for the modified units (#1 OX, #2 OX, #1 PTA, #2 PTA, and Cooling Towers) are based on Post Project PTE – Baseline Average Emissions (BAE). The PSD emission calculations for the unmodified but debottlenecked units (Tank Farm and Shipping) are based on PTE-BAE. The PSD emission calculations for the incremental boiler steam are based on the emissions from producing the additional steam required by the project. The pre- and post-emissions are calculated for both the controlled and uncontrolled scenarios. The uncontrolled emissions estimates assume 0 percent recovery/

removal for the control devices. The emissions calculations are included in Appendix B in the following tables as shown in Table 2.3.2.

Table 2.3.1 Prevention of Significant Deterioration Analysis Summary

Step 1

POLLUTANTS	TOTAL PTE (before BACT)	TOTAL TWO-YEAR BASELINE AVERAGE	DELTA	PSD SIGNIFICANCE	ABOVE PSD
NO _X	30.7	3.1	27.6	40	No
VOC	402.8	319.9	82.9	40	Yes
CO	771.9	346.7	425.2	100	Yes
SO ₂	0.3	0.04	0.3	40	No
PM	40.7	33.7	7.0	25	No
PM ₁₀	39.6	33.0	6.7	15	No
PM _{2.5}	36.9	31.1	5.8	10	No
CO ₂ e	87,098	69,793	17,304	75,000	No

Contemporaneous Emissions

PROJECT	YEAR	CO (tpy)	VOC (tpy)
502b10 - CR #1 OX BR-301A Alternate Water Withdrawal	2008	0.0	0
PTA FIP Project (Permit CS)	2008	0.01	8.24
502b10 - #1 OX/PTA Op Flex	2011	0	0
PTA BHS Filter Project	2012	26.9	27.6
Total		26.9	35.8

Step 2 - Facility Netting

POLLUTANTS	voc	СО	NO _X	SO ₂	PM	PM ₁₀	PM _{2.5}	CO₂e
Step 1 Delta	82.9	425.2	27.6	0.3	7.0	6.7	5.8	17304.2
Total Contemporaneous	35.8	26.9	N/A	N/A	N/A	N/A	N/A	N/A
Net Emissions	118.8	452.1	27.6	0.3	7.0	6.7	5.8	17304.2
PSD Significance	40	100	40	40	25	15	10	75,000
Above PSD	Yes	Yes	No	No	No	No	No	No

Table 2.3.2 Appendix B Tables

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31	Cooling Tower Sample Calculations

2.4 Prevention of Significant Deterioration Emission Limits

As a result of this application and the Best Available Control Technology (BACT) analysis included for VOC and CO emissions, the following existing PSD avoidance limits shown in Table 2.4.1 are requested to be removed and replaced by the applicable BACT/PSD limits shown in the table. The PSD analysis has included the emission impacts of the removal of these PSD avoidance limits on the resulting PTE emissions.

Table 2.4.1 Emission Limit Revisions

EMISSION POINT	POLLUTANT	PREVIOUS PSD AVOIDANCE LIMITS ⁽¹⁾	REQUESTED BACT/PSD LIMITS (tpy)	SHORT-TERM BACT/PSD LIMITS (lbs/hr)
#1 OX LPA	VOC	80 tpy and 40 lb/hr	42.0	12
#1 OX LPA	СО	40 tpy	18.0	5
#1 DUT Corubbor	VOC	165 tpy and 60 lb/hr	N/A – no longer vents	
#1 DHT Scrubber	СО	380 tpy	atmos	sphere

Table 2.4.1 Emission Limit Revisions

EMISSION POINT	POLLUTANT	PREVIOUS PSD AVOIDANCE LIMITS ⁽¹⁾	REQUESTED BACT/PSD LIMITS (tpy)	SHORT-TERM BACT/PSD LIMITS (lbs/hr)	
	VOC	80 tpy and 85 lb/hr	20.5	6	
#1 HPVGTS	СО	375 tpy and 1,452 lb/hr	385.0	106	
#1 PTA Crystallizer Vent Scrubber	VOC	None	46.5	13	
#2 LPA	VOC		38.8	11	
#2 OX HPVGTS		215.9 tpy and	15.3	5	
#2 PTA Crystallizer Vent Scrubber		49.3 lb/hr	46.5	13	
#2 LPA	00	CO None	None	15.2	5
#2 OX HPVGTS		None	329.0	90	
Combined total for #1 OX and #2 OX, #1 PTA and #2 PTA	VOC	1,825 tpy	Replaced by individual vent limits		

⁽¹⁾ All these previous PSD avoidance limits are requested to be removed

BP will continue to abide by all of the other synthetic minor (PSD avoidance) limits in the existing Title V permit as they presently exist. This includes all limits for PM, particulate matter (nominally 10 microns or less) (PM_{10}), nitrogen oxides (NO_X), and sulfur dioxide (SO_2) in the existing Title V permit. Table 2.4.2 shows those synthetic minor limits that will remain unchanged and to which CR BP will continue to abide.

Table 2.4.2 Unchanged Synthetic Minor Emission Limits

EMISSION POINT	POLLUTANT	PSD AVOIDANCE LIMITS	
#1 OX Silo Scrubber	PM ₁₀	2.16 lb/hr	
Silos CF-701 A-E	PM ₁₀	1.08 lb/hr (each)	
Silo CF-701 F	PM ₁₀	0.48 lb/hr	
	PM/PM ₁₀	50.9 tpy combined	
Boilers AB-350 A/B	SO ₂	733.4 tpy combined	
DUIIGIS AD-300 A/D	NO _X	317.0 tpy combined	
	СО	299.6 tpy combined	

2.5 Best Available Control Technology Monitoring

Table 2.5.1 is a summary of the proposed monitoring parameters from the BACT analysis contained in Section 4 of this application. The operational ranges for the proposed monitoring parameters will be submitted to SC DHEC along with supporting documentation within 180 days of completing the project construction. The operational range of the parameters will be determined based on operational and stack test data, vendor recommendations, equipment design properties, as visual inspections as appropriate for a parameter.

Table 2.5.1 BACT Monitoring Parameters

UNIT	EMISSION POINT	POLLUTANT	PARAMETER 1 MONITORED	PARAMETER 2 MONITORED
	LPA	VOC	Scrubbing Liquid Fluid Flow	Scrubber Top Temperature
#1 OX	HPVGTS	VOC	Reactor Inlet Temperature	Reactor Outlet Temperature
	Equipment Fugitives	VOC	HON LDAR Monitoring program	N/A
	LPA	VOC	Scrubbing Liquid Fluid Flow	Scrubber Top Temperature
#2 OX	HPVGTS	VOC	Reactor Inlet Temperature	Reactor Outlet Temperature
	Equipment Fugitives	VOC	HON LDAR Monitoring program	N/A
#1 PTA	Crystallizer Vent Scrubber	VOC	Specialized Performance Test every 5 years	N/A
#2 PTA	Crystallizer Vent Scrubber	VOC	Specialized Performance Test every 5 years	N/A
#1 OX	LPA	СО	None	N/A
	HPVGTS	СО	Reactor Inlet Temperature	Reactor Outlet Temperature
#2 OX	LPA	СО	None	N/A
	HPVGTS	СО	Reactor Inlet Temperature	Reactor Outlet Temperature

Table 2.5.2 indicates the monitoring and reporting frequency for the BACT monitoring parameters. For parameters that have a monitoring frequency specified as "continuously with daily average," at least one data point shall be obtained each 15-minute period and all data points collected within a 24-hour period (during those times that the process or emissions generating equipment was being operated) shall be averaged together for a daily reading for comparison to an established monitoring range. All records of the parameters will maintained for at least 5 years after being recorded.

Table 2.5.2 BACT Monitoring Frequency and Reporting

UNIT	EMISSION POINT	PARAMETER	FREQUENCY	REPORTING
#1 OX	LPA	Scrubbing Liquid Flow	Continuously with daily average	Semiannual
		Scrubber Top Temperature	Continuously with daily average	Semiannual
	HPVGTS	Reactor Inlet Temperature	Continuously with daily average	Semiannual
		Reactor Inlet Temperature	Continuously with daily average	Semiannual
	Equipment Fugitives	HON LDAR Monitoring	Per HON LDAR regulation	Semiannual
#2 OX	LPA	Scrubbing Liquid Flow	Continuously with daily average	Semiannual
		Scrubber Top Temperature	Continuously with daily average	Semiannual
	HPVGTS	Reactor Inlet Temperature	Continuously with daily average	Semiannual
		Reactor Inlet Temperature	Continuously with daily average	Semiannual
	Equipment Fugitives	HON LDAR Monitoring	Per HON LDAR regulation	Semiannual
#1 PTA	Crystallizer Vent Scrubber	Special Performance Test	Every 5 years	Every 5 years
#2 PTA	Crystallizer Vent Scrubber	Special Performance Test	Every 5 years	Every 5 years

Figure 2-1.1
BP Cooper River Overall Process Flow Diagram

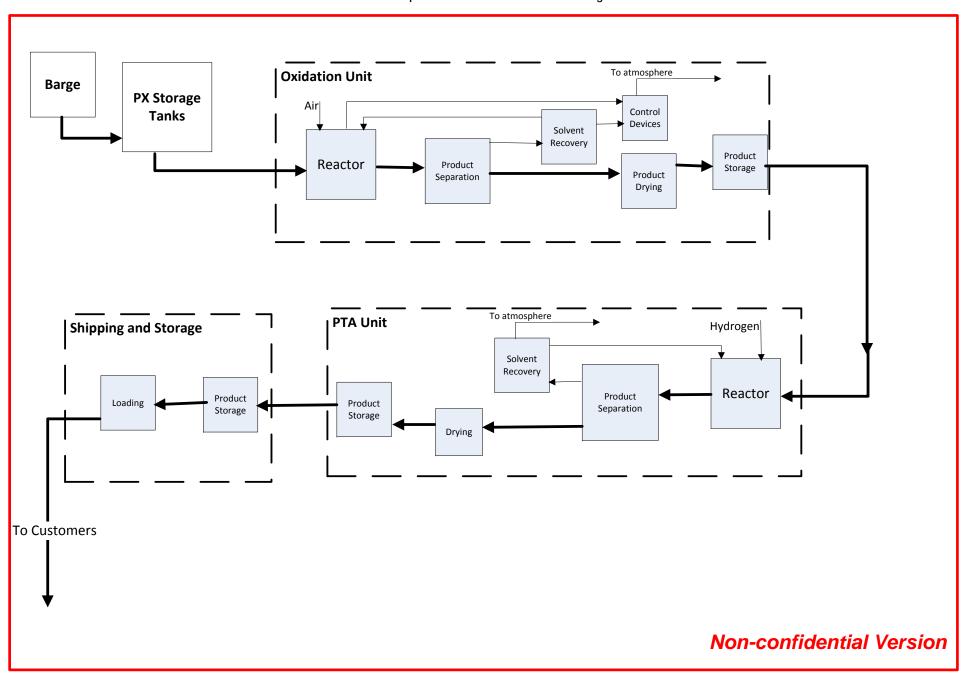


Figure 2-1.2 #1 OX Unit Existing Process Flow Diagram

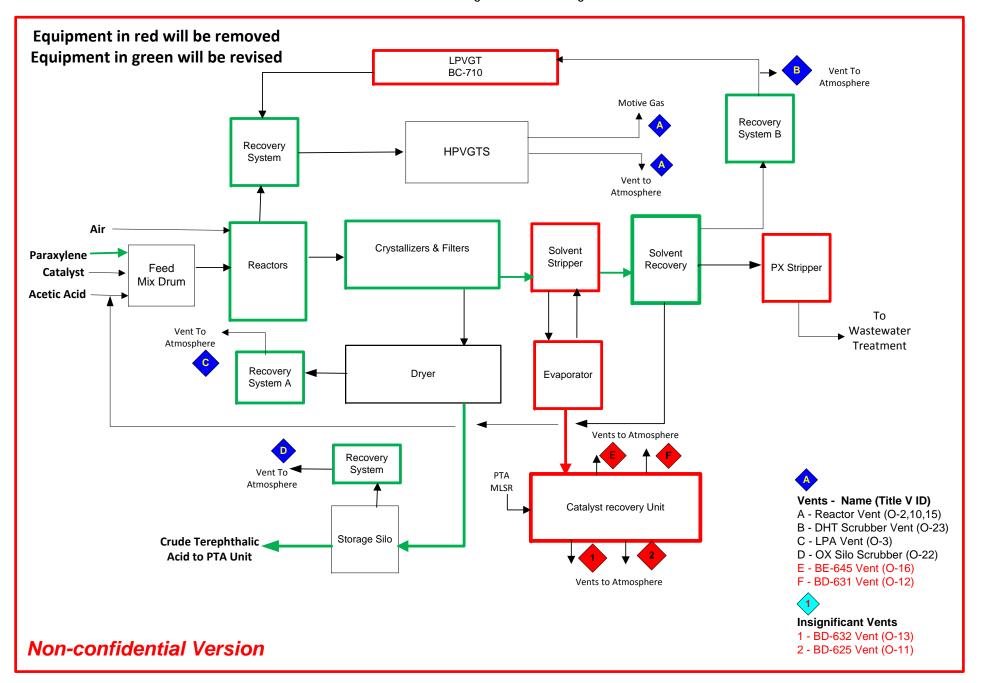


Figure 2-1.3 #1 PTA Unit Existing Process Flow Diagram

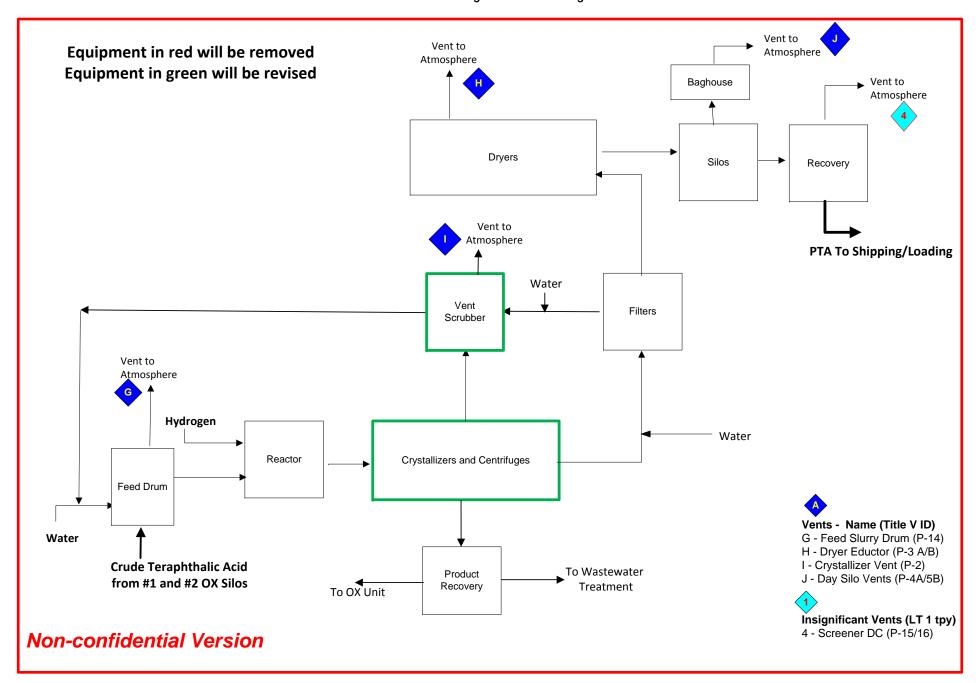


Figure 2-1.4 #2 OX Unit Existing Process Flow Diagram

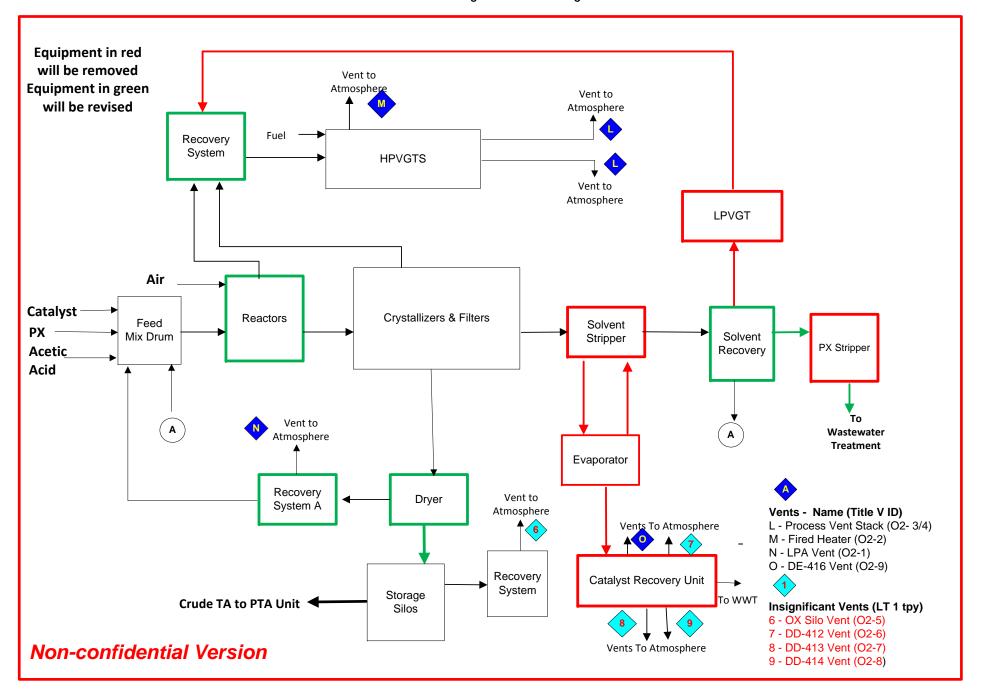


Figure 2-1.5 #2 PTA Unit Existing Process Flow Diagram

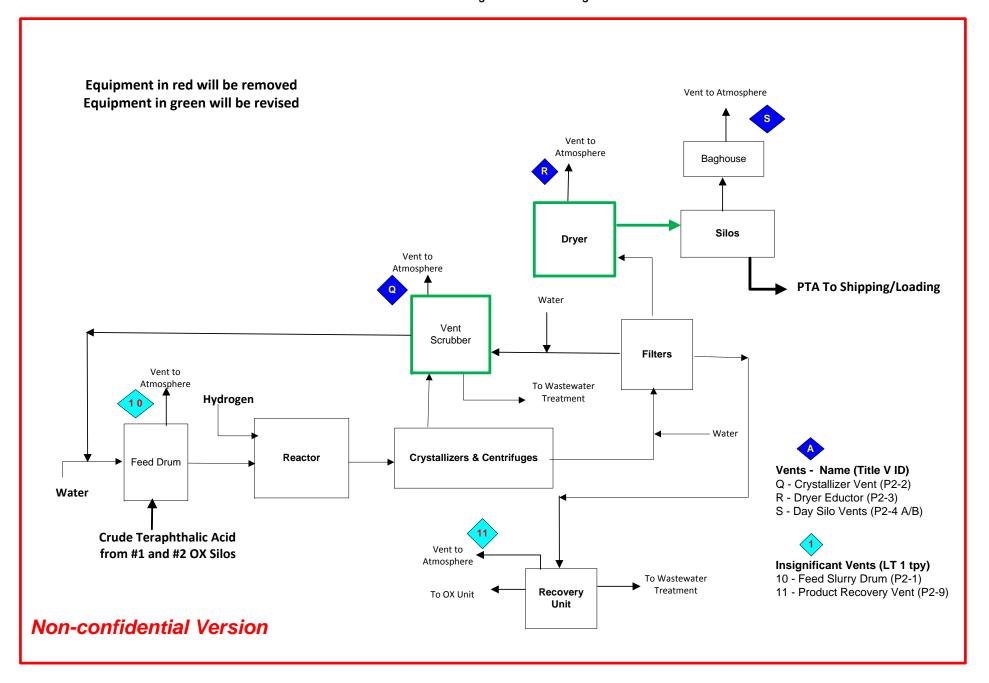


Figure 2-2.1 #1 OX Unit Future Process Flow Diagram

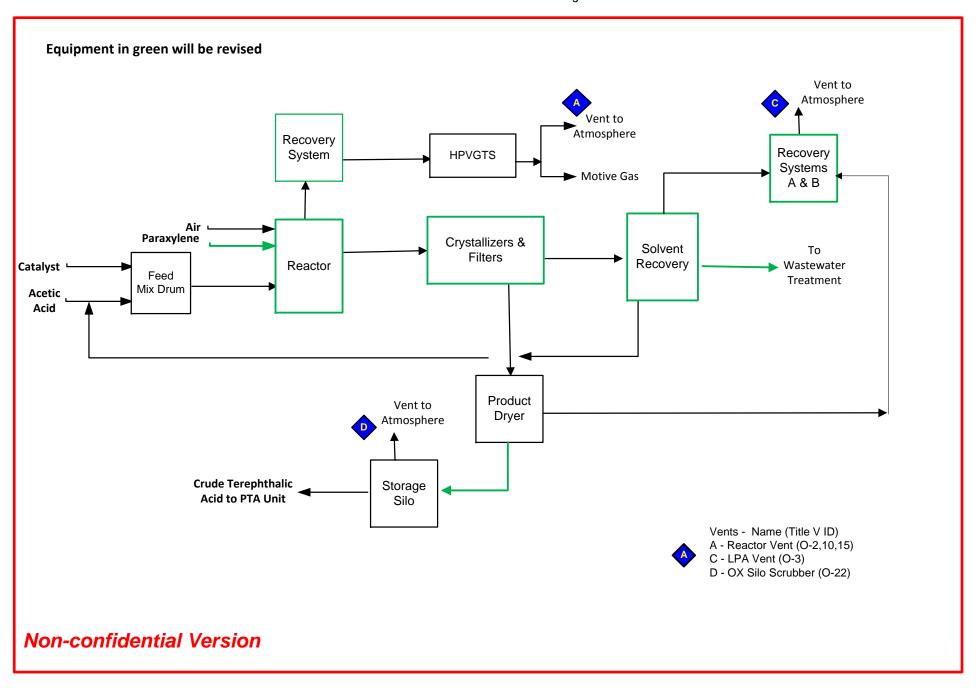


Figure 2-2.2 #1 PTA Unit Future Process Flow Diagram

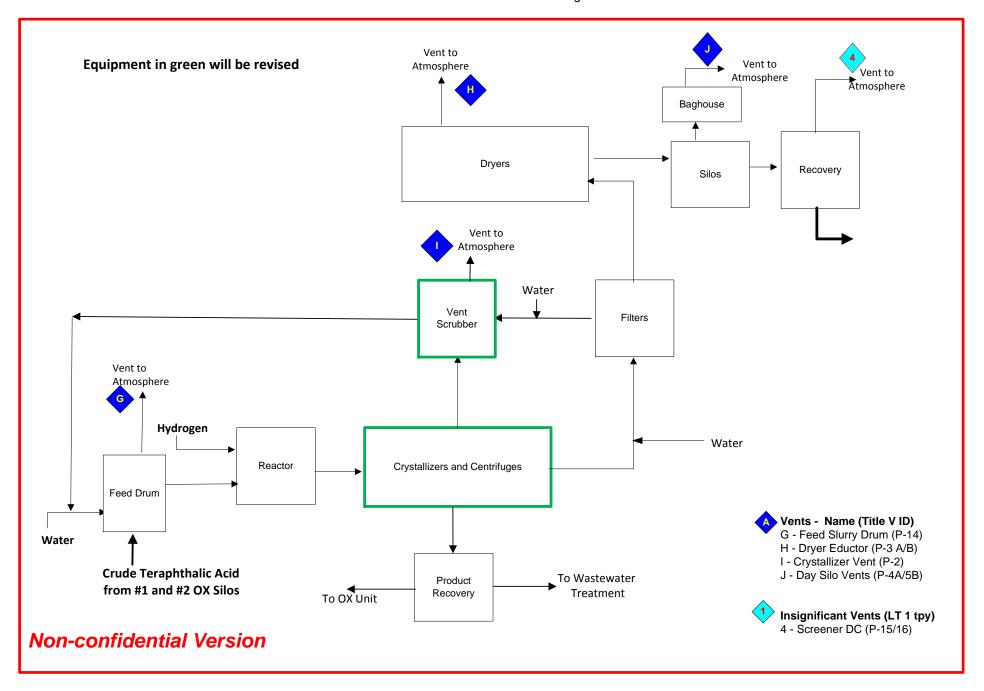


Figure 2-2.3 #2 OX Unit Future Process Flow Diagram

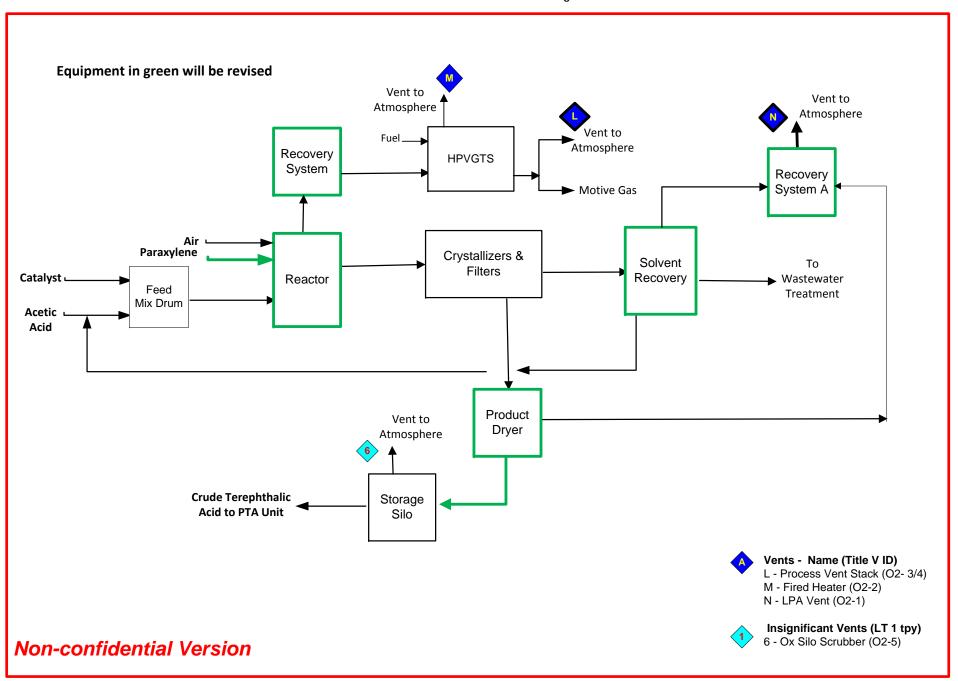
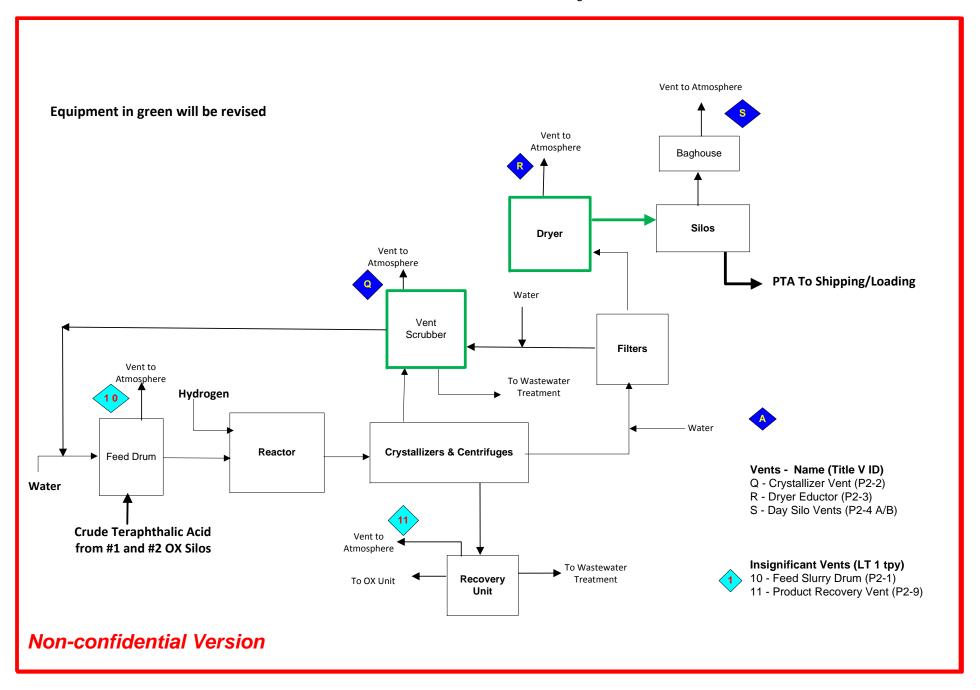


Figure 2-2.4 #2 PTA Unit Future Process Flow Diagram



Section 3 **Applicable Regulations**

A regulatory assessment was completed for the proposed OX Modernization/Debottleneck Project at the BP CR Plant. A review of both South Carolina and Federal regulations was conducted to determine the applicable air quality requirements for the proposed project. Each potentially applicable regulation is summarized in Table 3-1 and is described in the following subsections and, where applicable, the emissions limits are outlined as well as the required record keeping and monitoring requirements.

3.1 State Regulations

The following state regulations are potentially applicable to this project.

3.1.1 South Carolina Air Quality Rule 61-62.1 Section II - Permit Requirements

This regulation is applicable to the project because it states that any person who plans to construct, alter, or add to a source of air contaminants, including installation of any device for the control of air contaminant discharges, shall first obtain a construction permit from the Department prior to commencement of construction. This application is being submitted to meet this requirement.

3.1.2 South Carolina Air Quality Rule 61-62.5 Standard No. 1

This regulation is applicable to fuel combustion sources and includes emission limits for visible emissions (opacity), SO₂, and PM. This regulation would apply to the heater for the #1 OX HPVGTS. The proposed project will not change any of the existing limits or requirements for the facility.

3.1.3 South Carolina Air Quality Rule 61-62.5 Standard No. 2

This regulation is applicable to the facility. The CO PSD modeling using AERMOD shows the emissions impacts of the project are below the significant impact level. Therefore, no further modeling analysis of emissions for Standard No. 2 is needed.

Table 3-1 Summary of Potentially Applicable Regulation

REGULATORY ASSESSMENT SUMMARY				
POTENTIALLY AP	APPLICABLE TO PROJECT			
State (SC DHEC) Regulations				
SC DHEC Reg 61-62.5 Section II	Permit Requirements	Y		
SC DHEC Reg 61-62.5 Std. No. 1	Emissions from Fuel Burning Operations	Y		
SC DHEC Reg 61-62.5 Std. No. 1	Ambient Air Quality Standards	Y		
SC DHEC Reg 61-62.5 Std. No. 3	Waste Combustion and Reduction	N		
SC DHEC Reg 61-62.5 Std. No. 4	Emissions from Process Industries	Y		
SC DHEC Reg 61-62.5 Std. No. 5.1	BACT/Lowest Achievable Emission Rate (LAER) Applicable to VOCs	Y		
SC DHEC Reg 61-62.5 Std. No. 5.2	Control of NO _X	N		
SC DHEC Reg 61-62.5 Std. No. 7	PSD	Y		
SC DHEC Reg 61-62.5 Std. No. 8	TAPs	Y		
SC DHEC Reg 61-62.7	GEP Stack Height	Y		
SC DHEC Reg 61-62.60	NSPS	Y		
SC DHEC Reg 61-62.61	National Emission Standards for Hazardous Air Pollutant (NESHAP)	Y		
SC DHEC Reg 61-62.63	NESHAPs for Source Categories	Υ		
Federal Regulations				
40 CFR Part 60, Subpart A	General Provisions	Υ		
40 CFR Part 60, Subpart Da	NSPS for Electric Utility Steam Generating Units	N		
40 CFR Part 60, Subpart Db	NSPS for Industrial-Commercial- Institutional Steam Generating Units	Y		
40 CFR Part 60, Subpart Kb	NSPS for Volatile Organic Liquid Storage Tanks	N		
40 CFR Part 60, Subpart VV	NSPS for Equipment Leaks of VOC in the SOCMI Before November 7, 2006	Y		
40 CFR Part 60, Subpart VVa	NSPS for Equipment Leaks of VOC in the SOCMI After November 7, 2006	Y		
40 CFR Part 60, Subpart III	NSPS for VOC Emissions from the SOCMI Air Oxidation Unit Processes	Y		
40 CFR Part 60, Subpart NNN	NSPS for VOC Emissions from SOCMI Distillation Operations	Y		

 $TRC\ Environmental\ Corporation |\ BP\ Amoco\ Chemical\ Company\ -\ Cooper\ River\ Plant\ PSD\ Air\ Permit\ Application$

Table 3-1 **Summary of Potentially Applicable Regulation**

REGULATORY ASSESSMENT SUMMARY				
POTENTIALLY AP	APPLICABLE TO PROJECT			
40 CFR Part 60, Subpart RRR	NSPS for VOC Emissions from SOCMI Reactor Operations	N		
40 CFR Part 60, Subpart YYY (proposed)	VOC Emissions from SOCMI Wastewater	Will review when rule finalized		
40 CFR Part 60, Subpart IIII	NSPS for Stationary Compression Ignition Internal Combustion Engines	N		
40 CFR Part 61, Subpart M	National Emission Standard for Asbestos	Υ		
40 CFR Part 61, Subpart FF	National Emission Standard for Benzene Waste Operations	Y		
40 CFR Part 63, Subpart A	NESHAPs for Source Categories; General Provisions	Y		
40 CFR Part 63, Subpart F	NESHAPs for Source Categories; HON from SOCMI	Y		
40 CFR Part 63, Subpart G	NESHAPs for Source Categories; HON from SOCMI for Process Vents, Storage Vessels, Transfer Operations, and Wastewater	Y		
40 CFR Part 63, Subpart H	NESHAPs for Source Categories; HON for Equipment Leaks	Y		
40 CFR Part 63, Subpart EEEE	NESHAPs for Organic Liquids Distribution (Non-Gasoline)	N		
40 CFR Part 63, Subpart ZZZZ	NESHAPs for Stationary RICEs	Y		
40 CFR Part 63, Subpart DDDDD	NESHAPs for Industrial, Commercial, and Institutional Boilers and Process Heaters	Y		
40 CFR Part 63, Subpart GGGGG	NESHAPs for Site Remediation	Υ		
40 CFR Part 64	CAM	Y		

3.1.4 South Carolina Air Quality Rule 61-62.5 Standard No. 3

This regulation is shown as an applicable regulation for the HPVGTS catalytic oxidation reactor in the existing Title V permit. However, in the Title V renewal application submitted in January 2012, the following justification was provided to remove this as an applicable regulation:

> The existing Title V permit has both of the HPVGTS reactors subject to the SC DHEC regulation 61-62.5 Standard 3 (Waste Combustion and Reduction). The HPVGTS is not a combustion system as was intended to be covered by this regulation. However, even if the regulation is potentially applicable to the HPVGTS since the outlet of the reactors pass through a liquid scrubber prior to being released to the atmosphere it is not possible for either PM or visible emissions from the reactor to be emitted. We request that SC DHEC either agree that the regulation is not applicable to the HPVGTS or that it be exempted since the pollutants of potential concern cannot be emitted by the system.

South Carolina Air Quality Rule 61-62.5 Standard No. 4

The #1 OX/PTA and #2 OX/PTA units have emissions that are subject to this standard. All emission sources, including any fugitives, are subject to 20 percent opacity and PM limits under this standard. The proposed project does not change the process weight for any unit so it does not change any limits or create any new requirements for the affected units under this regulation.

3.1.6 South Carolina Air Quality Rule 61-62.5 Standard No. 5.1

This standard applies to the site overall. Since the net VOC emissions increase is less than 100 tons per year (tpy), this regulation has no applicable requirements for this project. However, since the net VOC emission increase exceeds the PSD threshold, a VOC BACT analysis has been completed for this PSD permit application and is included in Section 4 of the application.

3.1.7 South Carolina Air Quality Rule 61-62.5 Standard No. 5.2

This standard does not apply to this project since no new fuel combustion source is being built and none of the existing fuel combustion sources burners are being replaced in this project.

3.1.8 South Carolina Air Quality Rule 61-62.5 Standard No. 7

This standard will apply to this project since the facility is a PSD major source and the net emissions increase for at least one PSD pollutant exceeds the PSD threshold. This application is for a PSD permit for the pollutants exceeding the threshold. The results of the PSD analysis are shown in Table B-1 in Appendix B.

3.1.9 South Carolina Air Quality Rule 61-62.5 Standard No. 8

This standard would be applicable to the project since the units are a source of toxic air pollutants (TAPs). However, since both the OX and PTA units are subject to the HON Maximum Achievable Control Technology (MACT) regulation they are exempt per Standard No. 8 Section I (D) from the regulation. Therefore, air toxics modeling of the revised facility is not required by the regulation.

3.1.10 South Carolina Air Quality Rule 61-62.7

This regulation requires all emissions stacks to be in compliance with good engineering practice (GEP) provisions. All stacks have previously been assessed for compliance with GEP provisions and this project will not change any of the stacks.

3.1.11 South Carolina Air Quality Rule 61-62.60

This regulation is applicable to the project since the affected units are subject to 40 CFR Part 60 regulations that are incorporated by reference in this state regulation. This regulation will be met by the facility meeting the requirements contained in the applicable federal 40 CFR Part 60 regulations. A regulation-specific description of the requirements is contained in subsequent subsections discussing the applicable federal regulations.

3.1.12 South Carolina Air Quality Rule 61-62.61

This regulation is applicable to the unit since the facility in general is subject to 40 CFR Part 61 regulations (Subparts M and FF) that are incorporated by reference in this state regulation. This regulation will be met by the facility meeting the requirements contained in the applicable federal 40 CFR Part 61 regulations. The proposed project does not create any new or revise any requirements for the facility under this regulation.

3.1.13 South Carolina Air Quality Rule 61-62.63

This regulation is applicable to the affected units since they are subject to 40 CFR Part 63 regulations that are incorporated by reference in this state regulation. This regulation will be met by meeting the requirements contained in the applicable federal 40 CFR Part 63 regulations discussed in a later section. The proposed project does subject the units to applicability of any new federal regulations under this regulation. A regulation specific description of the requirements is contained in subsequent subsections.

3.2 Federal Regulations

The following federal regulations are potentially applicable to this project.

3.2.1 40 CFR Part 60, Subpart A

This regulation is applicable to the units and provides general requirements for emissions from source categories. This project will not change the requirements of this regulation to the affected units.

3.2.2 40 CFR Part 60, Subpart Da

This regulation is not applicable to the boilers. They may supply some portion of their steam to the steam turbines being added to the units to generate electricity but it will only be a small portion of their steam capacity and any electricity generated will be for internal use and none will be sold to a third party.

3.2.3 40 CFR Part 60, Subpart Db

This regulation is applicable to the boilers. This project will require incremental steam from the boilers but they will not be modified or increase previously permitted emissions. This project will not add any new or revise any requirements of the regulation.

3.2.4 40 CFR Part 60, Subpart Kb

The new tanks being added to the units to store the NBA or NBA/Butanol/PX mixtures will meet the minimum size to be subject to the regulation. However, the material stored has a vapor pressure at storage temperatures that is less than the minimum vapor pressure (3.5 kPa) needed for the regulation to apply to the new tanks. This regulation is not applicable to this project.

3.2.5 40 CFR Part 60, Subpart VV

The #2 OX and PTA units are subject to the New Source Performance Standard (NSPS) for equipment leaks of VOC in Synthetic Organic Chemical Manufacturing Industry (SOCMI) as set forth in 40 CFR 60, Subpart VV. The #1 OX and PTA units were built before the regulatory applicability date and they have not been modified as defined in the regulation since the applicability date so they are not subject to this regulation. In 2007, BP CR voluntarily agreed to implement a VOC Leak Detection and Repair (LDAR) program equivalent to Subpart VV for the #1 unit as a PSD offset. Neither #1 nor #2 PTA units have any process streams containing over 10 percent VOC content. BP CR is currently in compliance with all requirements of Subpart VV.

The BACT analysis for fugitives in Section 4 concluded that monitoring all equipment leak components according to 40 CFR 63 Subpart H (HON MACT LDAR) would be the applicable BACT. BP will assume that all VOCs are HAPs for determining which components will be part of the HON LDAR program. The use of the single LDAR regulation was concluded to be BACT and will simplify the monitoring program and recordkeeping.

3.2.6 40 CFR Part 60, Subpart VVa

The units are not presently subject to this regulation since they were built before the regulatory applicability date and have not been modified as defined in the regulation since the applicability date. This regulation will be applicable to the units since they will be modified as defined in the regulation after the November 6, 2006 applicability date. However, the facility has chosen an alternative means of compliance within the regulation. The facility will comply with Part 63, subpart H. Owners or operators may choose to comply with the provisions of 40 CFR Part 63, Subpart H, to satisfy the requirements of §§ 60.482-1a through 60.487a for an affected facility. When choosing to comply with 40 CFR Part 63, Subpart H, the requirements of § 60.485a (d), (e), and (f), and § 60.486a(i) and (j) still apply.

3.2.7 40 CFR Part 60, Subpart III

The #2 OX unit reactor is subject to the NSPS for VOC emissions from SOCMI air oxidation units as set forth in 40 CFR 60, Subpart III. The new #1 OX reactor will also be subject to this regulation. The Subpart III total resource evaluation (TRE) is above four after the last recovery device for both units. There are no requirements for this regulation other than to keep track of potential changes in the TRE per 40 CFR 60.610(c).

3.2.8 40 CFR Part 60, Subpart NNN

The #2 OX DHT is presently subject to the NSPS for VOC emissions from SOCMI distillation operations as set forth in 40 CFR 60, Subpart NNN. An additional NNN operation (Entrainer Recovery Tower) will be added to the unit with this project. This new distillation tower will vent to the same recovery system as the #2 OX DHT recovery system. The NNN TRE after the last recovery device in the distillation tower vent system will be above eight so there will be no requirements for this regulation other than to keep track of potential changes in the TRE.

The modifications to the #1 OX DHT will cause it to be subject to this regulation. An additional NNN operation (Entrainer Recovery Tower) will be added to the unit with this project. This new distillation tower will vent to the same recovery system as the #1 OX DHT recovery system. The NNN TRE after the last recovery device in the distillation tower vent system will be above eight so there will be no requirements for this regulation other than to keep track of potential changes in the TRE.

3.2.9 40 CFR Part 60, Subpart RRR

The regulation specifies that it is applicable to reactors, excluding reactor processes using air as a reactant, that produce one of the chemicals listed in the regulation. However, the PTA unit reactors do not produce a chemical but only purify a chemical produced in the OX unit reactor which is subject to Subpart III.

3.2.10 40 CFR Part 60, Subpart YYY

This regulation has been proposed but has not been finalized. When the regulation is finalized, the applicability to the units and the regulatory requirements will have to be assessed at that time.

3.2.11 40 CFR Part 60, Subpart IIII

None of the Reciprocating Internal Combustion Engines (RICE) associated with the affected units are subject to this regulation since they were purchased prior to the regulatory applicability date. This project will not add any RICE subject to this regulation.

3.2.12 40 CFR Part 61, Subpart M

The facility has asbestos-containing materials (ACM) on the site that must be handled in accordance with this regulation. This project will not change the requirements of this

regulation to the facility. Any ACM that is removed or disturbed during the project will be handled in accordance with this regulation.

3.2.13 40 CFR Part 61, Subpart FF

The total annual benzene (TAB) quantity from facility waste has historically been less than 1 megagrams per year (Mg/yr). This project will not cause the facilities TAB to be greater than 1 Mg/yr. This project will not change the applicable requirements to the facility.

3.2.14 40 CFR Part 63, Subpart A

This regulation is applicable to the unit and provides general requirements for the control of HAPs emissions in various regulations under 40 CFR 63. This project will not change the requirements of this regulation that are applicable to the units.

3.2.15 40 CFR Part 63, Subpart F

This regulation is applicable to the units and provides general requirements for HAP emissions from SOCMI sources. This project will not change the requirements of this regulation to the unit.

3.2.16 40 CFR Part 63, Subpart G

The #1 and #2 OX and PTA units are subject to the requirements of Subpart G as set forth in 40 CFR Part 63. These units are subject to the process vent and wastewater provisions of Subpart G with all the existing sources being HON Group 2 sources. BP CR is currently in compliance with all requirements of Subpart G. The modifications to the units will not constitute reconstruction as defined in the MACT regulations since the total cost of the project will be substantially less than the 50 percent replacement cost threshold. Therefore, the #1 units will remain existing sources and the #2 units will continue as new sources.

This project will create some new HON process vents that will also be Group 2 vents and remove some existing HON process vents. This project will also add some new tanks that will all be Group 2 storage tanks.

3.2.17 40 CFR Part 63, Subpart H

The #1 and #2 OX and PTA units are subject to the requirements of Subpart H as set forth in 40 CFR Part 63. BP CR is currently in compliance with all presently applicable requirements of Subpart H. However, based on the BACT determination for fugitives

and in order to simplify the LDAR program BP will expand this regulations' applicability by including all components that meet the 5 percent HAP content requirement for inclusion by considering all VOC as HAPs for the LDAR program determination.

3.2.18 40 CFR Part 63, Subpart EEEE

The regulation would potentially be applicable to some sources at the facility but they are all subject to the HON regulations. Hence, they are all excluded from this regulation and there are no requirements under this regulation.

3.2.19 40 CFR Part 63, Subpart GGGGG

This regulation is applicable to remediation at the site. There is currently no ongoing remediation at the site. However, if any events occur at the site that trigger remediation, the requirements of this regulation will be applied.

3.2.20 40 CFR Part 63, Subpart ZZZZ

The RICEs associated with the units are subject to this regulation. All the subject engines are diesel-powered combustion ignition engines and do not have any applicable emission standards but have work practice standards to meet. This project will not add any new equipment subject to this regulation nor will it revise the requirements for the existing engines.

3.2.21 40 CFR Part 63, Subpart DDDDD

The boilers and #2 OX-HPVGTS heater are subject to the requirements for HAP emissions as set forth in 40 CFR 63, Subpart DDDDD. The Title V renewal application submittal has requested a permit revision to limit the boilers to burning gaseous fuels and would only burn liquid fuel during a gas curtailment or for no more than 48 hours per year for testing. The boilers will meet the requirements for a gas-fired boiler. The #2 HPVGTS heater only burns gas and will meet the requirements for a gas-fired heater. This project will not change the requirements of this regulation to the sources.

3.2.22 40 CFR Part 64

This regulation specifies the requirements for monitoring to assure compliance with emission limits for applicable pollutant specific emission units. The facility has received a Title V renewal permit including required compliance assurance monitoring (CAM) conditions. The present CAM will be revised, as necessary, to reflect the changes in the process flow and control schemes.

Section 4 Best Available Control Technology Analysis for Volatile Organic Compound Emissions and Carbon Monoxide

Control Technology Information 4.1

The following is a brief description of each of the control technologies that will be considered in at least one of the BACT analysis to follow. The possible control efficiency for each technology shown in the following descriptions is the upper range for each technology and may not be possible but has been assumed for BACT purposes (i.e., an RTO may not be able to achieve 99 percent in practice).

- **Thermal Oxidizer (TO)** –A TO is a controlled combustion technology for air pollution control of a gaseous stream. Fuel and air are added to a combustion chamber through which the exhaust gases pass to maintain a high minimum operating temperature and decompose the VOC and CO into carbon dioxide (CO2) and water (H2O) before releasing them to the atmosphere. This technology has a possible control efficiency of 99 percent for VOC and 95 percent for CO. The operation of a TO will result in an increase in pollutants from natural gas combustion, specifically nitrogen oxides, which is an added environmental impact.
- Regenerative Thermal Oxidizer (RTO) This control technology is similar to a TO in the manner it controls the VOC and CO emissions. The difference in the RTO versus a TO is the energy efficiency it achieves by storing heat in ceramic media as the process stream enters and exits the combustion chamber. The directions of the airflow is reversed every 1 to 3 minutes by a series of valves to alternately store and regenerate the heat – the inlet process stream gets pre-heated and the outlet process stream gives up the heat. The result is a more energy efficient operation than a TO. This technology has a possible control efficiency of 99 percent for VOC and 95 percent for CO. The operation of a RTO will result in an increase in pollutants from natural gas combustion, specifically nitrogen oxides, which is an added environmental impact.
- **Recuperative Thermal Oxidizer (RCO)** This control technology is similar to a TO in the manner it controls the VOC and CO emissions. The difference in the RCO versus a TO is the energy efficiency it achieves by a primary and/or secondary heat exchanger within the system. A primary heat exchanger preheats the incoming vent stream by recuperating heat from the exiting treated stream. As the incoming air passes on one side of the exchanger heat is transferred to it through the process of conduction from the hot clean air from the

combustion chamber passing on the other side of the exchanger. This technology has a possible control efficiency of 99 percent for VOC and 95 percent for CO. The operation of a RCO will result in an increase in pollutants from natural gas combustion, specifically nitrogen oxides, which is an added environmental impact.

- Catalytic Thermal Oxidizer (CTO) This control technology decomposes the VOC and CO into CO2 and water at lower temperatures than a TO in the presence of a catalyst to promote the reaction. The lower temperatures will reduce the amount of supplemental heat required for the process and reduce possible natural gas combustion emissions. Catalytic oxidation occurs through a chemical reaction between the VOC hydrocarbon molecules and a precious-metal catalyst bed that is internal to the oxidizer system. A catalyst is a substance that is used to accelerate the rate of a chemical reaction, allowing the reaction to occur in a much lower normal temperature range. This technology has a possible control efficiency of 99 percent for VOC and 95 percent for CO. The operation of a CTO will result in an increase in pollutants from natural gas combustion, specifically nitrogen oxides, which is an added environmental impact. An additional disadvantage is the disposal of the spent catalyst. Depending on the catalyst type, the spent catalyst may require disposal in an approved hazardous waste disposal site.
- Flare A gas flare, alternatively known as a flare stack, is an open air gas combustion device used for burning off flammable gas that will be released to the atmosphere. The vent stream being treated must contain a minimum British thermal units/standard cubic feet (Btu/scf) value to maintain combustion or a supplemental fuel must be added to meet the minimum. The control requirements in 40 CFR 60.18 states a flare shall only be used as a control device if the vent stream being combusted has a net heating value of at least 200 Btu/scf. This is to prevent very low Btu vent streams from blowing out the flare flame. This technology has a possible control efficiency of 98 percent for VOC. This control technology has a disadvantage of potentially producing as many CO emissions as it would destroy so it may not be a feasible technology for CO control.
- Absorber/Scrubber Absorber/Scrubber systems are air pollution control devices that can be used to remove some particulates and/or gases from industrial exhaust streams. This process works via the contact of contaminants with the absorbing/scrubbing solution to remove the contaminants from the vent stream. The process uses rapid gas absorption by use of pressure drop and excellent gas and liquid distribution either mechanically or physically to remove the contaminants. Solutions may simply be water (for dust) or solutions of reagents that specifically target certain compounds. Gas enters at the bottom of the absorber and is contacted in a countercurrent fashion in the absorption section by the scrubbing liquid that is sprayed into the top of the scrubber. The gas stream passes upward in the tower through a mist eliminator where entrained droplets are removed before the exhaust gas enters the stack. The scrubber solution is collected in the bottom of the tower where most of the scrubbing solution is recycled to the top of the tower. A small amount of scrubber solution is bled to remove the scrubbed VOC and to allow for the

addition of fresh scrubbing liquid. This technology has a possible control efficiency of 95 percent for VOC but will not control CO emissions. The operation of an absorber/scrubber will result in an increase of a spent scrubbing solution that must be treated before being disposed.

- **Adsorber** An adsorber removes contaminants by adsorbing them onto a solid material, such as activated carbon, that has a high surface area and is used to capture a gas or liquid. The adsorbed material can then be removed by steam or combustion and the carbon reused. This technology has a possible control efficiency of 98 percent for VOC but will not control CO emissions. The operation of an absorber/scrubber will result in an increase of a solid waste (spent carbon) that must be treated before being disposed
- **Condenser** A condenser is a device or unit used to condense a substance from its gaseous to its liquid state, typically by cooling it. In so doing, the latent heat is given up by the substance, and will transfer to the condenser coolant. Condensers are typically heat exchangers which have various designs and come in many sizes ranging from rather small (hand-held) to very large industrial-scale units used in plant processes. The condensed liquid can be recovered or recycled. This technology has a possible control efficiency of range of 50 to 90 percent for VOC depending on the concentration and VOC compounds present in the stream but will not control CO emissions.

Best Available Control Technology Analysis for Volatile Organic Compound 4.2 **Emissions from Low Pressure Absorbers**

The OX unit LPA is a recovery device for several process streams in the unit. The LPA recovers the acetic acid in the inlet streams and recycles it into to the process so it eventually reaches the reactor system. This is a valuable material that acts as the solvent for the process and any loss from the LPA outlet must be replaced by purchase of fresh acetic acid. Part of the optimization of the manufacturing process is to minimize the loss of acetic acid.

This project plans to remove the compressor on the DHT overhead stream (LPVGT) and route the DHT overhead through an acetic acid scrubber and then to the LPA. The LPA operates at about 5 inches water (H2O) pressure and is estimated to recover over \$1,000,000 per year of valuable process solvents.

The PTE VOC emissions from the LPA will be 42.0 tpy for #1 OX LPA and 38.8 tpy for #2 OX LPA. The LPA outlet stream will require a fan to raise the pressure sufficiently to allow the stream to go to a control device. This analysis will be based on add-on controls to the outlet of the LPA recovery device.

4.2.1 Identification of Control Technologies

The reasonably available control technology (RACT), BACT, LAER Clearinghouse (RBLC) database was queried for emission sources and control devices of VOC that are used in the process types 64.000, 64.003 and 64.999, SOCMI production. The results of the RBLC search are shown in Appendix C. The search returned several facilities and processes for BACT in these industrial categories. The following control devices were identified from the search as potential add-on controls to the LPA outlet:

Absorber/ScrubberCondenserRTO

Flare

In the RBLC, no control devices were found to apply directly to the PTA manufacturing process.

Other resources of control technology were reviewed, such as *EPA Air Pollution Control Technology Fact Sheets*; *EPA Air Pollution Control Cost Manual Sixth Edition*, EPA/452/B-02-001, January 2002; and the applicable NSPS and NESHAP standards. The results of this review indicated that the following control equipment may be effective in

the reduction of VOCs:

_ Adsorber _ CT

– RCO

A BACT analysis was performed for each of the control equipment options. The processes currently do not have any add-on controls after the LPA.

4.2.2 Elimination of Infeasible Control Options

Seven control options were evaluated qualitatively to determine if these options are technically feasible. The following control technologies were all determined to be technically feasible for control of VOC:

4-4

- 1. TO
- 2. RTO
- 3. RCO
- 4. CTO
- Absorber/Scrubber
- 6. Adsorber

7. Condenser

8. Flare

While the above technologies are all technically feasible, they will require the additional equipment to raise the pressure on the LPA outlet to allow it to flow through any of these control devices. The installation of the additional equipment to increase the pressure of the process stream (i.e., fan/blower) to allow it to flow through a control device will in turn increase the capital cost for the proposed configuration. Also any VOC or organics recovered/captured would not be able to be recycled to the process since the materials would be contaminants for the process and be detrimental to the operation. Therefore, additional equipment will be required to treat the recovered material. The addition of an absorber/wet scrubber to the outlet of the LPA while being feasible will have much lower removal efficiency than a normal scrubber since the stream is already being treated in the LPA which is a two-stage absorber system.

A detailed economic analysis of the technically feasible options has been performed and is summarized in the following subsections.

4.2.3 Ranking of Remaining Control Technologies

The potential effectiveness of the remaining control options has been evaluated by reviewing manufacturer information and United States Environmental Protection Agency (USEPA) documents. The remaining control options and their associated anticipated efficiencies are listed below:

CONTROL OPTION	EFFICIENCY (%)
то	99
СТО	99
RTO	99
RCO	99
Carbon Adsorption/TO	98
Flare	98
Refrigerated Condenser	55
Absorber/Scrubber	50

4.2.4 Evaluation of Most Effective Control Technologies and Selection of Best Available Control Technology

The BACT analysis is a three-part investigation that includes economic, energy, and environmental impacts. Each of the remaining options was reviewed with respect to the impacts to determine if they meet BACT requirements.

Economic Analysis

The economic analysis is composed of a calculation of the control technologies' average cost effectiveness (ACE) based on a comparison of the cost of each feasible control technology in terms of cost per mass of pollutant removed. In general, technologies with excessive costs per ton of pollutant removed are considered excessive in most cases and the installation of that technology would not be deemed economically feasible.

The ACE was determined by estimating the capital cost for an installed system and the resulting annual operating and maintenance costs. The capital and operating expenses were obtained from using the EPA Air Pollution Control Cost Manual Sixth Edition, EPA/452/B-02-001 or EPA's Air Pollution Control Fact *Sheets.* The ACE is estimated according to the following formula:

ACE = (Control Option Annualized Cost)/(Baseline emission rate - Control option emission rate)

The baseline VOC emissions from #1 OX LPA are estimated at 42.0 tpy and #2 OX LPA as 38.8 tpy. The #1 OX LPA emission rate was used as the baseline emission rate for the BACT analysis. This emission rate is used to determine the ACE for each specific control option. This emission rate would be representative for both #1 OX LPA and #2 OX LPA since the ratio of the flow rate impact on equipment costs and emission rates were both about 92 percent. Since the #1 emission rate is higher it would give the lowest ACE values for determining if any of the control technologies were economically feasible.

The ACE can be estimated from the capital and annual operating costs by annualizing the capital cost (multiplying by a factor of 0.10 to simulate a 20-year equipment life and an 8 percent interest rate). This value is added to the annual operating cost and the sum is divided by the product of the control efficiency and the uncontrolled emission rate. As an example ACE calculation, assume the control efficiency of an option is 99 percent. The (baseline emission rate-control option emission rate) for each option is equal to {42.0 tpy - [42.0 tpy X (1-99%)]} or 41.6 tons on an annual basis. This emission rate is used to determine the ACE for the specific control option.

Table 4-1 provides a summary of the annualized operating cost and average cost effectiveness for each of the control options. The cost analysis information is provided in Appendix D, BACT Analysis Cost Information.

Table 4-1 LPA VOC BACT Analysis

CONTROL OPTION	EMISSION REDUCTION (tpy)	TOTAL CAPITAL COST (\$)	ANNUALIZED OPERATING COST (\$)	AVERAGE COST EFFECTIVENESS (\$/ton)	INCREASED ENERGY USAGE (\$/yr)	ADVERSE ENVIRONMENTAL IMPACTS?
ТО	41.6	\$1,070,7562	\$478,978	\$11,506	\$249,1272	Yes
СТО	41.6	1,464,014	394,328	9,472	100,324	Yes
RTO	41.6	1,179,994	365,915	8,790	105,751	Yes
RCO	41.6	1,660,644	518,557	12,456	110,983	Yes
Carbon Adsorber/TO	41.2	1,247,886	509,141	12,355	14,811	Yes
Flare	41.2	643,438	2,454,509	59,565	2,072,818	Yes
Refrigerated Condenser	23.1	764,251	360,665	15,528	17,050	Yes
Absorber/Scrubber	21.0	637,990	421,904	20,067	3,789	Yes

The ACE value for the options discussed above are high enough per ton of VOC removed, to not be economically feasible. A comparison to recent South Carolina PSD permit application for AGY-Aiken, LLC shows that ACE values in the range of \$5,760 to \$9,031 were deemed not cost effective for control of VOC. The options with the lowest ACE are a CTO or a RTO. However, the use of an RTO for a stream containing a halogen compound (methyl bromide) is not recommended because of the formation of highly corrosive acid gases per USEPA technology fact sheets (see Appendix H). The only remaining potentially feasible option is a CTO which has the lowest ACE value. The energy and environmental factors need to be considered for the CTO option to determine the appropriate BACT technology.

Energy Analysis

An energy impact analysis is used to identify if the technically feasible control options result in any significant or unusual energy penalties or benefits. The feasible control options have been evaluated and it has been determined that no unusual energy penalties exist beyond what was considered in the economic analysis described in the previous section. Each of the combustion options will require a substantial amount of increased fuel gas consumption. The carbon adsorption will require additional fuel to produce the regeneration steam and the natural gas for the combustion device to control the VOC emissions during the regeneration. An analysis of energy benefits was also considered; the various options do not result in any energy benefit for the BP facility.

Environmental Analysis

A review of the control options with respect to the environment was conducted to determine if any of the options created any adverse environmental impacts. The TO, RTO, RCO, and CTO control options results in significant increases in energy usage from powering fans with electricity to heating the vent streams with natural gas. The scrubber option generates a large volume of wastewater that would need to be treated. Thermal options (TO, RTO, and RCO) will also generate more products of combustion such as greenhouse gases (GHG), CO, and NOx that make these control options less environmentally beneficial. The CTO option will generate more GHG and NOx making it a poor choice for BACT considering the ACE for this option is high. The condenser option will create a large volume of liquid waste that will need to be treated prior to discharge. The proposed technically feasible options are not environmentally

beneficial and in all cases create byproducts such as wastewater and secondary air emissions.

4.2.5 Selection of Best Available Control Technology

Based on the economic, energy, and environmental impacts associated with the technically feasible control options, BP has concluded that the proper operation of the LPA recovery system is BACT and no add-on control technology to the LPA outlet is justified. BP proposes a BACT limit for VOC emissions from the #1 OX LPA of 42.0 tpy (12 lbs/hr) and #2 OX LPA of 38.8 tpy (11 lbs/hr) on a rolling 12-month sum. This process vent will be subject to CAM monitoring and will be monitored in accordance with the existing CAM plan to demonstrate compliance with the BACT limits. The details of the monitoring are listed in Subsection 2.5 of this application. If performance testing is required the VOC emissions will be determined every 36 months in accordance with either Method 18 or 25A.

4.3 Best Available Control Technology Analysis for Volatile Organic Compound **Emissions from High Pressure Absorbers**

The OX unit reactor temperature is controlled by boiling off some of the liquid in the reactor. This vapor stream goes through several stages of condensing, with the condensed liquid being returned to the reactor, before the reactor overhead is sent to the recovery system. This recovery system consists of an acetic acid scrubber and then the HPA. This analysis will be based on add-on controls to the outlet of the HPA recovery device.

Presently the outlet of the HPA is sent to the HPVGTS where the pollutants (VOC, CO, and HAPs) are controlled in a catalytic oxidation reactor and a bromine scrubber before the stream is exhausted to either the inert gas system for use as a carrier gas for the conveying system or the expander for power recovery prior to being exhausted to the atmosphere. Any control option must include a bromine scrubber to comply with the Montreal Protocol agreement on methyl bromide emissions. The carrier gas for the conveying system must not contain over 5 percent oxygen to avoid explosive conditions in silos with the PTA dust. Therefore, any thermal control technology that requires additional air for the control option would have to provide an alternative inert carrier gas (e.g., nitrogen).

The PTE VOC emissions from the HPA will be 1,025.0 tpy for #1 OX HPA and 765.0 tpy for #2 OX HPA.

Identification of Control Technologies

The RBLC database was queried for emission sources and control devices of VOC that are used in the process type Process Vents (emissions from air OX, distillation, and other reaction vessels), Organic Chemical production. The results of the RBLC search are shown in Appendix C. The search returned nine facilities and 33 processes for BACT in this industrial category. The following control devices were identified from the search:

Absorber/Wet Scrubber Condenser

TO **RTO**

Flare

No control devices were found to apply directly to the PTA manufacturing process.

Other resources of control technology were reviewed, such as EPA Air Pollution Control Technology Fact Sheets; EPA Air Pollution Control Cost Manual Sixth Edition, EPA/452/B-02-001, January 2002; and the applicable NSPS and NESHAPs standards. The results of this review indicated that the following control equipment may be effective in the reduction of VOCs:

Adsorber **RCO**

CTO

A BACT analysis was performed for each of the control equipment options. The processes currently utilize a CTO as the add-on control device.

4.3.2 Elimination of Infeasible Control Options

The control options were evaluated qualitatively to determine if these options are technically feasible. The following control technologies were all determined to be technically feasible for control of VOC:

- 1. Absorber/Wet Scrubber
- 2. Adsorber
- 3. TO
- 4. **RTO**
- 5. **RCO**
- 6. CTO (existing HPVGTS)
- 7. Condenser

The use of a Flare was found to be technically infeasible since as discussed above the outlet of the control device would need to go to a bromine scrubber to remove the halogens per the Montreal Protocol agreement. Sources controlled by flares are not amenable to post-flare control. Since a scrubber cannot be added to the flare outlet, this control option is technically infeasible. The addition of an absorber/wet scrubber to the outlet of the HPA while being feasible will have much lower removal efficiency than a normal scrubber since the stream is already being treated in a two-stage absorber system that has already removed most of the pollutants.

A detailed economic analysis of the technically feasible options has been performed and is summarized in the following subsections.

4.3.3 Ranking of Remaining Control Technologies

The potential effectiveness of the remaining control options has been evaluated by reviewing manufacturer information and USEPA documents. The remaining control options and their associated anticipated efficiencies are listed below:

CONTROL OPTION	EFFICIENCY (%)
TO/Bromine Scrubber	99
RTO/Bromine Scrubber	99
RCO/Bromine Scrubber	99
CTO (Existing HPVGTS with Bromine Scrubber)	98
Carbon Adsorption/TO/Bromine Scrubber	98
Refrigerated Condenser/Bromine Scrubber	90
Scrubber/Absorber	55

4.3.4 Evaluation of Most Effective Control Technologies and Selection of Best Available Control Technology

The BACT analysis is a three-part investigation that includes economic, energy, and environmental impacts. Each of the options was reviewed with respect to the impacts to determine if they meet BACT requirements.

Economic Analysis

The economic analysis is composed of a calculation of the control technologies' ACE based on a comparison of the cost of each feasible control technology in terms of cost per mass of pollutant removed. In general, technologies with

excessive costs per ton of pollutant removed are considered excessive in most cases and the installation of that technology would not be deemed economically feasible.

The ACE was determined by estimating the capital cost for an installed system and the resulting annual operating and maintenance costs. The capital and operating expenses were obtained from the EPA Air Pollution Control Cost Manual Sixth Edition, EPA/452/B-02-001 or EPA's Air Pollution Control Fact *Sheets.* The ACE is estimated according to the following formula:

ACE = (Control Option Annualized Cost)/(Baseline emission rate - Control option emission rate)

The #1 OX baseline emissions are estimated at 1,025.0 tpy. This emission rate was used as the baseline emission rate for the BACT analysis. This emission rate is used to determine the ACE for the specific control option. The #1 OX emissions would give the worst case answer since the equipment cost ratio based on relative flow rates would be about 90 percent but the #2 emission rate is only about 75 percent. Therefore the ACE for the #2 OX case would be higher for a comparable control option.

The ACE can be estimated from the above capital and annual operating costs by annualizing the capital cost (multiplying by a factor of 0.10 to simulate a 20-year equipment life and an 8 percent interest rate). This value is added to the annual operating cost and the sum is divided by the product of the control efficiency and the uncontrolled emission rate. Table 4-2 provides a summary of the annualized cost and ACE values for each of the control options. The cost analysis information is provided in Appendix D, BACT Analysis Cost Information.

The TO, RTO, and RCO options are not cost effective based on a comparison to recent South Carolina PSD permit application for AGY-Aiken, LLC that indicated that ACE values in the range of \$5,760 to \$9,031 were deemed not cost effective for control of VOC. The ACE value for the CTO (existing HPVGTS with existing bromine scrubber) is the highest efficiency control option with an economically feasible control cost. Therefore the existing control option meets the criteria for BACT.

Table 4-2 HPA VOC BACT Analysis

CONTROL OPTION	EMISSION REDUCTION (tpy)	TOTAL CAPITAL COST (\$)	ANNUALIZED OPERATING COST (\$)	AVERAGE COST EFFECTIVENESS (\$/ton)	INCREASED ENERGY USAGE (\$/yr)	ADVERSE ENVIRONMENTAL IMPACTS?
TO/Bromine Scrubber	1,014.7	\$2,512,7044	\$29,543,821	\$29,117	11,306,341	Yes
RTO/Bromine Scrubber	1,014.7	5,530,255	19,689,949	19,405	1,002,328	Yes
RCO/Bromine Scrubber	1,014.7	3,331,993	29,079,323	28,659	5,563,302	Yes
CTO (Existing HPVGTS with Bromine Scrubber)	1,004.4	0	806,690	803	0	Yes
Carbon Adsorption/TO/ Bromine Scrubber	1,004.4	2,321,727	4,747,662	4,727	28,257	Yes
Scrubber/Absorber	563.8	2,860,342	2,003,871	3,555	0	Yes
Refrigerated Condenser/ Bromine Scrubber	922.4	2,990,787	1,129,548	1,225	0	Yes

Energy Analysis

An energy impact analysis is used to identify if the technically feasible control options result in any significant or unusual energy penalties or benefits. The feasible control options have been evaluated and it has been determined that no unusual energy penalties exist beyond what was considered in the economic analysis described in the previous section. Each of the combustion options will require a substantial amount of increased fuel gas consumption. The carbon adsorption will require additional fuel to produce the regeneration steam and the natural gas for the combustion device to control the VOC emissions during the regeneration. An analysis of energy benefits was also considered; the various options do not result in any energy benefit for the BP facility.

Environmental Analysis

A review of the control options with respect to the environment was conducted to determine if any of the options created any adverse environmental impacts. The TO, RTO, and RCO control options results in significant increases in energy usage from powering fans with electricity to heating the vent stream with natural gas. The scrubber option generates a large volume of wastewater that that must be treated. Thermal options (TO, RTO, and RCO) will also generate more products of combustion such as GHG, CO, and NOx that make these control options less environmentally beneficial. The condenser option will create a large volume of liquid waste that will need to be treated prior to discharge. The proposed technically feasible options are not environmentally beneficial and in all cases create byproducts such as wastewater and secondary air emissions.

4.3.5 Selection of Best Available Control Technology

Based on the energy, environmental, and economic impacts associated with the technically feasible control options, BP has concluded that the CTO (existing HPVGTS with bromine scrubber) is the highest control efficiency option that is economically feasible. Therefore the CTO (existing HPVGTS with bromine scrubber) control option meets the criteria for BACT. BP proposes a BACT limit for VOC emissions from the #1 HPVGTS of 20.5 tpy (6 lbs/hr) and #2 HPVGTS of 15.3 tpy (5 lbs/hr) on a rolling 12-month sum. These process vents are subject to CAM requirements and will be monitored in accordance with the existing CAM plan to demonstrate compliance with the BACT limit. The details of the monitoring are listed in Subsection 2.5 of this

application. If performance testing is required the VOC emissions will be determined every 36 months in accordance with either Method 18 or Method 25A.

4.4 Best Available Control Technology Analysis for Volatile Organic Compound **Emissions from Crystallizer Vent Scrubbers**

The temperature of the PTA crystallizers is controlled by flashing off some of the liquid in the crystallizer. This vapor stream is routed to the PTA Crystallizer Vent Scrubber where the stream is scrubbed with water to remove the entrained PM, which in mostly PTA product. The scrubbing water containing the PM is sent to the PTA feed drum for slurrying the TA feed and to recycle the PTA recovered in the Vent Scrubber.

The scrubbed vapor from the Crystallizer Vent Scrubber, which is about 99 percent steam, is emitted to the atmosphere and contains about 46.5 tpy of VOC in #1 and #2 PTA Crystallizer Vent Scrubbers. The VOC emitted from the vent scrubber is material entrained in the TA feed to the PTA section.

4.4.1 Identification of Control Technologies

Absorber/Wet Scrubber

The RBLC database was queried for emission sources and control devices of VOC that are used in the process type Process Vents (emissions from air OX, distillation, and other reaction vessels), Organic Chemical production. The results of the RBLC search are shown in Appendix C. The search returned nine facilities and 33 processes for BACT in this industrial category. The following control device was identified from the search:

Condenser

RTO

No control devices were found to apply directly to the PTA manufacturing process.
Other resources of control technology were reviewed, such as EPA Air Pollution Control
Technology Fact Sheets; EPA Air Pollution Control Cost Manual Sixth Edition,
EPA/452/B-02-001, January 2002; and the applicable NSPS and NESHAP standards. The
results of this review indicated that the following control equipment may be effective i

Adsorber **CTO**

RCO

the reduction of VOCs:

TO

Flara

A BACT analysis was performed for each of the control equipment options. The processes currently do not have any add-on controls to the PTA crystallizer emissions.

4.4.2 Elimination of Infeasible Control Options

The control options were evaluated qualitatively to determine if these options are technically feasible. The following control technologies were determined to be technically feasible for control of VOC:

- 1. Absorber/Scrubber
- 2. TO
- 3. **CTO**
- 4. **RTO**
- 5. **RCO**
- 6. Condenser

The use of a Flare was found to be technically infeasible since the use on a high volume stream that is over 99 percent steam with a heating value of less than 1 Btu/scf is not feasible.

The use of carbon adsorption is not technically feasible because of the high moisture content, over 99 percent, of the stream from the crystallizer scrubber. At moisture contents over 50 percent, water molecules begin to compete with the hydrocarbon for active adsorption sites which significantly lowers the efficiency and capacity of the system.

A detailed economic analysis of the remaining technically feasible options has been performed and is summarized in the following subsections.

4.4.3 Ranking of Remaining Control Technologies

The potential effectiveness of the remaining control options has been evaluated by reviewing manufacturer information and USEPA documents. The remaining control options and their associated anticipated efficiencies are listed below:

CONTROL OPTION	EFFICIENCY (%)
то	99
СТО	99
RTO	99

OX Modernization/Debottleneck Project

CONTROL OPTION	EFFICIENCY (%)
RCO	99
Scrubber	95
Condenser	70

4.4.4 Evaluation of Most Effective Control Technologies and Selection of Best Available Control Technology

The BACT analysis is a three-part investigation that includes economic, energy, and environmental impacts. Each of the remaining options was reviewed with respect to the impacts to determine if they meet BACT requirements.

Economic Analysis

The economic analysis is composed of a calculation of the control technologies' ACE based on a comparison of the cost of each feasible control technology in terms of cost per mass of pollutant removed. In general, technologies with excessive costs per ton of pollutant removed are considered excessive in most cases and the installation of that technology would not be deemed economically feasible.

The ACE was determined by estimating the capital cost for an installed system and the resulting annual operating and maintenance costs. The capital and operating expenses were obtained from the *EPA Air Pollution Control Cost Manual Sixth Edition*, EPA/452/B-02-001 or *EPA's Air Pollution Control Fact Sheets*. The ACE is estimated according to the following formula:

ACE = (Control Option Annualized Cost)/(Baseline emission rate - Control option emission rate)

The baseline emissions are estimated at 46.5 tpy for the #2 PTA crystallizer vent scrubber emissions. The #2 PTA emission rate was used as the baseline emission rate for the BACT analysis. This emission rate is used to determine the ACE for the specific control option. The #2 emission rate would give the worst case answer since the equipment cost ratio based on relative flow rates would be over 100 percent but the #1 emission rate is only about 56 percent. Therefore the ACE for the #2 OX case would be higher for a comparable control option. Table 4-3 provides a summary the annualized cost and ACE values for each of the control options. The cost analysis information is provided in Appendix D, BACT Analysis Cost Information.

Table 4-3 Crystallizer Scrubber VOC BACT Analysis

CONTROL OPTION	EMISSION REDUCTION (tpy)	TOTAL CAPITAL COST (\$)	ANNUALIZED OPERATING COST (\$)	AVERAGE COST EFFECTIVENESS (\$/ton)	INCREASED ENERGY USAGE (\$/yr)	ADVERSE ENVIRONMENTAL IMPACTS?
ТО	46.0	\$1,322,004	\$1,248,118	\$27,113	\$982,627	Yes
СТО	46.0	2,414,389	1,052,109	22,855	627,544	Yes
RTO	46.0	1,453,090	711,415	15,454	410,012	Yes
RCO	46.0	2,326,998	1,367,493	29,707	933,265	Yes
Scrubber	44.2	1,702,867	572,957	12,971	3,800	Yes
Condenser	32.6	753,259	359,105	11,033	17,050	Yes

A comparison to recent South Carolina PSD permit application for AGY-Aiken, LLC shows that ACE values in the range of \$5,760 to \$9,031 were deemed not cost effective for control of VOC. Since the ACE value for the options are all very high per ton of VOC removed, these are not economically feasible.

Energy Analysis

An energy impact analysis is used to identify if the technically feasible control options result in any significant or unusual energy penalties or benefits. The feasible control options have been evaluated and it has been determined that no unusual energy penalties exist beyond what was considered in the economic analysis described in the previous section. The remaining options do not appear to have any significant energy savings that have not already been considered as part of the economic analysis.

Environmental Analysis

A review of the control options with respect to the environment was conducted to determine if any of the options created any adverse environmental impacts. Each of the control options results in significant increases in energy usage from powering fans with electricity to heating vent streams with natural gas. The scrubber and condenser options will generate large quantities of wastewaters that will need to be treated in the wastewater plant. Thermal options (TO, RTO, and RCO) will also generate significant quantities of products of combustion such as GHG, CO, and NOX that make these control options less environmentally beneficial. The results of those analyses are combined with this analysis to select the best control option.

4.4.5 Selection of Best Available Control Technology

Based on the energy, environmental, and economic impacts associated with the technically feasible control options, BP has determined that none of the technically feasible control options is BACT. BACT for this emission source would be no further control. BP proposes a BACT limit for VOC emissions from the #1 PTA Crystallizer Vent Scrubber of 46.5 tpy (13 lbs/hr) and #2 PTA Crystallizer Vent Scrubber of 46.5 tpy (13 lbs/hr) on a rolling 12-month sum. This limit would be monitored by a specialized performance test, using methodology negotiated with the agency, on this steam stream once every 5 years.

Best Available Control Technology Analysis for Volatile Organic Compound 4.5 **Emissions from Oxidation Unit Fugitives**

The OX Units equipment has fluids that contain VOCs which can have fugitive emissions from valves, flanges, drains, vents, pumps, relief valves and other equipment. The PTA Units do not have VOC-containing process streams.

Presently, the OX units have several LDAR programs to minimize the fugitive emissions. The LDAR programs include components subject to NSPS VV, HON and a program similar to NSPS VV. The estimated PTE emissions from the oxidation unit equipment fugitive points after the project with the present LDAR monitoring programs and before considering the impact of BACT is 193.1 tpy of VOC.

Identification of Control Technologies 4.5.1

The RBLC database was queried for emission sources and control devices of VOC that are used in the process type Equipment Leaks, Organic Chemical production. The search returned 12 facilities and 23 processes for BACT in this industrial category. The following control device was the only one identified from the search:

LDAR Program

Other resources of control technology were reviewed, such as EPA Air Pollution Control Technology Fact Sheets; EPA Air Pollution Control Cost Manual Sixth Edition, EPA/452/B-02-001, January 2002; and NSPS and NESHAPs standards. The results of this review did not find any additional control options applicable to this emission source.

A BACT analysis was performed for this option including an upgrade of the present LDAR program.

4.5.2 Elimination of Infeasible Control Options

The control options were evaluated qualitatively to determine if these options are technically feasible. An upgrade of the existing program for components subject to NSPS VV or a similar program to either an NSPS VVa or a HON LDAR program was determined to be technically feasible.

A detailed economic analysis of the different possible LDAR program upgrades has been performed and is summarized in the following subsections.

4.5.3 Ranking of Remaining Control Technologies

The potential effectiveness of the remaining control options has been evaluated by reviewing USEPA documents. The remaining control options and their associated anticipated effectiveness factors for a couple of different components are shown below as a comparison of relative efficiency:

CONTROL OPTION	LIQUID VALVE EFFECTIVENESS FACTOR (%)	LIGHT LIQUID PUMPS EFFECTIVENESS FACTOR (%)
HON MACT LDAR Program	88	75
NSPS VVa LDAR Program	88	71
LDAR VV Program (existing)	61	69

4.5.4 Evaluation of Most Effective Control Technologies and Selection of Best Available Control Technology

The BACT analysis is a three-part investigation that includes economic, energy, and environmental impacts. Each of the remaining options was reviewed with respect to the impacts to determine if they meet BACT requirements.

Economic Analysis

The economic analysis is composed of a calculation of the control technologies' ACE based on a comparison of the cost of each feasible control technology in terms of cost per mass of pollutant removed. In general, technologies with excessive costs per ton of pollutant removed are considered excessive in most cases and the installation of that technology would not be deemed economically feasible.

The ACE was determined by estimating the resulting annual operating and maintenance costs. The operating expenses were based on historical costs for the existing BP CR LDAR program. The ACE is estimated according to the following formula:

ACE = (Control Option Annualized Cost)/(Baseline emission rate - Control option emission rate)

The baseline emissions for the existing LDAR program for both #1 and #2 Units combined are estimated and reported as 193.1 tpy. This emission rate was used as the baseline emission rate for the BACT analysis. This emission rate is used to determine the ACE for the specific control option. Table 4-4 provides a

summary of the annualized cost, and the ACE values for each of the control options. The cost analysis information is provided in Appendix D, BACT Analysis Cost Information.

Table 4-4 **Fugitives VOC BACT Analysis**

CONTROL OPTION	EMISSION REDUCTION (tpy)	ANNUALIZED OPERATING COST (\$)	AVERAGE COST EFFECTIVENESS (\$/TON)
Upgrade NSPS VV to HON	146.0	\$72,600	\$497
Upgrade NSPS VV to VVa	46.4	59,640	1,285

Since the ACE value for each of the options is low per ton of VOC removed, these options are both economically feasible.

Energy Analysis

An energy impact analysis is used to identify if the technically feasible control options result in any significant or unusual energy penalties or benefits. The feasible control options have been evaluated and it has been determined that no unusual energy penalties or benefits exist beyond what was considered in the economic analysis described in the previous section.

Environmental Analysis

A review of the control options with respect to the environment was conducted to determine if any of the options created any adverse environmental impacts. The control options do not create any adverse environmental impacts.

4.5.5 Selection of Best Available Control Technology

Based on the energy, environmental and economic impacts associated with the technically feasible control options, BP has concluded that upgrading the existing LDAR program by considering all VOCs as HAPs and using the HON LDAR program for the applicable components would be BACT. BP CR will upgrade the LDAR program for the #1 and #2 units. These emissions will be monitored by the HON LDAR requirements and reported per the HON reporting to demonstrate compliance with BACT.

4.6 Best Available Control Technology Analysis for Carbon Monoxide Emissions from Low Pressure Absorbers

The OX Unit LPA is a recovery device for several process streams in the unit. The LPA recovers the acetic acid in the inlet streams and recycles it into the process so it eventually reaches the reactor system. This is a valuable material that acts as the solvent for the process and any loss from the LPA outlet must be replaced by purchase of fresh acetic acid. Part of the optimization of the manufacturing process is to minimize the loss of acetic acid. The CO is produced in the reactor by unwanted "acid burning" which causes the loss of the valuable acetic acid that must be replaced and the diversion of the oxygen from the desired reaction to produce TA. The LPA does not recover any of the CO which is a contaminant and diluent for the process and would adversely impact the process if recycled to the unit. This analysis will be based on add-on controls to the outlet of the LPA recovery device.

The PTE of CO emissions from the LPA will be about 18.0 tpy for #1 OX LPA and 15.2 tpy for #2 OX LPA. The LPA outlet stream will require a fan to raise the pressure sufficiently to allow the stream to go to a control device.

4.6.1 Identification of Control Technologies

The RBLC database was queried for emission sources and control devices of CO that are used in the process types 64.000, 64.003 and 64.999, SOCMI production. The results of the RBLC search are shown in Appendix C. The search returned seven facilities and nine processes for BACT in these industrial categories. The following control devices were identified from the search:

_	CTO	_	Good Combustion

In the RBLC, no control devices were found to apply directly to the PTA manufacturing process.

Other resources of control technology were reviewed, such as *EPA Air Pollution Control Technology Fact Sheets*; *EPA Air Pollution Control Cost Manual Sixth Edition*, EPA/452/B-02-001, January 2002; and NSPS and NESHAPs standards. The review indicated that control equipment is typically not employed to reduce CO emissions. The results of this review indicated that the following control equipment may be effective in the reduction of CO:

_	TO	_	RTO
_	RCO	_	Flare

4.6.2 Elimination of Infeasible Control Options

Seven control options were evaluated qualitatively to determine if these options are technically feasible. The following control technologies were determined to be technically feasible for control of CO:

- 1. TO
- 2. **RTO**
- 3. **RCO**
- **CTO** 4.

Since the OX LPA is not a combustion process, the good combustion practices control option is not feasible. The Flare is not a feasible option since the emissions factors for CO emissions from a flare in AP-42 (Table 13.5-1) would indicate that more CO would be created from the combustion of all the required supplemental natural gas than would be removed. A detailed economic analysis of the remaining technically feasible options has been performed and is summarized in the following subsections.

Ranking of Remaining Control Technologies 4.6.3

The potential effectiveness of the remaining control options has been evaluated by reviewing manufacturer information and USEPA documents. The remaining control options and their associated anticipated efficiencies are listed below:

CONTROL OPTION	EFFICIENCY (%)
то	95
СТО	95
RTO	95
RCO	95

4.6.4 Evaluation of Most Effective Control Technologies and Selection of Best Available Control Technology

The BACT analysis is a three-part investigation that includes economic, energy, and environmental impacts. Each of the remaining options was reviewed with respect to the impacts to determine if they meet BACT requirements.

Economic Analysis

The economic analysis is composed of a calculation of the control technologies' ACE based on a comparison of the cost of each feasible control technology in terms of cost per mass of pollutant removed. In general, technologies with excessive costs per ton of pollutant removed are considered excessive in most cases and the installation of that technology would not be deemed economically feasible.

The ACE was determined by estimating the capital cost for an installed system and the resulting annual operating and maintenance costs. The capital and operating expenses were obtained from using the *EPA Air Pollution Control Cost Manual Sixth Edition*, EPA/452/B-02-001 or *EPA's Air Pollution Control Fact Sheets*. The ACE is estimated according to the following formula:

ACE = (Control Option Annualized Cost)/(Baseline emission rate - Control option emission rate)

The baseline emissions from #1 OX LPA are estimated at 18.0 tpy. The #1 OX LPA emission rate was used as the baseline emission rate for the BACT analysis. This emission rate is used to determine the ACE for the specific control option. This would be the worst case since the #2 to #1 ratio of the flow rate impact on equipment costs would be about 92 percent and emission rate ratio would only be about 85 percent. As an example ACE calculation, assume the control efficiency of an option is 95 percent. The (baseline emission rate-control option emission rate) for each option is equal to {18.0 tpy – [18.0 tpy X (1-95%)]} or 17.1 tons on an annual basis. This emission rate is used to determine the ACE for the specific control option.

The ACE can be estimated from the above capital and annual operating costs by annualizing the capital cost (multiplying by a factor of 0.10 to simulate a 20-year equipment life and an 8 percent interest rate). This value is added to the annual operating cost and the sum is divided by the product of the control efficiency and the uncontrolled emission rate. Table 4-5 provides a summary of the annualized cost and ACE values for each of the control options. The cost analysis information is provided in Appendix D, BACT Analysis Cost Information.

Table 4-5 LPA CO BACT Analysis

CONTROL OPTION	EMISSION REDUCTION (tpy)	TOTAL CAPITAL COST (\$)	ANNUALIZED OPERATING COST (\$)	AVERAGE COST EFFECTIVENESS (\$/ton)	INCREASED ENERGY USAGE (\$/yr)	ADVERSE ENVIRONMENTAL IMPACTS?
ТО	17.1	\$1,070,756	\$478,978	\$28,010	\$249,127	Yes
СТО	17.1	1,464,014	394,328	23,060	100,324	Yes
RTO	17.1	1,179,994	365,915	21,399	105,751	Yes
RCO	17.1	1,660,644	518,557	30,325	110,983	Yes

Since the ACE value for the options are all very high per ton of CO removed, these are not economically feasible. The ACE values are compared to Georgia PSD applications for Johns Manville-Winder and Houston American Cement which indicated that ACE values of \$5,800-9,696 were not cost effective for CO control.

Energy Analysis

An energy impact analysis is used to identify if the technically feasible control options result in any significant or unusual energy penalties or benefits. The feasible control options have been evaluated and it has been determined that no unusual energy penalties exist beyond what was considered in the economic analysis described in the previous section. Each of the combustion options will require a substantial amount of increased fuel gas consumption. An analysis of energy benefits was also considered; the various options do not result in any energy benefit for the BP facility.

Environmental Analysis

A review of the control options with respect to the environment was conducted to determine if any of the options created any adverse environmental impacts. The TO, RTO, and RCO control options results in significant increases in energy usage from powering fans with electricity to heating the vent stream with natural gas. Thermal options (TO, RTO, and RCO) will also generate significant quantities of products of combustion such as CO and NOx that make these control options less environmentally beneficial. The proposed technically feasible options are not environmentally beneficial and in some cases create byproducts such as secondary air emissions.

4.6.5 Selection of Best Available Control Technology

Based on the energy, environmental, and economic impacts associated with the technically feasible control options, BP has concluded that the add-on control equipment options are not economically or environmentally feasible. The proposed BACT for CO emissions from the LPA is no further control. BP proposes a BACT limit for CO emissions from the #1 OX LPA of 18.0 tpy (5 lbs/hr) and #2 OX LPA of 15.2 tpy (5 lbs/hr) on a rolling 12-month sum. The LPA provides control for VOC emissions and monitoring has been proposed in Subsection 4.2. No monitoring will be proposed for LPA CO emissions. The LPA only controls VOC and HAPs emissions. Monitoring for VOC has been proposed in Subsection 4.2 as the existing CAM plans. It has no impact

on CO emissions since it does not control CO. Any monitoring of LPA will tell you nothing about the resulting CO emissions. If performance testing of the LPA CO emissions is required, the CO will be determined every 36 months in accordance with Method 10B.

4.7 Best Available Control Technology Analysis for Carbon Monoxide Emissions from High Pressure Absorbers

The OX reactor temperature is controlled by boiling off some of the liquid in the reactor. This vapor stream goes through several stages of condensing, with the condensed liquid being returned to the reactor, before the reactor overhead is sent to the recovery system. This recovery system consists of an acetic acid scrubber and then the HPA. This analysis will be based on the outlet of the HPA recovery device.

Presently the outlet of the HPA is sent to the HPVGTS where the pollutants (VOC, CO, and HAPs) are controlled in a catalytic oxidation reactor and a bromine scrubber before the stream is exhausted to either the inert gas system for use as a carrier gas for the conveying system or the expander for power recovery prior to being exhausted to the atmosphere. Any control option must include a bromine scrubber to comply with the Montreal Protocol agreement on methyl bromide emissions. The carrier gas for the conveying system must not contain over about 5 percent oxygen to avoid explosive conditions in silos with the PTA dust. Therefore, any thermal control system that requires additional air for the control option would have to provide an alternative inert carrier gas (*i.e.*, nitrogen).

The PTE CO emissions from the HPA will be 7,700 tpy for #1 OX HPA and 6,578 tpy for #2 OX HPA.

4.7.1 Identification of Control Technologies

The RBLC database was queried for emission sources and control devices of CO that are used in the process types 64.000, 64.003, and 64.999, SOCMI production. The results of the RBLC search are shown in Appendix C. The search returned seven facilities and nine processes for BACT in these industrial categories. The following control devices were identified from the search:

CTOGood Combustion

In the RBLC no control devices were found to apply directly to the PTA manufacturing process. The processes currently utilize a CTO as the add-on control device.

Other resources of control technology were reviewed, such as *EPA Air Pollution Control Technology Fact Sheets*; *EPA Air Pollution Control Cost Manual Sixth Edition*,

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EPA/452/B-02-001, January 2002; and the applicable NSPS and NESHAPs standards. The review indicated that control equipment is typically not employed to reduce CO emissions. The results of this review indicated that the following control equipment may be effective in the reduction of CO:

TO **RTO RCO Flare**

A BACT analysis was performed for each of the control equipment options. The processes currently utilize catalytic oxidation units and continued utilization of the existing abatement devices was determined to meet BACT for the processes. The other options were determined to be technically infeasible and/or economically infeasible to the control option selected.

4.7.2 Elimination of Infeasible Control Options

Seven control options were evaluated qualitatively to determine if these options are technically feasible. The following control technologies were determined to be technically feasible:

- 1. TO
- 2. **RTO**
- 3. **RCO**
- 4. CTO (existing HPVGTS)

Since the HPA is not a combustion process the good combustion practices control option is not feasible. The Flare is not a feasible option since the emissions factors for CO emissions from a flare in AP-42 (Table 13.5-1) would indicate that more CO would be created from the combustion of all the required supplemental natural gas than would be removed. A detailed economic analysis of the remaining technically feasible options has been performed and is summarized in the following subsections.

4.7.3 Ranking of Remaining Control Technologies

The potential effectiveness of the remaining control options has been evaluated by reviewing manufacturer information and USEPA documents. The remaining control options and their associated anticipated efficiencies are listed below:

CONTROL OPTION	EFFICIENCY (%)
TO/Bromine Scrubber	95
RTO/Bromine Scrubber	95
RCO/Bromine Scrubber	95
CTO (Existing HPVGTS with Bromine Scrubber)	95

4.7.4 Evaluation of Most Effective Control Technologies and Selection of Best Available Control Technology

The BACT analysis is a three-part investigation that includes economic, energy, and environmental impacts. Each of the remaining options was reviewed with respect to the impacts to determine if they meet BACT requirements.

Economic Analysis

The economic analysis is composed of a calculation of the control technologies' ACE based on a comparison of the cost of each feasible control technology in terms of cost per mass of pollutant removed. In general, technologies with excessive costs per ton of pollutant removed are considered excessive in most cases and the installation of that technology would not be deemed economically feasible.

The ACE was determined by estimating the capital cost for an installed system and the resulting annual operating and maintenance costs. The capital and operating expenses were obtained from using the EPA Air Pollution Control Cost Manual Sixth Edition, EPA/452/B-02-001 or EPA's Air Pollution Control Fact *Sheets.* The ACE is estimated according to the following formula:

ACE = (Control Option Annualized Cost)/(Baseline emission rate - Control option emission rate)

The #1 OX HPA baseline emissions are estimated at 7,700 tpy. This emission rate was used as the baseline emission rate for the BACT analysis. This emission rate is used to determine the ACE for the specific control option. The #1 OX emissions would give the worst case answer since the equipment cost ratio based on relative flow rates would be about 90 percent but the #2 emission rate is only about 85 percent. Therefore the ACE for the #2 OX case would be higher for a comparable control option.

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The ACE can be estimated from the above capital and annual operating costs by annualizing the capital cost (multiplying by a factor of 0.10 to simulate a 20-year equipment life and an 8 percent interest rate). This value is added to the annual operating cost and the sum is divided by the product of the control efficiency and the uncontrolled emission rate. Table 4-6 provides a summary of the annualized cost and ACE values for each of the control options. The cost analysis information is provided in Appendix D, BACT Analysis Cost Information.

The emission reduction in the above table includes the destruction of the CO in the inlet stream and the additional CO generated by the combustion of fuel. The ACE value for all the control options would be economically feasible per ton of pollutants removed but the CTO (existing HPVGTS with bromine scrubber) has the largest overall CO destruction and the lowest ACE. Also as shown previously for the VOC control, the CTO (existing HPVGTS) control option was the choice for BACT.

Hence looking at the emission reduction, ACE, and VOC BACT choice, the CTO (existing HPVGTS with bromine scrubber) would be BACT for CO.

Energy Analysis

An energy impact analysis is used to identify if the technically feasible control options result in any significant or unusual energy penalties or benefits. The feasible control options have been evaluated and it has been determined that no unusual energy penalties exist beyond what was considered in the economic analysis described in the previous section. An analysis of energy benefits was also considered; the various options do not result in any energy benefit for the BP facility.

Environmental Analysis

A review of the control options with respect to the environment was conducted to determine if any of the options created any adverse environmental impacts. The TO, RTO, and RCO control options results in significant increases in energy usage from powering fans with electricity to heating vent streams with natural gas. Thermal options (TO, RTO, and RCO) will also generate significant quantities of products of combustion such as GHG, CO, and NOx that make these control options less environmentally beneficial. The proposed technically feasible options are not environmentally beneficial and in some cases create byproducts such as secondary air emissions.

Table 4-6 HPA CO BACT Analysis

CONTROL OPTION	EMISSION REDUCTION (tpy)	TOTAL CAPITAL COST (\$)	ANNUALIZED OPERATING COST (\$)	AVERAGE COST EFFECTIVENESS (\$/ton)	INCREASED ENERGY USAGE (\$/yr)	ADVERSE ENVIRONMENTAL IMPACTS?
TO/Bromine Scrubber	7,160.6	\$2,512,704	\$29,543,821	\$4,126	11,306,341	Yes
RTO/Bromine Scrubber	7,288.6	5,530,255	20,485,522	2,697	1,002,328	Yes
RCO/Bromine Scrubber	7,231.6	3,331,993	29,079,323	3,857	5,563,302	Yes
CTO (Existing HPVGTS with Bromine Scrubber)	7,297.6	0	806,690	111	0	Yes

4.7.5 Selection of Best Available Control Technology

Based on the energy, environmental, and economic impacts associated with the technically feasible control options, BP has concluded that the CTO (existing HPVGTS with bromine scrubber) is the highest control efficiency option with the lowest cost per ton of control. Therefore the CTO (existing HPVGTS with bromine scrubber) control option meets the criteria for BACT. BP proposes a BACT limit for CO emissions from the #1 OX HPA of 385.0 tpy (106 lbs/hr) and #2 OX HPA of 329.0 tpy (90 lbs/hr) on a rolling 12-month sum. This process vent will be subject to the requirements for a CAM plan and will be monitored in accordance with the existing CAM plan. The details of the monitoring are listed in Subsection 2.5 of this application. If performance testing of the HPVGTS CO emissions is required, the CO will be determined every 36 months in accordance with Method 10B.

Section 5 Air Quality Analysis

5.1 Background

This project triggers PSD permitting requirements for CO and VOCs only. The project does not involve any new sources of CO but a re-distribution of emissions from one source to another. Modeling is only required for CO emissions. No air quality model exists that can evaluate the air quality impact of a point source of VOC emissions on area-wide ozone concentrations. The changes will allow the facility to operate in a more efficient manner. Because PSD permitting requirements have been triggered, air quality analyses are necessary for the proposed changes.

The project is located at the BP-Cooper River facility (see Figure 5-1). Figures 5-2 and 5-3 provide a representation of the facility's boundary and project source locations.

5.2 Modeling Protocol

A modeling protocol was submitted to SC DHEC for review on January 8, 2013. The following section summarizes the approach to the air quality modeling analysis. The air modeling information is included in Appendix G.

5.2.1 Model Selection

Air dispersion modeling was performed using the American Meteorological Society/ Environmental Protection Agency Regulatory Model AERMOD (AERMOD), Version 12345. AERMOD is the preferred model for areas within 50 Km of the source. AERMOD also includes the Plume Rise Model Enhancements (PRIME) algorithms for building downwash.

5.2.2 Information on Urban/Rural Characteristics

The site is located north of the City of Charleston in a predominantly rural area. The AERMOD model was utilized in its non-urban configuration.

5.2.3 Surrounding Terrain

The area surrounding the facility has only minor terrain relief. However following standard AERMOD guidelines, terrain elevations for grid receptors were included in the AERMOD modeling through use of the AERMAP terrain processor and applicable National Elevation Data (NED) files. NED files with NAD83 coordinates were used.

5.2.4 Good Engineering Practice Stack Heights and Building Downwash

No stack in the modeling analysis for this project meets the definition of formula GEP stack height so the BPIP PRIME computer algorithm was used to determine wind directionally dependent building dimensions for use in the AERMOD analysis. A BPIP input file for the facility is included in the modeling files submitted with this application.

5.2.5 Cavity Analysis

Cavities are eddies or areas of nearly stagnant air created on the leeward side of a building. The BP CR facility has the potential to produce cavity impacts. The AERMOD model, with building input data prepared using BPIPPRM algorithm, was used to directly evaluate cavity concentrations.

5.2.6 Meteorological Data

The meteorological data set used in this analysis is from the SC DHEC Website (files CHS-chs_0206_.SFC and CHS-chs_0206_.pfl). These data are from the Charleston meteorological station. Specifically for this project, SC DHEC has updated the meteorological data set with the use of the AERMET Version 12345 processer.

An assessment was made of the applicability of these meteorological data to a modeling analysis at BP CR. The BP CR site is located less than 10 miles from the Charleston airport (the meteorological observation station). The airport site and the BP CR site are both located about 15 miles from the Atlantic coast. There is only minor terrain relief in this part of South Carolina. The AERSURFACE algorithm was used to assess three basic parameters, albedo, Bowman Ratio, and roughness length on an annual basis for 12 wind sectors (results shown in Tables 5-1 and 5-2). The results in Tables 5-1 and 5-2 show that while there is some degree of similarity for albedo there are differences with Bowen Ratio and surface roughness values between the sites. These differences are typical however for comparing the surface characteristics an observation site at an airport with a site not at an airport. Given the relatively small predicted impacts in comparison to the significant impact levels and considering the proximity of the airport site to the project site, this meteorological data set is considered to be a reasonable choice for this analysis.

Table 5-1
Charleston Meteorological Site AURSURFACE Parameters

```
** Generated by AERSURFACE, dated 13016
** Generated from "southcarolina.bin"
** Center UTM Easting (meters):
                                 589718.0
** Center UTM Northing (meters):
                                 3640551.0
** UTM Zone:
                   Datum: NAD83
             17
** Study radius (km) for surface roughness:
** Airport? Y, Continuous snow cover? N
** Surface moisture? Average, Arid region? N
** Month/Season assignments? User-specified
** Late autumn after frost and harvest, or winter with no snow: 1,2
** Winter with continuous snow on the ground: 0
** Transitional spring (partial green coverage, short annuals): 3,4
** Midsummer with lush vegetation: 5,6,7,8,9
** Autumn with unharvested cropland: 10,11,12
  FREO SECT ANNUAL 12
  SECTOR
          1
               0
                    60
  SECTOR
               30
         3 60
                    90
  SECTOR
  SECTOR
          4
               90
                   120
  SECTOR 5 120
                   150
  SECTOR
           6 150
                   180
          7 180
                   210
  SECTOR
          8 210
  SECTOR
                   240
          9 240
                   270
  SECTOR
  SECTOR 10 270
                   300
  SECTOR 11
              300
                   330
  SECTOR 12 330
                   360
                     Sect
                             Alb
                                      Во
                                                Zo
                             0.16
                                      0.70
                                               0.039
  SITE_CHAR
               1
                       1
  SITE_CHAR
                       2
                             0.16
                                      0.70
               1
                                               0.050
  SITE CHAR
               1
                       3
                             0.16
                                      0.70
                                               0.054
               1
                       4
                                      0.70
                                               0.037
  SITE CHAR
                             0.16
  SITE CHAR
               1
                       5
                             0.16
                                      0.70
                                               0.029
  SITE_CHAR
               1
                       6
                             0.16
                                      0.70
                                               0.023
  SITE_CHAR
               1
                       7
                                      0.70
                                               0.023
                             0.16
                       8
  SITE_CHAR
               1
                             0.16
                                      0.70
                                               0.038
                       9
  SITE CHAR
               1
                             0.16
                                      0.70
                                               0.039
  SITE CHAR
                      10
                             0.16
                                      0.70
                                               0.042
               1
  SITE CHAR
               1
                      11
                             0.16
                                      0.70
                                               0.028
  SITE_CHAR
               1
                      12
                             0.16
                                     0.70
                                               0.022
```

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Table 5-2
BP Cooper River Site AURSURFACE Parameters

```
** Generated by AERSURFACE, dated 13016
** Generated from "southcarolina.bin"
** Center UTM Easting (meters):
                                  604442.0
** Center UTM Northing (meters):
                                 3648960.0
** UTM Zone:
                   Datum: NAD83
             17
** Study radius (km) for surface roughness:
** Airport? N, Continuous snow cover? N
** Surface moisture? Average, Arid region? N
** Month/Season assignments? User-specified
** Late autumn after frost and harvest, or winter with no snow: 1,2
** Winter with continuous snow on the ground: 0
** Transitional spring (partial green coverage, short annuals): 3,4
** Midsummer with lush vegetation: 5,6,7,8,9
** Autumn with unharvested cropland: 10,11,12
  FREO SECT ANNUAL 12
  SECTOR
          1
               Ω
                     30
                     60
  SECTOR
               30
               60
                    90
  SECTOR
          3
  SECTOR
          4
               90
                   120
  SECTOR
         5 120
                   150
  SECTOR
           6 150
                   180
          7 180
                    210
  SECTOR
          8 210
  SECTOR
                    240
          9 240
                   270
  SECTOR
  SECTOR 10 270
                   300
  SECTOR 11
              300
                   330
  SECTOR 12
              330
                   360
                     Sect
                             Alb
                                      Во
                                                 Zo
                              0.14
                                      0.33
                                                0.787
  SITE_CHAR
               1
                       1
  SITE_CHAR
                        2
                              0.14
                                      0.33
                                                0.777
               1
  SITE CHAR
               1
                       3
                              0.14
                                      0.33
                                                0.839
               1
                       4
                                      0.33
                                                0.855
  SITE CHAR
                              0.14
  SITE CHAR
               1
                       5
                              0.14
                                      0.33
                                                0.791
  SITE_CHAR
               1
                       6
                              0.14
                                      0.33
                                                0.420
  SITE_CHAR
               1
                       7
                              0.14
                                      0.33
                                                0.476
                       8
  SITE_CHAR
               1
                              0.14
                                      0.33
                                                0.520
                       9
  SITE CHAR
               1
                              0.14
                                      0.33
                                                0.351
  SITE CHAR
                      10
                              0.14
                                      0.33
                                                0.569
               1
  SITE_CHAR
               1
                      11
                              0.14
                                      0.33
                                                0.690
...SITE_CHAR
               1
                      12
                              0.14
                                      0.33
                                                0.753
```

TRC Environmental Corporation | BP Amoco Chemical Company - Cooper River Plant PSD Air Permit Application

5.2.7 Model Receptors

Receptors were placed along the fence at a spacing of 25 meters to 50 meters out to a distance to define the maximum predicted impacts as being within the interior of the grid. The maximum predicted impacts were on the facility boundary in an area of 25 to 50 meter spacing. Figure 5-4 contains a representation of the receptors used in the analysis.

5.2.8 Visibility Impairment Analysis

This project triggers PSD air quality evaluation requirements for CO and VOCs only. Neither of these pollutants is typically understood to affect visibility so no visibility impairment assessment is needed or was undertaken.

5.2.9 Toxic Air Pollutant Analysis

The facility is not subject to a South Carolina Standard No. 8 modeling evaluation because processes at the facility that emit Standard No. 8 pollutants are subject to MACT requirements which can be substituted to meet Standard No. 8 requirements.

5.3 Class I Area Impact Analysis

The responsible FLMs for the Cape Romain Class I area have been contacted and provided information concerning the proposed BP CR project. The land managers did not have any comments concerning the project.

As indicated earlier, this project triggers PSD requirements only for CO and VOCs only. Project net emission increases of nitrogen dioxide (NO₂), SO₂, and PM (PM₁₀ and PM_{2.5}) do not exceed PSD significance levels. The tools available for a visibility analysis (such as VISCREEN) do not include inputs for CO and VOC emissions, so it is assumed this project would have minimal impacts on visibility in the Class I area.

5.4 Significance Modeling Results for Carbon Monoxide

Project emissions of CO are summarized in Table 5-3. The basis for these emission estimates are presented in other parts of this application. Figure 5-3 shows the location of the project sources.

It should be noted that while Table 5-3 shows an offset emission source with a negative emission rate for #1 OX DHT Overhead Scrubber (BT-702). This source would have operated at that rate only sporadically. Consequently a separate source group was used that included only the four stacks with the positive emissions rates. These results are shown below. The initial modeling analysis showed the following worst-case impacts.

Table 5-3
Project Emission Sources with Parameters

MODEL ID	DESCRIPTION	X (m)	Y (m)	ELEV. (m)	PROJECT EMISSIONS (g/s)	PROJECT EMISSIONS (lb/hr)	STACK HEIGHT (m)	TEMP. (K)	VEL. (m/s)	DIAM. (m)
BT_702 ⁽¹⁾	DHT Overhead Scrubber	604491.1	3649074	10.02	-10.96	-87.0	10.67	305	21.3	0.304
BT_603	LPA	604628.1	3649119	8.67	0.517	4.1	21.5	322	3.4	0.762
HPVGTS-1	HPVGTS-1	604666.1	3649104	8.81	11.075	87.9	30.48	350	79.8	0.91
DT_302	LPA	604521.3	3648901	8.75	0.437	3.5	24.4	308	0.98	1.07
HPVGTS-2	HPVGTS-2	604642.3	3648896	8.92	9.45	75.0	41.46	333	29.87	1.3

⁽¹⁾ Source would historically operate at the listed emission rates only occasionally. An analysis was completed with all five sources operating and another with only the four stacks with the positive emission rates.

- n 1-hour CO Highest Predicted Impact 143 micrograms per cubic meter (μg/m³)
- n 8- hour CO Highest Predicted Impact 70 μg/m³

These predicted values are below the PSD significant impact thresholds of 2,000 μ g/m³ (1-hour) and 500 μ g/m³ (8-hours). Therefore, no further modeling analysis of emissions for Standard No. 2 is needed.

5.5 Preconstruction Monitoring Requirements

The worst case predicted concentrations are also below the Preconstruction Monitoring threshold of 575 μ g/m³.

No further analysis is therefore needed for CO for this project.

5.6 Analysis for Volatile Organic Compound Impact

No air quality model exists that can evaluate the air quality impact of a point source of VOC emissions on area-wide ozone concentrations. This project was evaluated using a project related net increase in VOC emissions of 72.6 tpy. The estimated increase in emissions of NOx is below the PSD significant emission increase threshold.

The area measured values of ozone in the Charleston area for the last 3 years are listed below.

- Bushy Park Monitor # 450150028-hour average 4^{th} high – 0.061 parts per million (ppm), 0.065 ppm, 0.066 ppm (2012, 2011, 2010)
- Cape Romain # 4501900468-hour average 4^{th} high -0.064 ppm, 0.066 ppm, 0.068 ppm (2012, 2011, 2010)

The National Ambient Air Quality Standard (NAAQS) for ozone is 0.075 ppm. The monitored values above show the area to be well in attainment of the 8-hour ozone NAAQS.

The VOC impact was based on the project having a relative small increase in VOC emissions of 72.4 tpy and less than 40 tpy of NOx emissions. Ozone concentrations in South Carolina have been shown to be limited by the presence of NOx. This project does not result in a significant increase in NOx emissions so it would be expected that the project as a whole would have minimal impact on area ozone concentrations.

To better assess the relative nature of the project increase in VOC emissions, average actual VOC emissions for the Charleston County and three other surrounding Counties are presented below.

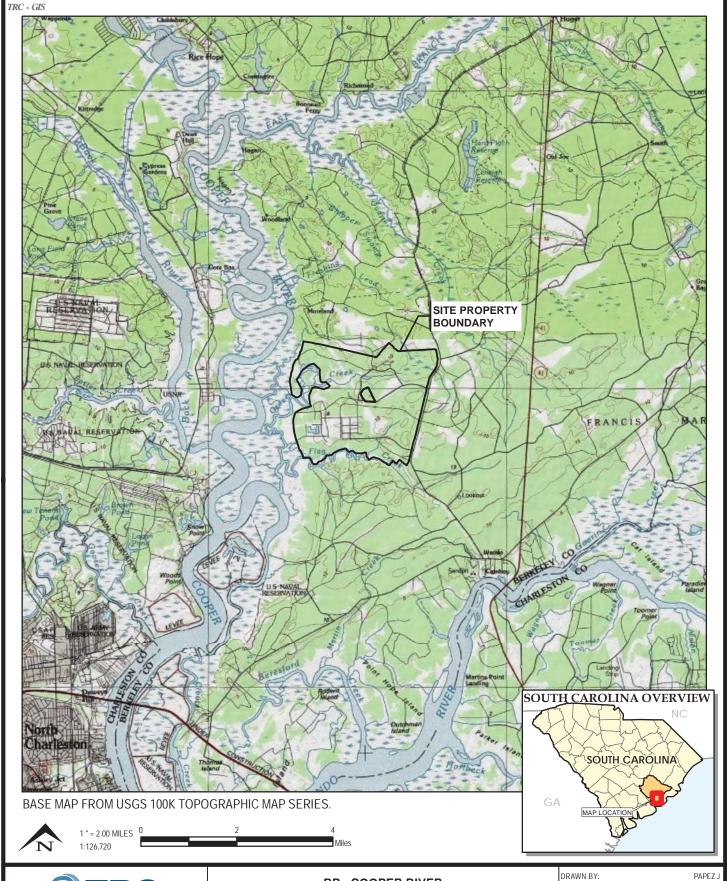
COUNTY	3-YEAR AVERAGE ACTUAL VOC EMISSIONS (tpy)
Charleston	1,430
Berkeley	1,625
Dorchester	470
Colleton	857
Total for Area	4,382

The project VOC emissions impact was based on an estimated VOC emissions increase of 72.6 tpy from this project. This value represents 1.7 percent of the actual area-wide point source emissions of VOCs. Note that this total does not include mobile sources or emissions from minor sources in the area.

Because project emission level increases for VOCs for this project are relatively small and the project does not have a significant increase in NOx emissions (recall the area is NOx limited with respect to the formation of ozone), it is concluded this project would not cause area-wide ozone concentrations to increase significantly.

5.7 Preconstruction Monitoring for Ozone

The project emissions of VOCs do not exceed the monitoring *de minimis* threshold of 100 tpy of VOC emissions. Consequently no preconstruction monitoring of ozone is needed for the project.





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FIGURE 5-1 SITE LOCATION MAP

DRAWN BY:	PAPEZ J
APPROVED BY:	FOX D
PROJECT NO:	187464
FILE NO.	187464-003slm.mxd
DATE:	JANUARY 2013

LEGEND

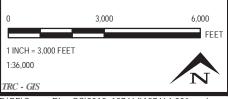


APPROXIMATE FACILITY BOUNDARY

NOTES

. BASE MAP IMAGERY FROM ESRI WEB SERVICE BASEMAP LAYER, "WORLD IMAGERY".





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BP COOPER RIVER SOUTH CAROLINA

FIGURE 5-2 SITE MAP - FACILITY BOUNDARY

DRAWN BY:	PAPEZ J
APPROVED BY:	FOX D
PROJ. NO.:	187464
FILE NO.:	187464-001.mxd
DATE:	JANUARY 2013

LEGEND



APPROXIMATE FACILITY BOUNDARY

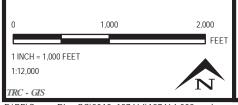
9

STACK LOCATION

NOTES

. BASE MAP IMAGERY FROM ESRI WEB SERVICE BASEMAP LAYER, "WORLD IMAGERY".





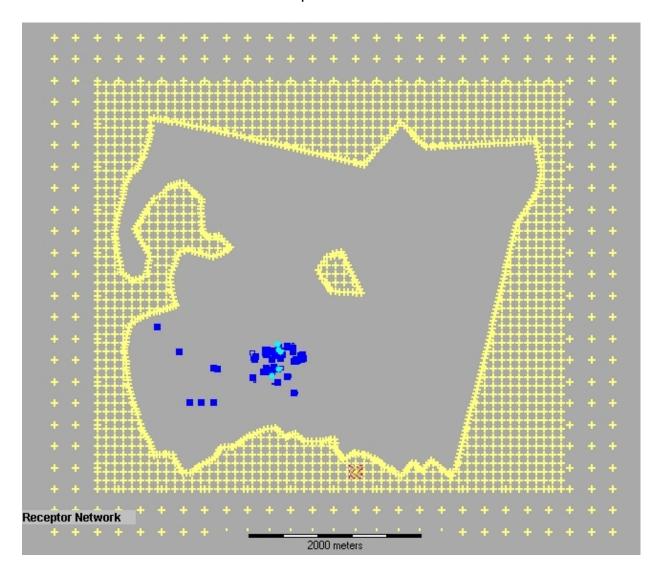
CTRC

708 Heartland Trail, Suite 3000 Madison, WI 53717 Phone: 608.826.3600 www.trcsolutions.com BP COOPER RIVER SOUTH CAROLINA

FIGURE 5-3
PROJECT EMISSION SOURCES

DRAWN BY:	PAPEZ J
APPROVED BY:	FOX D
PROJ. NO.:	187464
FILE NO.:	187464-002.mxd
DATE:	JANUARY 2013

Figure 5-4 Receptor Network



Section 6 **Additional Impacts Analyses**

The provisions of South Carolina Regulation 62.5, Standard No. 7 require that additional environmental impact analyses be performed to determine the impairment to visibility, soil, and vegetation that would occur as a result of construction and operation of a major source or a modification to a major source. These regulatory provisions also require that analyses be performed to determine the general commercial, residential, industrial, and other growth associated with operation of a major source or modification, as well as the air quality impact projected for the area as a result of such growth.

6.1 Visibility/Regional Haze

As indicated earlier in this report, the project is projected to have insignificant impact on regional visibility or haze due to the fact that the project triggers PSD requirements only for CO and VOCs. Neither pollutant is a variable that is input in models to determine visibility impacts (such as in the VISCREEN algorithm).

6.2 Associated Growth Impacts

The proposed modification at the BP CR facility is not anticipated to result in any significant increase in full-time employment (an associated increase in traffic flow) at the facility. The construction activity related to the project may allow for a temporary increase in local traffic due to construction related jobs and associated traffic.

6.3 Impacts on Soil and Vegetation

CO at the insignificant predicted levels of concentration for this project do not have any known effects on soils or vegetation. VOC emissions from the project are not projected to have any significant effect on local ozone concentrations. Consequently, no effects on soils or vegetation would be expected from the project.

Section 7 Title V Permit Revisions for PSD Application

The implementation of the requested permit limits will require the revision of some of the permit condition contained in the existing Title V permit. Many of these revisions have been requested in the Title V permit renewal application submitted in January 2012. However, there are some additional Title V permit revisions that will become necessary due to this permit application. The following are some examples of the necessary Title V permit revisions:

- Recognition that the two boilers are gas-fired units rather than oil fired
- Revision of the oil and emissions limits on the boilers
- Revision of 40 CFR 63 Subpart DDDDD and 40 CFR 60 Subpart Db requirements for boilers since gas-fired
- Existing emissions limits for VOC and CO in the OX and PTA units to be replaced with the new BACT emission limits
- Removal of emission points from permit where equipment and emissions are being removed from the process
- Removal of #2 OX requirements for a Group 1 HON process vent since all are now Group 2 vents.

The following existing specific emissions limits in Table 7-1 will be replaced by the BACT limits or revised due to regulatory status changes in the application:

Table 7-1 **Emission Limits**

UNIT ID	POLLUTANT	LIMIT	UNIT ID	POLLUTANT	LIMIT
03 (#1 HPVGTS)	СО	1,452 lb/hr	03 (BT-702)	VOC	60 lb/hr
03 (#1 HPVGTS)	СО	375 tpy	03 (BT-702)	VOC	165 tpy
03 (#1 HPVGTS)	VOC	85 lb/hr	03-06	VOC	1825 tpy
03 (#1 HPVGTS)	VOC	80 tpy	03-06 (HPVGT)	DRE	95%
03 (#1 LPA)	СО	40 tpy	05-06	VOC	49.3 lb/hr
03 (#1 LPA)	VOC	40 lb/hr	05-06	VOC	215.9 tpy
03 (#1 LPA)	VOC	80 tpy	15-16 Boilers	СО	400 ppm
03 (BT-702)	СО	380 tpy	15-16 Boilers	Oil use	18.675 MM gal

e Title V permit mark-up that was included in the Title V renewal is included in Appendix E. e Title V mark-up has the revisions necessary for this PSD application indicated with yellow ghlighting.	

Appendix A SC DHEC Permit Application Forms



Bureau of Air Quality Expedited Review Request Construction Permits Page 1 of 1

BAQ Use: Recv'd By:

To be eligible for expedited review, the appropriate Construction Permit Application Forms must be included with this sheet.

	FACILITY II	DENTIFICATION		
Facility 1	Name: BP AMOCO Chemical Company - Cooper River			
Applicat	ion Date: 4/09/2013 - Revised 3/04/2014	SC Air Permit Number (8-digits only)): 0420 - 0029	
T'(1 /D		PERMIT CONTACT		
	sition: Environmental Engineer Salutation: Mr		t Name: Pace	
E-mail A	Address: Brent.Pace@bp.com	Phone No.: 843.881.5182 Cell	No.: 419.303.	.3987
	SECONDARY AIR	R PERMIT CONTACT		
	(If the Department is unable to contact the primary	air permit contact please provided a seco	ondary contact)
Title/Pos	sition: HSSE Manager Salutation: Ms		Name: Lessli	
E-mail A	Address: Judith.Lesslie@bp.com		No.: 843.870.	
GI. I		*		
Check One	Permit	Гуре		Fee*
	Minor Source Construction Permit			\$3,000
	Synthetic Minor Construction Permit			\$4,000
	Prevention of Significant Deterioration (PSD) not impa	cting a Class I Area (no Class I modeling	g required)	\$20,000
	Prevention of Significant Deterioration (PSD) impacting	g a Class I Area (Class I modeling requi	red)	\$25,000
	General Pe	rmit Program		
	Minor Source Construction Permit / Relocation Reques	t (Concrete)		\$1,500
	Minor Source Construction Permit / Relocation Reques	t (Asphalt)		\$2,000
	Synthetic Minor Source Construction Permit / Relocation	on Request (Concrete)		\$3,000
* DO NO	Synthetic Minor Source Construction Permit / Relocation	on Request (Asphalt)		\$3,500
* DO NO	T send fee payment with this form. If chosen for exped am. Fees must be paid within five business days of accep	ited review, you will be notified by phor	ne for verbal a	cceptance into
the progra	and rees must be paid within five business days of accep	tance.		
	PRIMARY AIR PERMIT	T CONTACT SIGNATURE		
I have re	ead the Expedited Review Program Standard Operating	Procedures and accept all of the term	ns and condit	ions within I
understan	id that it is my responsibility to ensure an application of	the highest quality is submitted in a tin	nely manner a	and to address
any reque	ests for additional information by the deadline specified	. I understand that submittal of this requ	uest form is no	ot a guarantee
that expe	dited review will be granted.			ar a guarantee
	. 0			
15.	terare	3/10	0/14	
	of Primary Air Permit Contact	Date	Carlon II	
		Date	P.	



1. SC Air Permit Number (8-digits only): 0420 - 0029

Bureau of Air Quality Construction Permit Application Facility Information Page 1 of 2

A. FACILITY INFORMATION

BAQ Use: CP ID: Recv'd By:

2. Application Date: 4/09/2013- Revised 03/04/2014

3. Facility Name: BP Amoco Chemical Company - Cooper River	r 4. Facility Federal Tax Identification No.: SCD084703909				
Plant 5. Physical Address 1206 America Dr.					
5. Physical Address: 1306 Amoco Dr.	ggg	6. County: Berkeley			
7. City: Wando	State: SC	8. Zip Code: 29492			
	Coordinates	Etho fooility			
Facility coordinates should be based at the Latitude: 604725.47E Longitude: 3648659.	·				
Latitude: 604725.47E Longitude: 3648659.	IAN NA	D27 Of NAD83			
B. COMPANY	NFORMATION				
1. Company Name: BP Amoco Chemical Company - Cooper Rive					
2. Mailing Address: 1306 Amoco Dr.		1			
3. City: Wando	4. State: SC	5. Zip Code: 29492			
or early manage		[0. Exp 0.000. 2) 1) 2			
C. CO-LOCATION	DETERMINATION				
Are there other facilities in close proximity that could be considered	ed co-located? No Yes*	**			
List potential co-located facilities, including air permit numbers if	applicable:				
If applicable, location in application for co-location determination:					
(**If yes, please submit co-location applicability determine		to this application.)			
		,			
	NFORMATION / DATA				
Does this application contain confidential information or data?	No X Yes***				
(***If yes, include a sanitized version of the application f	or public review.)				
E. COMMUNI	TY OUTREACH				
What are the potential air issues and community concern Based of		nodeling attached to this application.			
there are no potential air issues / community concerns from this pr		,			
	•				
F. FACILITY'S PRO	DUCTS / SERVICES				
1. Primary Products / Services: Purified Terephthalic Acid (PTA)					
2. Primary SIC Code: 2869	3. Primary NAICS Code: 325	199			
4. Other Products / Services:					
5. Other SIC Code(s):	6. Other NAICS Code(s):				
	IT CONTACT				
(Person who can answer questions about					
Title/Position: Environmental Engineer Salutation: Mr.	First Name: Brent	Last Name: Pace			
Mailing Address: 1306 Amoco Dr.		_			
City: Wando	State: SC	Zip Code: 29492			
E-mail Address: Brent.Pace@bp.com	Phone No.: 843.881.5182	Cell No.: 419.303.3987			
The signed permit will be mailed to the Air Permit Contact listed above unless o postal service. Additional copies can be sent electronically. Please indicate					
Name		ail Address			
Michael Doerner		trcsolutions.com			



Bureau of Air Quality Construction Permit Application Facility Information Page 2 of 2

	H. OWNER O	R OPERATOR	
Title/Position: Plant Manager	Salutation: Mr.	First Name: Mark	Last Name: Fitts
Mailing Address: 1306 Amoco Dr.			
City: Wando	,	State: SC	Zip Code: 29492
E-mail Address: mark.fitts@bp.com		Phone No.: 843.881.5201	Cell No.:
		ATOR SIGNATURE	
I certify, to the best of my knowledge and bel	ief, that no applical	ble standards and/or regulations v	will be contravened or violated. I
certify that any application form, report, or	compliance certific	cation submitted in this permit a	application is true, accurate, and
complete based on information and belief for	med after reasonab	ole inquiry. I understand that an	y statements and/or descriptions,
which are found to be incorrect, may result in t	he immediate revoc	ation of any permit issued for this	s application.
M E 2 d	1	3/	holzo14
Signature of Owner or Operator		/	Date
	I AID DEDMIT	CONSULTANT	·
(If not		the Professional Engineer.)	
Consulting Firm Name: TRC Environmental C		the Frotessional Engineer.)	
	Salutation: Mr.	First Name: Michael	Last Name: Doerner
Mailing Address: 30 Patewood Dr. Suite 300	Suraturom 1111	That I tames is included	East Hame. Boomer
City: Greenville		State: SC	Zip Code: 29615
E-mail Address: mdoerner@trcsolutions.com		Phone No.: 864.234.9481	Cell No.: 864.884.2683
<u></u>			
J. PRO	FESSIONAL ENG	GINEER INFORMATION	
Consulting Firm Name: TRC Environmental C			
	Salutation: Mr.	First Name: Robert	Last Name: vandenMeiracker
Mailing Address: 30 Patewood Dr. Suite 300			
City: Greenville		State: SC	Zip Code: 29615
E-mail Address: RVandenMeiracker@trcsoluti	ons.com	Phone No.: 864.234.9177	Cell No.: 864.787.5261
SC License/Registration No.: 28265			
	K. LIST OF FOI	RMS INCLUDED	
Form Name			ed (Y/N)
Equipment/Processes (DHEC Form	n 2567)		Yes
Control Devices (DHEC Form 2	568)		s 🗌 No
,		If No; Exp	
Emissions (DHEC Form 2569			Yes
Regulatory Review (DHEC Form	2570)		Yes
Modeling Information (DHEC Form	n 2573)		s No
Expedited Review Request (DHEC Fo	orm 2212)	If No, Exp	
Expedited Review Request (DTEC 14	51111 2212)		S L NO
IPR	OFFSSIONAL EN	NGINEER SIGNATURE	
I have placed my signature and seal on the cape application as it pertains to the requirements of NO. 2820 Signature of Professional Engineer.	Stuff Carolina Reg	submitted, signifying that I have gulation 61-62, Air Pollution Con	reviewed this construction permit trol Regulations and Standards.
11/1/1/1/1/1/1/1/1/1/1/1/1/1/1/1/1/1/1/1	11111		



Bureau of Air Quality Construction Permit Application Equipment/Processes Page 1 of 3

A. APPLICATION IDENTIFICATION

1. Facility Name: BP Amoco Chemical Company - Cooper River Plant

2. SC Air Permit Number (8-digits only): 0420 - 0029 3. Application Date: 4/09/2013 – Revised 03/04/2014

B. PROJECT DESCRIPTION

Brief Project Description (What, why, how, etc.): #1 and #2 OX units: These units produce Terephthalic Acid (TA) by the air oxidation of p-Xylene (PX) in a acetic acid (HAC) solvent. The TA solid product is crystallized from the solvent, filtered, dried and sent to intermediate storage silos. A more complete description is included in sections 1 and 2 of the application.

C. ATTACHMENTS						
 Process Flow Diagram Location in Application: Located in Section 2 of the application 						
3. Detailed Project Description	4. Location in Application: Located in Section 1 and 2 of the application					

	D. EQUIPMENT / PROCESS INFORMATION											
1. Equipment ID / Process ID	2. Action	3. Equipment / Process Description	4. Maximum Design Capacity (Units)	5. Fuels Combusted	6. Control Device ID(s)	7. Emission Point ID(s)	8. Raw Material(s)	9. Product(s)	10. Pollutant(s)/ Parameter(s) Monitored	11. Monitoring Frequency	12. Reporting Frequency	13. Monitoring / Reporting Basis
#1 OX		Oxidation Unit	Confidential				PX/Air	TA				
BR-301A	R	Reactor*		N/A	#1 HPVGTS	O- 2/10/15	N/A	N/A				
BR-301B	R	Reactor*		N/A	#1 HPVGTS	O- 2/10/15	N/A	N/A				
BR-301C	R	Reactor*		N/A	#1 HPVGTS	O- 2/10/15	N/A	N/A				
BR-301D	R	Reactor*		N/A	#1 HPVGTS	O- 2/10/15	N/A	N/A				
BT-605	R	Solvent Stripper		N/A	N/A	N/A	N/A	N/A				
BM-606	R	Residue Evaporator		N/A	N/A	N/A	N/A	N/A				
BD-625	R	CRU- Extraction Drum		N/A	N/A	O-11	N/A	N/A				
BD-631	R	CRU - ML Drum		N/A	N/A	O-12	N/A	N/A				
BD-632	R	CRU-Solid Reslurry Drum		N/A	N/A	O-13	N/A	N/A				
BE-645	R	CRU - Condenser		N/A	N/A	O-16	N/A	N/A				
BC-710	R	LPVGT		N/A	N/A	N/A	N/A	N/A				
BR-301	N	Reactor*		N/A	#1 HPVGTS	O- 2/10/15	N/A	N/A	N/A	 	N/A	N/A
BT-701	M	Dehydration Tower		N/A	N/A	O-3	N/A	N/A	HON MACT	HON MACT	HON MACT	HON MACT



Bureau of Air Quality Construction Permit Application Equipment/Processes Page 2 of 3

	D. EQUIPMENT / PROCESS INFORMATION												
1. Equipment ID / Process ID	2. Action	3. Equipment / Process Description	4. Maximum Design Capacity (Units)	5. Fuels Combusted	6. Control Device ID(s)	7. Emission Point ID(s)	8. Raw Material(s)	9. Product(s)	10. Pollutant(s)/ Parameter(s) Monitored	11. Monitoring Frequency	12. Reporting Frequency	13. Monitoring / Reporting Basis	
BD-401	M	1 st Crystallizer		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
BT-603	M	Low Pressure Absorber		N/A	N/A	O-3	N/A	N/A	HON MACT	HON MACT	HON MACT	HON MACT	
BC-104	M	Power Recovery Expander		N/A	N/A	O- 2/10/15	N/A	N/A	N/A	N/A	N/A	N/A	
BD-200	N	PX Feed Drum		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
BC-906	N	60# Steam Generator**	Confidential	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
BT-400	M	PX Scrubber		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
BT-401	M	HP Absorber		N/A	#1 HPVGTS	O- 2/10/15	N/A	N/A	HON MACT	HON MACT	HON MACT	HON MACT	
BD-604	M	Azeo Storage Drum		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
BT-700	N	Liquid-Liquid Extraction Tower		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
BM-1107	N	ROG Chiller		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
BF-1405	N	NBA Storage Tank		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
BT-750	N	Entrainer Recovery Tower		N/A	N/A	O-3	N/A	N/A	N/A	N/A	N/A	N/A	
BD-204	M	Feed Mix Drum		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
BD-503	M	Filter Vacuum Sep. Drum		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
BM- 1101A/B	M	Off-Gas Dryer		N/A	N/A	O- 2/10/15	N/A	N/A	N/A	N/A	N/A	N/A	
BM- 1101C/D	M	Off-Gas Dryer		N/A	N/A	O- 2/10/15	N/A	N/A	N/A	N/A	N/A	N/A	
#2 OX		Oxidation Unit	Confidential	NG			PX/Air	TA					
DC-710	R	LPVGT		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
DT-402	R	Solvent Stripper		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
DM-403	R	Residue Evaporator		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
DD-412	R	CRU Extraction Drum		N/A	N/A	O2-6	N/A	N/A	N/A	N/A	N/A	N/A	
DD-413	R	CRU Slurry Drum		N/A	N/A	O2-7	N/A	N/A	N/A	N/A	N/A	N/A	
DD-414	R	CRU ML Drum		N/A	N/A	O2-8	N/A	N/A	N/A	N/A	N/A	N/A	
DE-416	R	CRU Evap OH Condenser		N/A	N/A	O2-9	N/A	N/A	N/A	N/A	N/A	N/A	
DT-404	R	PX Stripper		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A		



Bureau of Air Quality Construction Permit Application Equipment/Processes Page 3 of 3

	D. EQUIPMENT / PROCESS INFORMATION											
1. Equipment ID / Process ID	2. Action	3. Equipment / Process Description	4. Maximum Design Capacity (Units)	5. Fuels Combusted	6. Control Device ID(s)	7. Emission Point ID(s)	8. Raw Material(s)	9. Product(s)	10. Pollutant(s)/ Parameter(s) Monitored	11. Monitoring Frequency	12. Reporting Frequency	13. Monitoring / Reporting Basis
DT-403	M	Dehydration Tower		N/A	N/A	O2-1	N/A	N/A	HON MACT	HON MACT	HON MACT	HON MACT
DT-302	M	Low Pressure Absorber		N/A	N/A	O2-1	N/A	N/A	HON MACT	HON MACT	HON MACT	HON MACT
DC-104	M	Power Recovery Expander		N/A	N/A	O2-3/4	N/A	N/A	N/A	N/A	N/A	N/A
DD-402	M	Azeo Storage Drum		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
DT-400	N	Liquid-Liquid Extraction Tower		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
DT-404	N	DHT Scrubber		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
DF-460	N	NBA Storage Tank		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
DT-450	N	Entrainer Recovery Tower		N/A	N/A	O2-1	N/A	N/A	N/A	N/A	N/A	N/A
DC-906	N	60# Steam Generator**	Confidential	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
NOTES												
*		Reactor includes overhea						_		_		
**		60# Steam Generator will	only provide po	wer for inte	ernal use.							



Bureau of Air Quality Construction Permit Application Equipment/Processes Page 1 of 1

A. APPLICATION IDENTIFICATION

1. Facility Name: BP Amoco Chemical Company - Cooper River Plant

2. SC Air Permit Number (8-digits only): 0420 - 0029 3. Application Date: 4/09/2013 - Revised 3/04/2014

B. PROJECT DESCRIPTION

Brief Project Description (What, why, how, etc.): #1 and #2 PTA units: These units produce Purified Terephthalic Acid (PTA) by the hydrogenation of the TA in a water slurry to change the impurities into a compound that can be separated from the TA to improve its purity. The PTA product is separated from the impurities, dried and sent to storage silos. A more complete description is included in sections 1 and 2 of the application.

C. ATTACHMENTS								
1. Process Flow Diagram	2. Location in Application: Located in Section 2 of the application							
3. Detailed Project Description	4. Location in Application: Located in Section 1 and 2 of the application							

	D. EQUIPMENT / PROCESS INFORMATION											
1. Equipment ID / Process ID	2. Action	3. Equipment / Process Description	4. Maximum Design Capacity (Units)	5. Fuels Combusted	6. Control Device ID(s)	7. Emission Point ID(s)	8. Raw Material(s)	9. Product(s)	10. Pollutant(s)/ Parameter(s) Monitored	11. Monitoring Frequency	12. Reporting Frequency	13. Monitoring / Reporting Basis
#1 PTA		PTA Unit	Confidential	N/A			TA/H2	PTA				
CM-301	M	Crystallizer Vent Scrubber		N/A	N/A	P-2	N/A	N/A	PM/ Pressure	Daily	Semiannual	CAM Plan
CD-304	N	Crystallizer		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
#2 PTA		PTA Unit	Confidential	N/A			TA/H2	PTA				
DM-601	M	Crystallizer Vent Scrubber		N/A	N/A	P2-2	N/A	N/A	PM/Flow	Continuous	Semiannaul	CAM Plan



Bureau of Air Quality Construction Permit Application Control Devices Page 1 of 1

A. APPLICATION IDENTIFICATION

1. Facility Name: BP Amoco Chemical Company - Cooper River Plant

2. SC Air Permit Number (8-digits only): 0420 - 0029 3. Application Date: 4/09/2013 - Revised 3/04/2014

	B. CONTROL DEVICE INFORMATION												
1. Control Device ID	2. Action	3. Pollutants Controlled (Include CAS#)	4. Control Device Description	5. Maximum Design Capacity (Units)	6. Fuels Combusted	7. Inherent/ Required/ Voluntary (Explain)	8. Capture System Efficiency and Description	9. Destruction/ Removal Efficiency Determination	10. Pollutant(s)/ Parameter(s) Monitored	11. Averaging Period(s)	12. Monitoring Frequency	13. Reporting Frequency	14. Monitoring/ Reporting Basis
CD – BE-645	R	VOC	Condenser	N/A	N/A								
CD – CM-301	M	PM	Venturi Scrubber	N/A	N/A	R	100-Hard Piped	95-Stack Test	Pressure	N/A	Daily	Semiannual	Per CAM Plan
CD – DE-416	R	VOC	Condenser	N/A	N/A								
CD – DM-601	M	PM	Venturi Scrubber	N/A	N/A	R	100-Hard Piped	95-Stack Test	Flow	N/A	Continuous	Semiannual	Per CAM Plan
CD -													
CD -													
CD -													
CD -													
CD -													
CD -													



Bureau of Air Quality Construction Permit Application Emissions Page 1 of 6

A. APPLICATION IDENTIFICATION									
1. Facility Name: BP Amoco Chemical Company - Cooper River Plant									
2. SC Air Permit Number (8-digits only): 0420 - 0029	3. Application Date: 4/09/2013-Revised 03/04/2014								
В	. ATTACHMENTS								
1. Sample Calculations, Emission Factors Used, etc.	2. Detailed Explanation of Assumptions, Bottlenecks, etc.								
3. Supporting Information: Manufacturer's Data, etc.	4. Source Test Information								
5. Details on Limits Being Taken for Limited Emissions	6. NSR Analysis								

C. SUMMARY OF PROJECT	C. SUMMARY OF PROJECTED CHANGE IN FACILITY WIDE POTENTIAL EMISSIONS										
(C	alculated at maxim	um design capaci	ty.)								
	2. E r	nission Rates Pri	or to	3. Emission Rates After							
1. Pollutants	Construction	on / Modification	(tons/year)	Construction	on / Modification	(tons/year)					
	Uncontrolled	Controlled	Limited	Uncontrolled	Controlled	Limited					
Particulate Matter (PM)	5,617.2	81.8		5,396.9	77.1						
Particulate Matter <10 Microns (PM ₁₀)	5,589.7	78.0		5,359.0	73.0						
Particulate Matter <2.5 Microns (PM _{2.5})	5,522.7	73.8		5,264.4	67.9						
Sulfur Dioxide (SO ₂)	193.8	189.1		193.8	189.1						
Nitrogen Oxides (NO _x)	475.9	324.6		475.9	324.6						
Carbon Monoxide (CO)	17,113.9	2,533.8		14,619.4	1,040.3						
Volatile Organic Compounds (VOC)	2,485.2	757.0		2,479.5	490.2						
Lead (Pb)	1.0	1.0		1.0	1.0						
Greenhouse Gases (Mass Basis)	487,767	512,580		482,000	479,586						
Greenhouse Gases (CO ₂ e Basis)	488,196	513,031		482,424	480,008						
Highest HAP Prior to Construction (CAS #: 106-42-3)	430.8	47.3									
Highest HAP After Construction (CAS #: 106-42-3)				227.9	58.5						
Total HAP Emissions*	2,548.4	279.8		1688.1	128.6						

(*All HAP emitted from the various equipment or processes must be listed in the appropriate "Table D. Potential Emission Rates at Maximum Design Capacity.")



Bureau of Air Quality Construction Permit Application Emissions Page 2 of 6

	D. POTENTIAL EMISSION RATES AT MAXIMUM DESIGN CAPACITY											
1. Equipment	2. Emission	3. Pollutants	4. Calculation Methods / Limits Taken /	5. Unco	ntrolled	6. Con	trolled	7. Li i	mited			
ID / Process ID	Point ID	(Include CAS #.)	Other Comments	lbs/hr	tons/yr	lbs/hr	tons/yr	lbs/hr	tons/yr			
BM-1201	O-17	NO _X 11104-93-1	See Appendix B	10.4	0.5	10.4	0.5					
BM-1201	O-17	VOC	See Appendix B	0.8	0.0	0.8	0.0					
BM-1201	O-17	CO 630-08-0	See Appendix B	2.2	0.1	2.2	0.1					
BM-1201	O-17	SO ₂ 7446-09-5	See Appendix B	0.7	0.0	0.7	0.0					
BM-1201	O-17	PM	See Appendix B	0.7	0.0	0.7	0.0					
BM-1201	O-17	PM ₁₀	See Appendix B	0.7	0.0	0.7	0.0					
BM-1201	O-17	PM _{2.5}	See Appendix B	0.7	0.0	0.7	0.0					
BM-1201	O-17	CO ₂ e 124-38-9	See Appendix B	137.6	6.9	137.6	6.9					
#1 HPVGTS	O-2/10/15	VOC	See Appendix B	234	1025	4.7	20.5					
#1 HPVGTS	O-2/10/15	CO 630-08-0	See Appendix B	1758	7700	87.9	385.0					
#1 HPVGTS	O-2/10/15	CO ₂ e 124-38-9	See Appendix B	9521	41,700	9521	41,700					
BT-603	O-3	VOC	See Appendix B	9.6	42.0	9.6	42.0					
BT-603	O-3	CO 630-08-0	See Appendix B	4.1	18.0	4.1	18.0					
BT-603	O-3	CO ₂ e 124-38-9	See Appendix B	283.0	1240	283.0	1240					
BT-501	O-22	PM	See Appendix B	75	330	1.50	6.6					
BT-501	O-22	PM_{10}	See Appendix B	75	330	1.50	6.6					
BT-501	O-22	PM _{2.5}	See Appendix B	75	330	1.50	6.6					
#1 OX Fugitives	N/A	p-Xylene 106-42-3	See Appendix B	1.9	8.1	0.20	0.9					

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Bureau of Air Quality Construction Permit Application Emissions Page 3 of 6

	D. POTENTIAL EMISSION RATES AT MAXIMUM DESIGN CAPACITY											
1. Equipment	2. Emission	3. Pollutants	4. Calculation Methods / Limits Taken /		ntrolled		trolled	7. Li i	mited			
ID / Process ID	Point ID	(Include CAS #.)	Other Comments	lbs/hr	tons/yr	lbs/hr	tons/yr	lbs/hr	tons/yr			
#1 OX	N/A	Formaldehyde	See Appendix B	0	0	0	0					
Fugitives	IV/A	50-00-0		0	U	0	U					
#1 OX	N/A	Methanol	See Appendix B	0.01	0.02	0.001	0.002					
Fugitives	14/11	67-56-1		0.01	0.02	0.001	0.002					
#1 OX	N/A	Benzene	See Appendix B	0	0	0	0					
Fugitives		71-43-2										
#1 OX	N/A	Toluene	See Appendix B	0	0	0	0					
Fugitives		108-88-3			-							
#1 OX	N/A	Methyl Bromide	See Appendix B	0	0	0	0					
Fugitives		74-83-9	g									
#1 OX	N/A	Acetaldehyde	See Appendix B	0	0	0	0					
Fugitives		75-07-0	G 4 11 D									
#1 OX	N/A	Acetic Acid	See Appendix B	45.1	197.5	4.8	21.1					
Fugitives		64-19-7 NO _X	Can Aman din D									
DM-135	O2-10	11104-93-1	See Appendix B	25.75	6.44	25.75	6.44					
			See Appendix B									
DM-135	O2-10	VOC	See Appendix B	0.69	0.17	0.69	0.17					
D) / 105	02.10	CO	See Appendix B	5 00	1.40	7 00	1.40					
DM-135	O2-10	630-08-0	are sign and	5.90	1.48	5.90	1.48					
DM-135	O2-10	SO_2	See Appendix B	0.43	0.11	0.43	0.11					
DWI-133	02-10	7446-09-5		0.43	0.11	0.43	0.11					
DM-135	O2-10	PM	See Appendix B	0.75	0.19	0.75	0.19					
21,1 100	02 10				0.07							
DM-135	O2-10	PM_{10}	See Appendix B	0.75	0.19	0.75	0.19					
		·	See Appendix B									
DM-135	O2-10	PM _{2.5}	See Appendix B	0.75	0.19	0.75	0.19					
		CO ₂ e	See Appendix B									
DM-135	O2-10	124-38-9	zeeppenan. z	440.8	110.2	440.8	110.2					
DD 1012	02.2	NO_X	See Appendix B	1 47	6.4	1.47	6.4					
DB-1813	O2-2	11104-93-1	••	1.47	6.4	1.47	6.4					
DB-1813	O2-2	VOC	See Appendix B	0.08	0.4	0.08	0.4					
DD-1013	02-2	VOC		0.06	0.4	0.06	0.4					



Bureau of Air Quality Construction Permit Application Emissions Page 4 of 6

	D. POTENTIAL EMISSION RATES AT MAXIMUM DESIGN CAPACITY 1. Equipment 2. Emission 3. Pollutants 4. Calculation Methods / Limits Taken / 5. Uncontrolled 6. Controlled 7. Limited												
1. Equipment	2. Emission	3. Pollutants	4. Calculation Methods / Limits Taken /	5. Unco	ntrolled	6. Con	trolled	7. Li i	mited				
ID / Process ID	Point ID	(Include CAS #.)	Other Comments	lbs/hr	tons/yr	lbs/hr	tons/yr	lbs/hr	tons/yr				
DB-1813	O2-2	CO 630-08-0	See Appendix B	1.24	5.4	1.24	5.4						
DB-1813	O2-2	SO ₂ 7446-09-5	See Appendix B	0.01	0.04	0.01	0.0						
DB-1813	O2-2	PM	See Appendix B	0.11	0.5	0.11	0.5						
DB-1813	O2-2	PM ₁₀	See Appendix B	0.11	0.5	0.11	0.5						
DB-1813	O2-2	PM _{2.5}	See Appendix B	0.11	0.5	0.11	0.5						
DB-1813	O2-2	CO ₂ e 124-38-9	See Appendix B	1755	7,687	175	7,687						
#2 HPVGTS	O2-3/4	VOC	See Appendix B	175.0	766.5	3.50	15.3						
#2 HPVGTS	O2-3/4	CO 630-08-0	See Appendix B	1500.0	6571.5	75.0	329.0						
#2 HPVGTS	O2-3/4	CO ₂ e 124-38-9	See Appendix B	2300	10,074	2300	10,074						
DT-302	O2-1	VOC	See Appendix B	8.85	38.8	8.85	38.8						
DT-302	O2-1	CO 630-08-0	See Appendix B	3.47	15.2	3.47	15.2						
DT-302	O2-1	CO ₂ e 124-38-9	See Appendix B	231.7	1,015	231.7	1,015						
DT-500	O2-5	PM	See Appendix B	10	50	0.10	0.5						
DT-500	O2-5	PM ₁₀	See Appendix B	10	50	0.10	0.5						
DT-500	O2-5	PM _{2.5}	See Appendix B	10	50	0.10	0.5						
#2 OX Fugitives	N/A	p-Xylene 106-42-3	See Appendix B	2.2	9.4	0.2	1.0						
#2 OX Fugitives	N/A	Formaldehyde 50-00-0	See Appendix B	0	0	0	0						
#2 OX Fugitives	N/A	Methanol 67-56-1	See Appendix B	0.006	0.03	0.001	0.003						

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Bureau of Air Quality Construction Permit Application Emissions Page 5 of 6

	D. POTENTIAL EMISSION RATES AT MAXIMUM DESIGN CAPACITY 1. Equipment 2. Emission 3. Pollutants 4. Calculation Methods / Limits Taken / 5. Uncontrolled 6. Controlled 7. Limited												
1. Equipment	2. Emission	3. Pollutants	4. Calculation Methods / Limits Taken /		ntrolled		trolled		nited				
ID / Process ID	Point ID	(Include CAS #.)	Other Comments	lbs/hr	tons/yr	lbs/hr	tons/yr	lbs/hr	tons/yr				
#2 OX Fugitives	N/A	Benzene 71-43-2	See Appendix B	0	0	0	0						
#2 OX Fugitives	N/A	Toluene 108-88-3	See Appendix B	0	0	0	0						
#2 OX Fugitives	N/A	Methyl Bromide 74-83-9	See Appendix B	0	0	0	0						
#2 OX Fugitives	N/A	Acetaldehyde 75-07-0	See Appendix B	0	0	0	0						
#2 OX Fugitives	N/A	Acetic Acid 64-19-7	See Appendix B	46.2	202.5	4.8	21.2						
CM-301	P-2	VOC	See Appendix B	10.62	46.5	10.62	46.5						
CM-301	P-2	PM	See Appendix B	121	530	1.21	5.3						
CM-301	P-2	PM_{10}	See Appendix B	121	530	1.21	5.3						
CM-301	P-2	PM _{2.5}	See Appendix B	121	530	1.21	5.3						
CM-404 A/B	P-3 A/B	PM	See Appendix B	30 each	131.4 each	0.3 each	1.3 each						
CM-404 A/B	P-3 A/B	PM_{10}	See Appendix B	30 each	131.4 each	0.3 each	1.3 each						
CM-404 A/B	P-3 A/B	PM _{2.5}	See Appendix B	30 each	131.4 each	0.3 each	1.3 each						
CM-603 A/B	P-4 A/B	PM	See Appendix B	42.4 each	185.8 each	0.42 each	1.9 each						
CM-603 A/B	P-4 A/B	PM_{10}	See Appendix B	42.4 each	185.8 each	0.42 each	1.9 each						
CM-603 A/B	P-4 A/B	PM _{2.5}	See Appendix B	42.4 each	185.8 each	0.42 each	1.9 each						
CM-608 A/B	P-17/18	PM	See Appendix B	0.86 each	3.8 each	0.01 each	0.04 each						
CM-608 A/B	P-17/18	PM_{10}	See Appendix B	0.86 each	3.8 each	0.01 each	0.04 each						
CM-608 A/B	P-17/18	PM _{2.5}	See Appendix B	0.86 each	3.8 each	0.01 each	0.04 each						

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Bureau of Air Quality Construction Permit Application Emissions Page 6 of 6

	D. POTENTIAL EMISSION RATES AT MAXIMUM DESIGN CAPACITY Equipment 2. Emission 3. Pollutants 4. Calculation Methods / Limits Taken / 5. Uncontrolled 6. Controlled 7. Limited												
1. Equipment	2. Emission	3. Pollutants	4. Calculation Methods / Limits Taken /	5. Unco	ntrolled	6. Con	trolled	7. Li i	mited				
ID / Process ID	Point ID	(Include CAS #.)	Other Comments	lbs/hr	tons/yr	lbs/hr	tons/yr	lbs/hr	tons/yr				
CD-405	P-14	PM	See Appendix B	10	43.8	0.1	0.4						
CD-405	P-14	PM_{10}	See Appendix B	10	43.8	0.1	0.4						
CD-405	P-14	PM _{2.5}	See Appendix B	10	43.8	0.1	0.4						
DM-601	P2-2	VOC	See Appendix B	10.62	46.5	10.62	46.5						
DM-601	P2-2	PM	See Appendix B	54	236.5	0.54	2.4						
DM-601	P2-2	PM_{10}	See Appendix B	54	236.5	0.54	2.4						
DM-601	P2-2	PM _{2.5}	See Appendix B	54	236.5	0.54	2.4						
DD-500/DH-518	P2-1	PM	See Appendix B	4	17.5	0.04	0.2						
DD-500/DH-518	P2-1	PM_{10}	See Appendix B	4	17.5	0.04	0.2						
DD-500/DH-518	P2-1	PM _{2.5}	See Appendix B	4	17.5	0.04	0.2						
DM-704	P2-3	PM	See Appendix B	5.2	22.8	0.26	1.1						
DM-704	P2-3	PM_{10}	See Appendix B	5.2	22.8	0.26	1.1						
DM-704	P2-3	PM _{2.5}	See Appendix B	5.2	22.8	0.26	1.1						
DM-797 A/B	P2-4 A/B	PM	See Appendix B	265 each	1161 each	0.27 each	1.2 each						
DM-797 A/B	P2-4 A/B	PM_{10}	See Appendix B	265 each	1161 each	0.27 each	1.2 each						
DM-797 A/B	P2-4 A/B	PM _{2.5}	See Appendix B	265 each	1161 each	0.27 each	1.2 each		_				



Bureau of Air Quality Construction Permit Application Regulatory Review Page 1 of 3

A. APPLICATION IDENTIFICATION									
1. Facility Name: BP Amoco Chemical Company - Cooper River Plant									
2. SC Air Permit Number (8-digits only): 0420 - 0029	3. Application Date: 4/09/2013 – Revised 3/04/2014								

B. SOUTH CAROLINA AIR POLLUTION CONTROL REGULATIONS AND STANDARDS (If not listed below add any additional regulations that are triggered.)												
		licable		ts, work practices, monitoring, recor	d keeping, etc.							
1. Regulation	Yes	No	3. Explain Applicability Determination	4. List the specific limitations and/or requirements that apply.	5. How will compliance be demonstrated?							
Regulation 61-62.1, Section II(E) Synthetic Minor Construction Permits		\boxtimes	Major Source	N/A	N/A							
Regulation 61-62.1, Section II(G) Conditional Major Operating Permits		\boxtimes	Title V Source	N/A	N/A							
Regulation 61-62.5, Standard No. 1 Emissions from Fuel Burning Operations		\boxtimes	No new or modified fuel burn sources	N/a	N/A							
Regulation 61-62.5, Standard No. 2 Ambient Air Quality Standards			No changes to PTE previously modeled, CO modeling below SIL	N/A	N/A							
Regulation 61-62.5, Standard No. 3 Waste Combustion and Reduction		\boxtimes	No new or modified sources	N/A	N/A							
Regulation 61-62.5, Standard No. 3.1 Hospital, Medical, Infections Waste Incinerators (HMIWI)			No applicable sources at facility	N/A	N/A							
Regulation 61-62.5, Standard No. 4 Emissions from Process Industries	\boxtimes		PM sources- the PWR is unchanged	No Change from present	No Change from present							
Regulation 61-62.5, Standard No. 5 Volatile Organic Compounds		\boxtimes	No new or modified sources	N/A	N/A							
Regulation 61-62.5, Standard No. 5.1 BACT/LAER Applicable to VOC	\boxtimes	\boxtimes	VOC increase is less than 100 tpy per PSD analysis	N/A	N/A							
Regulation 61-62.5, Standard No. 5.2 Control of Oxides of Nitrogen		\boxtimes	No new or modified sources	N/A	N/A							
Regulation 61-62.5, Standard No. 7 Prevention of Significant Deterioration	\boxtimes		PSD Permit application									
Regulation 61-62.5, Standard No. 7.1 Nonattainment New Source Review		\boxtimes	Not a non-attainment area	N/A	N/A							
Regulation 61-62.5, Standard No. 8 Toxic Air Pollutants		\boxtimes	Exempt per section 1(d) since all sources covered by a MACT	N/A	N/A							



Bureau of Air Quality Construction Permit Application Regulatory Review Page 2 of 3

D. GOVERN GARDANNA AND DOLLA SERVICE OF THE SERVICE AND GENERAL DESCRIPTION OF THE SERVICE AND G													
B. SOU			AIR POLLUTION CONTROL RE										
	(If not listed below add any additional regulations that are triggered.) 2. Applicable Include all limits, work practices, monitoring, record keeping, etc.												
	2. App	licable											
1. Regulation	Yes	No	3. Explain Applicability	4. List the specific limitations	5. How will compliance be								
	105		Determination	and/or requirements that apply.	demonstrated?								
Regulation 61-62.6		\square	No new or modified sources	N/A	N/A								
Control of Fugitive Particulate Matter			No new of modified sources	N/A	N/A								
Regulation 61-62.68		\boxtimes	No new or modified sources	N/A	N/A								
Chemical Accident Prevention Provisions			No new of modified sources	N/A	N/A								
Regulation 61-62.70			Title V Modification	Davisa Tida V namit	Cl it 1; i								
Title V Operating Permit Program			Title v Modification	Revise Title V permit	Submit application								
Regulation 61-62.72		\boxtimes	No new or modified sources	N/A	NT/A								
Acid Rain			No new of modified sources	N/A	N/A								
Regulation 61-62.96		\boxtimes	No new or modified sources	N/A	N/A								
Nitrogen Oxides Budget Trading Program			No new of modified sources	N/A	N/A								
Regulation 61-62.99													
Nitrogen Oxides Budget Program			N 4:6: - 4	NI/A	NT/A								
Requirements for Stationary Sources			No new or modified sources	N/A	N/A								
Not In the Trading Program													

C. 40 CFR PART 60 - STANDARDS OF PERFORMANCE FOR NEW STATIONARY SOURCES															
	(If not listed below add any additional regulations that are triggered.)														
	2. App	licable	ble Include all limits, work practices, monitoring, record keeping, etc.												
1. Subpart and Title	Yes	No	3. Explain Applicability	4. List the specific limitations	5. How will compliance be										
	res	110	Determination	and/or requirements that apply.	demonstrated?										
Subpart A - General Provisions			New or modified sources subject												
NNN			New sources	Maintain TRE from recovery device	Monitor recovery per regulation to										
191919		Ш	New sources	above 8	maintain TRE										
III			New reactor on #1 OX	Maintain TRE from recovery device	Monitor recovery per regulation to										
III			New leactor on #1 OX	above 4	maintain TRE										
VV			New components	Will comply by HON LDAR	HON LDAR monitoring										
VVa			New components	Will comply by HON LDAR	HON LDAR monitoring										



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D. 40 CFR PART 61 - NATIONAL EMISSION STANDARDS FOR HAZARDOUS AIR POLLUTANTS (If not listed below add any additional regulations that are triggered.)											
		licable		its, work practices, monitoring, record keeping, etc.							
1. Subpart and Title	Yes	No	3. Explain Applicability Determination	4. List the specific limitations and/or requirements that apply.	5. How will compliance be demonstrated?						
Subpart A - General Provisions		\boxtimes	No new or modified sources	N/A	N/A						
M			General for facility demo work	Proper handling of asbestos	Proper handling methods						
FF			Need to re-evaluate TAB	Re-evaluate TAB < 1 Mg	TAB calculation						
E. 40 CFR PART 63 - NATI			ON STANDARDS FOR HAZARDOUT ted below add any additional regulation		CE CATEGORIES						
	2. App	licable	Include all limi	ts, work practices, monitoring, reco	rd keeping, etc.						
1. Subpart and Title	Yes	Nia	3. Explain Applicability	4. List the specific limitations	5. How will compliance be						
		No	Determination	and/or requirements that apply.	demonstrated?						
Subpart A - General Provisions	\boxtimes		New or modified sources								
F			New or modified sources								
G			New or modified sources	Maintain TRE of process vents	Monitor per HON regulation						
Н			New or modified sources	Have a LDAR program	Monitor & Report per HON						
DDDDD	\boxtimes		Applicable to equipment but no new or modified sources	No new limits or requirements	Burn only gas						
GGGGG	\boxtimes		Will be triggered if remediation occurs due to project	Comply with appropriate standards	Meet appropriate monitoring and reporting requirement of regulation						
			F. OTHER								
(If not listed below	add any	additiona	d regulations, enforcement requirement	<u> </u>							
	2. App	licable		ts, work practices, monitoring, reco	1 U/						
1. Regulation and Title / Other	Yes	No	3. Explain Applicability Determination	4. List the specific limitations and/or requirements that apply.	5. How will compliance be demonstrated?						
40 CFR Part 64 - Compliance Assurance			Novy or modified courses	Undata CAM plan as pagagami	Manitan man CAM mlan & nament						

New or modified sources

Monitoring (CAM)

 \boxtimes

Update CAM plan as necessary

Monitor per CAM plan & report



Bureau of Air Quality Modeling Information Page 1 of 4

		A. APPLICAT	TION IDENTIFI	CATION							
1. Facility Name: BP Amoco Cher	nical Company - Coope	r River Plant									
2. SC Air Permit Number (if know	· C 2/		3. Applica	tion Date: 4/09/2	013 – Revised 3/04	/2014					
4. Project Description: BP CR Mo	dernization/Debottlenec	k Project									
		B. FACIL	ITY INFORMA								
1. Is your company a Small Busine					ureau modeling ass			Yes	⊠ No		
3. Are other facilities co-modeled?	? ☐ Yes ⊠ No		4. If Yes, p	provide permit nu	imbers of co-mode	ed facili	ities:				
			DELING CON	TACT							
Consulting Firm Name (if applical			1								
Title/Position: Senior Environmen		Salutation: Mr.	First Name	e: David		ast Nan	ne: Fox				
Mailing Address: Suite 3000 708	8 Heartland Trail		T								
City: Madison State: Wi Zip Code: 53717											
E-mail Address: DFox@trcsolutio	ns.com		Phone No.	: 608-826-3622	[(Cell No.:	608-216-8986				
		D DELGG	N EOD MODE	r Dio							
			ON FOR MODE	· -							
1. Modeling Not Required	Explanation:	(Cne	ck all that apply.)								
1. Modernig Not Required	Particulate Matter	Particulate Matter	Sulfur	Nitrogen	Carbon	Lood	Heduagan	Air			
2. Modeling/Pollutant	<10 Microns (PM ₁₀)	<2.5 Microns (PM _{2.5})	Dioxide (SO ₂)	Oxides (NO _x)		Lead (Pb)	Hydrogen Fluoride (HF)	Toxics	Other		
Not Modeled		2.3 WHCI OHS (1 W12.5)	\boxtimes								
Standard 2 AAQS								N/A	HH		
Standard 2 Farigo Standard 2 Exemption/Deferral						H		N/A	╁╫		
Standard 7 Increment					N/A	N/A	N/A	N/A	H		
Standard 7 Exemption/Deferral					N/A	N/A	N/A	N/A	H		
Standard 8 Air Toxics	N/A	N/A	N/A	N/A	N/A	N/A	N/A				
Standard 8 De Minimis / Exempt	N/A	N/A	N/A	N/A	N/A	N/A	N/A				
NSR/PSD Project											
Air Compliance Demonstration											
Other											
3. "Other" Reason for modeling											



Bureau of Air Quality Modeling Information Page 2 of 4

E. EMISSION SOURCE DISPERSION PARAMETERS

Source data requirements are based on the appropriate source classification. Each emission source is classified as a point, area, volume, or flare source. Contact the Bureau of Air Quality for clarification of input data requirements. Include source on-site map. Also, a picture of area or volume sources would be helpful but is not required. A spreadsheet may be substituted in lieu of this form provided the required emission point parameters are submitted in the same order as presented in these tables.

Abbreviations / Units of Measure: UTM = Universal Transverse Mercator; °N = Degrees North; °W = Degrees West; m = meters; AGL = Above Ground Level; ft = feet; ft/s = feet per second; ° = Degrees; °F = Degrees Fahrenheit

	F. POINT SOURCE DATA (Point sources such as stacks, chimneys, exhaust fans, and vents.)														
Emission Point ID Description/Name		Stack Coord Projection: U			Release Height	Tomp	Exit	Inside	Discharge	Rain	Distance To Nearest		Building		
	Description/Name	UTM E (m)	UTM N (m)	Lat (°N)	Long (°W)	AGL (ft)	Temp. (°F)	Velocity (ft/s)	Diameter (ft)	Discharge Orientation	Cap? (Y/N)	Property Boundary (ft)	Height (ft)	Length (ft)	Width (ft)
BT_702	BT-702 DHT Scrubber	604625	3649190			35.00	90	69.9	1.00	V	N	964	54	62	51
BT_603	#1 OX LPA	604639	3649127			70.5	120	11.2	2.50	V	N	907	54	62	51
HPVGTS1	#1 Ox HPVGTS	604666.1	3649104.3			100.0	171	261.7	3.0	V	N	878	54	62	51
DT_302	#2 OX LPA	604565	3648820			80.0	95	3.2	3.5	V	N	590	32	44	29
HPVGTS2	#2 OX HPVGTS	604642.3	3648895.9	•		136.0	140	98.0	4.26	V	N	667	32	44	29

	G. AREA SOURCE DATA (Area sources such as storage piles, and other sources that have low level or ground level releases with no plumes.)														
Emission Point ID	Description/Name	Area Source Coordinates Projection: UTM E			Long	Release Height AGL (ft)	Easterly Length (ft)	Northerly Length (ft)	Angle From North	Distance To Nearest Property Boundary (ft)					
NA															
	_						<u> </u>								

	H. VOLUME SOURCE DATA (Volume sources that have initial dispersion prior to release. Volume sources differ from area sources in that they have an initial dispersion vertical depth.)														
Emission Point ID	Description/Name	Volume Source Coordinates Projection: UTM E UTM N Lat Long (m) (m) (°N) (°W)			Long	Release Height AGL (ft)	Initial Horizontal Dimension (ft)	Initial Vertical Dimension (ft)	Distance To Nearest Property Boundary (ft)						
NA															
	_														



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	I. FLARE SOURCE DATA (Point sources where the combustion takes place at the tip of the stack.)												
Emission	Description Nome		Stack Coo Projection			Release Height	Heat Release Rate	Distance To Nearest		Building			
Point ID	Description/Name	UTM E	UTM N	Lat	Long	AGL (ft)	(BTU/hr)	Property Boundary (ft)	Height	Length	Width		
		(m)	(m)	(°N)	(° W)			(It)	(ft)	(ft)	(ft)		
NA													

	J. AREA CIRCULAR SOURCE DATA												
Emission Point ID	Description/Name	Area Circular Source Coordinates Projection:				Release Height	Radius of Area	Distance To Nearest Property					
		UTM E (m)	UTM N (m)	Lat (°N)	Long (°W)	AGL (ft)	(ft)	Boundary (ft)					
NA													

	K. AREA POLY SOURCE DATA											
		Area I	Poly Source	e Coordinates								
Emission	Description/Name	Projection:			Release Height	Number of Vertices						
Point ID		UTM E	UTM N	Lat Long	AGL (ft)	Number of vertices						
		(m)	(m)	(°N) (°W)								
NA				NA								
				(See Instructions)								
				(See Histractions)								

	L. OPEN PIT SOURCE DATA											
		Ope	en Pit Sourc	e Coordinates								
Emission	Description/Nome		Projection	n:	Release Height	Easterly Length	Northerly Length	Volume	Angle From North			
Point ID	Description/Name	UTM E UT		Lat Long	AGL (ft)	(ft)	(ft)	(ft ³)	(°)			
		(m)	(m)	(°N) (°W)								
NA				NA								
				(See Instructions)								
				(See mstructions)								



Bureau of Air Quality Modeling Information Page 4 of 4

	M. M	ODELED EMISS	ION RATES			
Emission Point ID	Pollutant Name	CAS#	Emission Rate (lb/hr)	Same as Permitted ⁽¹⁾	Controlled or Uncontrolled	Averaging Period
BT-702	СО		-87.0	⊠ Yes □ No	Controlled	1,8
BT-603	СО		4.1	☐ Yes ⊠ No	Controlled	1,8
#1 HPVGTS	СО		87.9	☐ Yes ⊠ No	Controlled	1,8
DT-302	СО		3.5	☐ Yes ⊠ No	Controlled	1,8
#2 HPVGTS	СО		75.0	☐ Yes ⊠ No	Controlled	1,8
				Yes No		
				Yes No		
				Yes No		
				Yes No		
				Yes No		

⁽¹⁾ Any difference between the modeled rate and the permitted rate must be explained in the modeling report.

Appendix B Emission Data and Calculations

PSD Analysis

Table B-1
Project Dragonslayer PSD Emissions Analysis Summary

Post-Project PTE Emissions (Before BACT) (tpy)

POLLUTANTS	CR #1 OX	CR #2 OX	CR #1 PTA	CR #2 PTA	COOLING TOWER	TANK FARM ⁽¹⁾	SHIPPING ⁽¹⁾	INC. STEAM ⁽¹⁾	TOTAL				
NOx	0.5	12.9	0	0	0	0	0	17.3	30.7				
VOC	157.0	150.3	46.5	46.5	0	1.3	0	1.2	402.8				
СО	403.1	351.1	0	0	0	0	0	17.8	771.9				
SO ₂	0.03	0.1	0	0	0	0	0	0.1	0.3				
PM	6.6	1.1	12.1	6.0	3.8	0	9.9	1.1	40.7				
PM ₁₀	6.6	1.1	12.1	6.0	2.8	0	9.9	1.1	39.6				
PM _{2.5}	6.6	1.1	12.1	6.0	0.01	0	9.9	1.1	36.9				
CO ₂ e	42,947	18,886	0	0	0	0	0	25,265	87,098				

⁽¹⁾ These units will not be modified. Tank Farm and Shipping are debottlenecked and incremental steam from boiler.

Baseline Actual Average 2010-2011 Emissions (tpy)

POLLUTANTS	CR #1 OX	CR #2 OX	CR #1 PTA	CR #2 PTA	COOLING TOWER	TANK FARM	SHIPPING	INC. STEAM	TOTAL
NOx	0.2	2.9	0	0	0	0	0	0	3.1
VOC	124.7	111.9	40.1	42.0	0	1.2	0	0	319.9
CO	275.1	71.6	0	0	0	0	0	0	346.7
SO ₂	0.01	0.03	0	0	0	0	0	0	0.04
PM	3.3	0.6	12.9	5.4	2.7	0	8.8	0	33.7
PM ₁₀	3.3	0.6	12.9	5.4	1.9	0	8.8	0	33.0
PM _{2.5}	3.4	0.6	12.9	5.4	0.01	0	8.8	0	31.1
CO ₂ e	38,807	30,987	0	0	0	0	0	0	69,793

Step 1 - Project Pollutant Increases Above PSD Significance

POLLUTANTS	VOC	CO	NOx	SO ₂	PM	PM ₁₀	PM _{2.5}	CO ₂ e
TOTAL PTE	402.8	771.9	30.7	0.3	40.7	39.6	36.9	87,098
TOTAL BASELINE	319.9	346.7	3.1	0.04	33.7	33.0	31.1	69,793
DELTA	82.9	425.2	27.6	0.3	7.0	6.7	5.8	17,304
PSD SIGNIFICANCE	40	100	40	40	25	15	10	75,000
ABOVE PSD	Yes	Yes	No	No	No	No	No	No

Table B-1
Project Dragonslayer PSD Emissions Analysis Summary

Step 2 - Facility Netting

POLLUTANTS	VOC	CO	NOx	SO ₂	PM	PM ₁₀	PM _{2.5}	CO ₂ e
STEP 1 DELTA	82.9	425.2	27.6	0.3	7.0	6.7	5.8	17304.2
TOTAL CONTEMPORANEOUS	35.8	26.9	N/A	N/A	N/A	N/A	N/A	N/A
NET EMISSIONS	118.8	452.1	27.6	0.3	7.0	6.7	5.8	17304.2
PSD SIGNIFICANCE	40	100	40	40	25	15	10	75,000
ABOVE PSD	Yes	Yes	No	No	No	No	No	No

Contemporaneous Emissions

PROJECT	YEAR	CO (tpy)	VOC (tpy)
502b10 - CR #1 Ox BR-301A Alternate Water Withdrawl	2008	0.0	0
PTA FIP Project (Permit CS)	2008	0.01	8.24
502b10 - #1 OX/PTA Op Flex	2011	0	0
PTA BHS Filter Project	2012	26.9	27.6
Total		26.9	35.8

Post-Project PTE Emissions (After BACT) (tpy)

		, , , , , , , , , , , , , , , , , , , ,				(1.7)			
POLLUTANTS	CR #1 OX	CR #2 OX	CR #1 PTA	CR #2 PTA	COOLING TOWER	TANK FARM ⁽¹⁾	SHIPPING ⁽¹⁾	INC. STEAM ⁽¹⁾	TOTAL
NOx	0.5	12.9	0	0	0	0	0	17.3	30.7
VOC	84.5	76.8	46.5	46.5	0	1.3	0	1.2	256.8
CO	403.1	351.1	0	0	0	0	0	17.8	771.9
SO ₂	0.0	0.1	0	0	0	0	0	0.1	0.3
PM	6.6	1.1	12.1	6.0	3.8	0	9.9	1.1	40.7
PM ₁₀	6.6	1.1	12.1	6.0	2.8	0	9.9	1.1	39.6
PM _{2.5}	6.6	1.1	12.1	6.0	0.01	0	9.9	1.1	36.9
CO ₂ e	42,947	18,886	0	0	0	0	0	25265.0	87,098

⁽¹⁾ These units will not be modified. Tank Farm and Shipping are debottlenecked and incremental steam from boiler.

Table B-2 CR #1 OX PSD Analysis

PTE

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM FIRE RATE (HP)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR	UNITS	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS	
			NOx	0.031	lb/hp-hr	AP-42 3.3 (10/96)	10.385	100	0.5		
			VOC	0.00251	lb/hp-hr	AP-42 3.3 (10/96)	0.842	100	0.04		
			CO	0.00668	lb/hp-hr	AP-42 3.3 (10/96)	2.238	100	0.1		
Emergency Generator #2	BM-1201	335	SO ₂	0.00205	lb/hp-hr	AP-42 3.3 (10/96)	0.687	100 0.03 Die:	Diesel Fuel Sulfur = 0.05%,		
Efficigency Generator #2	DIVI-1201	333	PM	0.0022	lb/hp-hr	AP-42 3.3 (10/96)	0.737	100	0.04	Hours per RICE MACT limit	
			PM ₁₀	0.0022	lb/hp-hr	AP-42 3.3 (10/96)	0.737	100	0.04		
			PM _{2.5}	0.0022	lb/hp-hr	AP-42 3.3 (10/96)	0.737	100	0.04		
			CO ₂ e	163.6	lb/MMBtu	USEPA Data	137.634	100	6.9		
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (lb/hr)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR	UNITS	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS	
		234	VOC	98.0	% Removal	BP Calcs/BACT Limit	4.7	8,760	20.5	Maximum rate based on BP	
HPVGTS	HPVGTS-1	1758	CO	95.0	% Removal	DI Calcs/DACT LITTIL	87.9	8,760	385.0	design calculations &	
		9520.6	CO ₂ e	0	% Removal	BP calc/USEPA EF	9,520.6	8,760	41,700	Requested BACT Limit	
		9.6	VOC			BP Calcs/BACT Limit	9.6	8,760	42.0	Maximum rate based on BP	
Low Pressure Absorber	BT-603	4.1	CO			DI Galc3/DAGT EliTilit	4.1	8,760	18.0	design calculations &	
		283.0	CO₂e			BP calc/USEPA EF	283.0	8,760	1240	Requested BACT Limits	
CRU Extraction Drum	BD-625		VOC								
CRU Surge Drum	BD-631	CRU removed								CRU is being removed	
CRU Waste Slurry Drum	BD-632		VOC								
			PM	98	% Removal	Average of data from	1.50	8,760	6.6	Maximum rate based on	
Silo Scrubber	BT-501	75	PM ₁₀	98	% Removal	2/03 & 11/02 source	1.50	8,760	6.6	hourly emissions and %	
			PM _{2.5}	98	% Removal	tests	1.50	8,760	6.6	removal	
CRU Evaporator Overhd Condenser	BE-645	CRU removed	VOC							CRU being removed	
		Vent	VOC								
DHT Ovhd Scrubber	BT-702	Removed	CO							Vent Removed	
		Removed	CO ₂ e								
Process Fugitives			VOC			USEPA LDAR EF	21.5	8,760	94.4		

Table B-2 CR #1 OX PSD Analysis

2010 Actuals										
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM FIRE RATE (HP)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR	UNITS	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	ACTUAL OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
			NOx	0.031	lb/hp-hr	AP-42 3.3 (10/96)	10.385	33	0.2	
			VOC	0.00251	lb/hp-hr	AP-42 3.3 (10/96)	0.842	33	0.01	
			CO	0.00668	lb/hp-hr	AP-42 3.3 (10/96)	2.238	33	0.04	
Emergency Generator #2	BM-1201	335	SO ₂	0.00205	lb/hp-hr	AP-42 3.3 (10/96)	0.687	33	0.01	Diesel Fuel Sulfur = 0.05%
Emergency Generator #2	DIVI-1201	333	PM	0.0022	lb/hp-hr	AP-42 3.3 (10/96)	0.737	33	0.01	Diesei Fuei Sullul = 0.05%
			PM ₁₀	0.0022	lb/hp-hr	AP-42 3.3 (10/96)	0.737	33	0.01	
			PM _{2.5}	0.0022	lb/hp-hr	AP-42 3.3 (10/96)	0.737	33	0.01	
			CO ₂ e	163.6	lb/MMBtu	USEPA Data	137.634	33	2.3	
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (lb/hr)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR	UNITS	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	ACTUAL OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
			VOC			Emission Inventory	3	8,291	13.5	
HPVGTS	HPVGTS-1		CO			Emission inventory	77	8,291	319.8	
			CO ₂ e			BP calcs/EPA EF	9504	8,291	39,398.4	
			VOC			Emission Inventory	5	8,291	22.0	
Low Pressure Absorber	BT-603		CO			Linission inventory	1	8,291	3.9	
			CO₂e			BP calcs/EPA EF	110	8,291	457.2	
CRU Extraction Drum	BD-625		VOC			Emission Inventory	1.0	8,291	4.1	
CRU Surge Drum	BD-631		VOC			Emission Inventory	4.0	8,291	16.6	
CRU Waste Slurry Drum	BD-632		VOC			Emission Inventory	0.003	8,291	0.01	
			PM	98	% Removal	Average of data from	0.84	8,291	3.5	
Silo Scrubber	BT-501		PM ₁₀	98	% Removal	12/14/04 source test	0.84	8,291	3.5	
			PM _{2.5}	98	% Removal	12/11/01/0001001001	0.84	8,291	3.5	
CRU Evaporator Overhd Condenser	BE-645		VOC			Emission Inventory	0.3	8,291	1.2	
			VOC			Emission Inventory	20.6	62	0.6	
DHT Ovhd Scrubber	BT-702		CO			Liniosion inventory	76.5	62	2.4	Based on hours vent open
			CO₂e			BP calcs/EPA EF	534.1	62	16.6	
Process Fugitives			VOC			USEPA LDAR EF	19.8	8,291	82.1	

Table B-2 CR #1 OX PSD Analysis

2011 Actuals										
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM FIRE RATE (HP)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR	UNITS	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	ACTUAL OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
			NOx	0.031	lb/hp-hr	AP-42 3.3 (10/96)	10.385	44	0.2	
			VOC	0.00251	lb/hp-hr	AP-42 3.3 (10/96)	0.842	44	0.02	
			CO	0.00668	lb/hp-hr	AP-42 3.3 (10/96)	2.238	44	0.05	
Emergency Generator #2	BM-1201	335	SO ₂	0.00205	lb/hp-hr	AP-42 3.3 (10/96)	0.687	44	0.02	Diesel Fuel Sulfur = 0.05%
Emergency Generator #2	DIVI-1201	333	PM	0.0022	lb/hp-hr	AP-42 3.3 (10/96)	0.737	44	0.02	Diesei i dei Sulidi = 0.03 /6
			PM ₁₀	0.0022	lb/hp-hr	AP-42 3.3 (10/96)	0.737	44	0.02	
			PM _{2.5}	0.0022	lb/hp-hr	AP-42 3.3 (10/96)	0.737	44	0.02	
			CO ₂ e	163.6	lb/MMBtu	USEPA Data	137.634	44	3.0	
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (lb/hr)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR	UNITS	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	ACTUAL OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
			VOC			Emission Inventory	3	7,608	10.3	
HPVGTS	HPVGTS-1		CO			Emission Inventory	58	7,608	219.9	
			CO ₂ e			BP calcs/EPA EF	9800	7,608	37,278.5	
			VOC			Emission Inventory	1	7,608	3.0	
Low Pressure Absorber	BT-603		CO			Emission inventory	1	7,608	2.7	
			CO ₂ e			BP calcs/EPA EF	117	7,608	446.5	
CRU Extraction Drum	BD-625		VOC			Emission Inventory	1.0	7,608	3.8	
CRU Surge Drum	BD-631		VOC			Emission Inventory	4.0	7,608	15.2	
CRU Waste Slurry Drum	BD-632		VOC			Emission Inventory	0.003	7,608	0.01	
			PM	98	% Removal	Average of data from	0.84	7,608	3.2	
Silo Scrubber	BT-501		PM ₁₀	98	% Removal	12/14/04 source test	0.84	7,608	3.2	
			PM _{2.5}	98	% Removal	12/14/04 300100 1001	0.84	7,608	3.2	
CRU Evaporator Overhd Condenser	BE-645		VOC			Emission Inventory	0.3	7,608	1.1	
			VOC			Emission Inventory	14.5	59	0.4	
DHT Ovhd Scrubber	BT-702	-	CO			Lillippion inventory	54.7	59	1.6	Based on hours vent open
			CO ₂ e			BP calcs/EPA EF	379.5	59	11.2	
Process Fugitives			VOC			USEPA LDAR EF	19.8	7,608	75.4	

	TOTAL EMISSIONS - #1 OX PTE (tpy)											
POLLUTANT	PROCESS SOURCES	COMBUSTION SOURCES	FUGITIVE SOURCES	TOTALS								
NOx	0	0.5	N/A	0.5								
VOC	62.5	0.04	94.4	157.0								
CO	403.0	0.1	N/A	403.1								
SO ₂	0	0.03	N/A	0.03								
PM	6.6	0.04	N/A	6.6								
PM ₁₀	6.6	0.04	N/A	6.6								
PM _{2.5}	6.6	0.04	N/A	6.6								
CO ₂ e	42,939.8	6.9	N/A	42,946.7								

	TOTAL EMISSIONS - #1 OX BASELINE ACTUAL (tpy)											
POLLUTANT	PROCESS SOURCES	COMBUSTION SOURCES	FUGITIVE SOURCES	TOTALS								
NOx	0	0.2	N/A	0.2								
VOC	46.0	0.02	78.7	124.7								
CO	275.1	0.04	N/A	275.1								
SO ₂	0	0.01	N/A	0.01								
PM	3.3	0.01	N/A	3.3								
PM ₁₀	3.3	0.01	N/A	3.3								
PM _{2.5}	3.3	0.01	N/A	3.4								
CO₂e	38,804.2	2.6	N/A	38,806.8								

POLLUTANT	THRESHOLD	DELTA (PTE - ACTUAL)
NOx	40	0.3
VOC	40	32.2
CO	100	128.0
SO ₂	40	0.02
PM	25	3.3
PM ₁₀	15	3.3
PM _{2.5}	10	3.3
CO ₂ e	75,000	4,139.9

PTE

					NATURAL GAS	3				DIESEL FUEL (SULFUR = 0.05%)			
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM FIRE RATE	POLLUTANT EMITTED	AP-42 1.4 FACTOR (lb/MM scf)	NATURAL GAS EF (lb/MMBtu)	HOURLY EMISSION (lb/hr)	PERMIT OPERATE (hpy)	ANNUAL EMISSION (tpy)	AP-42 FACTOR (lb/hp-hr)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMIT OPERATE (hpy)*	Annual Emission (tpy) - Oil
			NOx						0.024	AP-42 3.4 (10/96)	25.75	500	6.44
		1072.8	VOC						0.000642	AP-42 3.4 (10/96)	0.69	500	0.17
			CO						0.0055	AP-42 3.4 (10/96)	5.90	500	1.48
Emergency Generator #3	DM-135		SO ₂						0.00040	AP-42 3.4 (10/96)	0.43	500	0.11
Emergency Generator #5	DIVI-133		PM						0.0007	AP-42 3.4 (10/96)	0.75	500	0.19
		hp	PM ₁₀						0.0007	AP-42 3.4 (10/96)	0.75	500	0.19
			PM _{2.5}						0.0007	AP-42 3.4 (10/96)	0.75	500	0.19
			CO₂e						163.6	lb/MMBtu-USEPA	440.76	500	110.19
			NOx	100	0.098	1.47	8,760	6.4					
		15.0	VOC	5.5	0.005	0.08	8,760	0.4					
			CO	84	0.082	1.24	8,760	5.4					
HPVGTS Heater	DB-1813		SO ₂	0.6	0.001	0.01	8,760	0.04					
The vote Houles	22 1010		PM	7.6	0.007	0.11	8,760	0.5					
		MMBtu/hr	PM ₁₀	7.6	0.007	0.11	8,760	0.5					
			PM _{2.5}	7.6	0.007	0.11	8,760	0.5					
			CO ₂ e		117.000	1755.00	8,760	7,687.0					
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (lb/hr)	POLLUTANT EMITTED	POLLUTANT EF (% Removal)	EMISSION FACTOR REFERENCE	HOURLY EMISSION (lb/hr)	PERMIT OPERATE (hpy)	ANNUAL EMISSION (tpy)		COI	MMENTS		
	DD 4044/ DT	175	VOC	98%	BP Calcs/BACT Limit	3.50	8,760	15.3					
HPVGTS	DR-1814/ DT- 1821	1500	CO	95%	DP Calcs/DACT LITTIL	75.0	8,760	329.0	Maximum rat	e based on BP desig	n calculations &	requested B	ACT limits
	1021	2300	CO ₂ e	0	BP calc/USEPA EF	2300	8,760	10,074					
		8.85	VOC		BP Calcs/BACT Limit	8.85	8,760	38.8					
Low Pressure Absorber	DT-302	3.47	CO		BF Calcs/BACT LITTIL	3.47	8,760	15.2	Maximum rat	e based on BP desig	n calculations &	requested B	ACT limits
		231.7	CO ₂ e		BP calc/USEPA EF	231.7	8,760	1,015					
			PM	99	BP Calcs	0.10	8,760	0.5	Maximum rat	e based on hourly em	piccione and %	omoval and	application
Intermediate Silo Scrubber	DT-500	10.4	PM ₁₀	99	BP Calcs	0.10	8,760	0.5	Waxiiiiuiii Tat	,	nit (permit CF)	emovai anu i	application
			PM _{2.5}	99	BP Calcs	0.10	8,760	0.5		101 #Z di	iit (permit or)		
CRU Extraction Drum	DD-412		VOC										
CRU Waste Slurry Drum	DD-413	CRU removed	VOC						CRU is being removed				
CRU Mother Liquor Drum	DD-414	Cito removed	VOC										
CRU Evaporation Drum	DE-416		VOC										
Process Fugitives			VOC		USEPA LDAR EF	5.06	8,760	95.7					

^{*} Hours of operation of DM-135 based on Title V permit limit.

Table B-3 #2 OX PSD Analysis

					NATURAL GAS	3				DIESEL FUEL (SULFUR = 0.05%)			
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM FIRE RATE	POLLUTANT EMITTED	AP-42 1.4 FACTOR (lb/MM scf)	NATURAL GAS EF (lb/MMBtu)	HOURLY EMISSION (lb/hr)	ACTUAL OPERATE (hpy)	ANNUAL EMISSION (tpy)	AP-42 FACTOR (lb/hp-hr)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	ACTUAL OPERATE (hpy)	ANNUAL EMISSION (tpy) - OIL
			NOx						0.024	AP-42 3.4 (10/96)	25.75	61	0.79
		1072.8	VOC						0.000642	AP-42 3.4 (10/96)	0.69	61	0.02
			CO						0.0055	AP-42 3.4 (10/96)	5.90	61	0.18
Emergency Generator #3	DM-135		SO ₂						0.00040	AP-42 3.4 (10/96)	0.43	61	0.01
Emergency Generator #3	DIVI-133		PM						0.0007	AP-42 3.4 (10/96)	0.75	61	0.02
		hp	PM ₁₀						0.0007	AP-42 3.4 (10/96)	0.75	61	0.02
			PM _{2.5}						0.0007	AP-42 3.4 (10/96)	0.75	61	0.02
			CO ₂ e						163.6	lb/MMBtu-USEPA	440.76	61	13.44
			NOx	100	0.098	0.45	8,083	1.8					
		4.64	VOC	5.5	0.005	0.03	8,083	0.1					
			CO	84	0.082	0.38	8,083	1.5					
HPVGTS Heater	DB-1813		SO ₂	0.6	0.001	0.00	8,083	0.01					
The VOTO Ficules	DB 1015		PM	7.6	0.007	0.03	8,083	0.1					
		MMBtu/hr	PM ₁₀	7.6	0.007	0.03	8,083	0.1					
			PM _{2.5}	7.6	0.007	0.03	8,083	0.1					
			CO₂e		117.000	542.50	8,083	2192.5					
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (lb/hr)	POLLUTANT EMITTED	POLLUTANT EF (% Removal)	EMISSION FACTOR REFERENCE	HOURLY EMISSION (lb/hr)	ACTUAL OPERATE (hpy)	ANNUAL EMISSION (tpy)		COI	MMENTS		
	DR-1814/ DT-		VOC		Emission Inventory	2.56	8,096	10.4					
HPVGTS	1821		CO		Linission inventory	18.13	8,096	73.4					
	1021		CO ₂ e		BP calcs/EPA EF	4707.58	8,096	19056.3					
			VOC		Emission Inventory	4.70	8,096	19.0					
Low Pressure Absorber	DT-302		CO		Linission inventory	0.02	8,096	0.1					
			CO ₂ e		BP calcs/EPA EF	6.25	8,096	25.3					
			PM	99	BP Calcs	0.10	8,096	0.4					
Intermediate Silo Scrubber	DT-500	10	PM ₁₀	99	BP Calcs	0.10	8,096	0.4	Maxi	mum rate based on h	ourly emissions	and % remo	val
			PM _{2.5}	99	BP Calcs	0.10	8,096	0.4					
CRU Extraction Drum	DD-412		VOC		BP Calcs	0.00	8,096	0.02					
CRU Waste Slurry Drum	DD-413		VOC		BP Calcs	0.04	8,096	0.2					
CRU Mother Liquor Drum	DD-414		VOC		BP Calcs	0.04	8,096	0.2					
CRU Evaporation Drum	DE-416		VOC		BP Calcs	1.00	8,096	4.0					
Process Fugitives			VOC		USEPA LDAR EF	20.05	8,096	81.2					

Table B-3 #2 OX PSD Analysis

2011 Actuals					NATURE GAS					DIESEL FUEL	(SULFUR = 0.05°	%)	
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM FIRE RATE	POLLUTANT EMITTED	AP-42 1.4 FACTOR (lb/MM scf)	NATURAL GAS EF (lb/MMBtu)	HOURLY EMISSION (lb/hr)	ACTUAL OPERATE (hpy)	ANNUAL EMISSION (tpy)	AP-42 FACTOR (lb/hp-hr)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	ACTUAL OPERATE (hpy)	ANNUAL EMISSION (tpy) - OIL
			NOx						0.024	AP-42 3.4 (10/96)	25.75	70	0.90
		1072.8	VOC						0.000642	AP-42 3.4 (10/96)	0.69	70	0.02
			CO						0.0055	AP-42 3.4 (10/96)	5.90	70	0.21
Emergency Generator #3	DM-135		SO ₂						0.00040	AP-42 3.4 (10/96)	0.43	70	0.02
Efficiency Generator #3	DIVI-133		PM						0.0007	AP-42 3.4 (10/96)	0.75	70	0.03
		hp	PM ₁₀						0.0007	AP-42 3.4 (10/96)	0.75	70	0.03
			PM _{2.5}						0.0007	AP-42 3.4 (10/96)	0.75	70	0.03
			CO ₂ e						163.6	lb/MMBtu-USEPA	440.76	70	15.43
			NOx	100	0.098	0.55	8,374	2.3					
		5.57	VOC	5.5	0.005	0.03	8,374	0.1					
			CO	84	0.082	0.46	8,374	1.9					
HPVGTS Heater	DB-1813		SO ₂	0.6	0.001	0.00	8,374	0.01					
TH VOTOTICALCI	DB 1010		PM	7.6	0.007	0.04	8,374	0.2					
		MMBtu/hr	PM ₁₀	7.6	0.007	0.04	8,374	0.2					
			PM _{2.5}	7.6	0.007	0.04	8,374	0.2					
			CO ₂ e		117.000	651.20	8,374	2726.6					
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (lb/hr)	POLLUTANT EMITTED	POLLUTANT EF (% Removal)	EMISSION FACTOR REFERENCE	HOURLY EMISSION (lb/hr)	ACTUAL OPERATE (hpy)	ANNUAL EMISSION (tpy)		COI	MMENTS		
	DR-1814/		VOC		Emission Inventory	0.29	8,392	1.2					
HPVGTS	DT-1821		CO		Linission inventory	15.67	8,392	65.7					
	D1-1021		CO ₂ e		BP calcs/EPA EF	9036.94	8,392	37,919.0					
			VOC		Emission Inventory	4.45	8,392	18.7					
Low Pressure Absorber	DT-302		CO		Linission inventory	0.02	8,392	0.1					
			CO ₂ e		BP calcs/EPA EF	5.92	8,392	24.8					
			PM	99	BP Calcs	0.10	8,392	0.4					
Intermediate Silo Scrubber	DT-500	10	PM ₁₀	99	BP Calcs	0.10	8,392	0.4	Maxir	mum rate based on h	ourly emissions	and % remo	val
			PM _{2.5}	99	BP Calcs	0.10	8,392	0.4					
CRU Extraction Drum	DD-412		VOC		BP Calcs	0.00	8,392	0.02					
CRU Waste Slurry Drum	DD-413		VOC		BP Calcs	0.04	8,392	0.2					
CRU Mother Liquor Drum	DD-414		VOC		BP Calcs	0.04	8,392	0.2					
CRU Evaporation Drum	DE-416		VOC		BP Calcs	1.00	8,392	4.2					
Process Fugitives			VOC		USEPA LDAR EF	20.05	8,392	84.1					

Table B-3 #2 OX PSD Analysis

	ANNUAL EMISSIONS - PTE										
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION SOURCES (tpy)	FUGITIVE SOURCES (tpy)	TOTALS							
NOx	0	12.9	N/A	12.9							
VOC	54.1	0.5	95.7	150.3							
CO	344.2	6.9	N/A	351.1							
SO ₂	0	0.1	N/A	0.1							
PM	0.5	0.7	N/A	1.1							
PM ₁₀	0.5	0.7	N/A	1.1							
PM _{2.5}	0.5	0.7	N/A	1.1							
CO ₂ e	11,088.8	7797.2	N/A	18,886.0							

	ANNNUAL EMISSIONS - BASELINE ACTUAL											
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION SOURCES (tpy)	FUGITIVE SOURCES (tpy)	TOTALS								
NOx	0	2.9	N/A	2.9								
VOC	29.1	0.1	82.7	111.9								
СО	69.7	1.9	N/A	71.6								
SO ₂	0	0.03	N/A	0.03								
PM	0.4	0.2	N/A	0.6								
PM ₁₀	0.4	0.2	N/A	0.6								
PM _{2.5}	0.4	0.2	N/A	0.6								
CO ₂ e	28512.7	2474.0	N/A	30986.7								

POLLUTANT	THRESHOLD	DELTA (PTE - ACTUAL)
NOx	40	10.0
VOC	40	38.4
CO	100	279.5
SO ₂	40	0.1
PM	25	0.5
PM ₁₀	15	0.5
PM _{2.5}	10	0.5
CO ₂ e	75,000	-12100.6

Table B-4 CR #1 PTA PSD Analysis

PTE

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (cfm)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR (gr/cfm)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
			PM	=	Average of data from	0.10	8,760	0.4	
Feed Slurry Drum Scrubber	CH-108	-	PM ₁₀	-	Average of data from 2/95 source test	0.10	8,760	0.4	
			PM _{2.5}	-		0.10	8,760	0.4	
			VOC	-	2/95 Source test	10.62	8,760	46.5	
Crystallizer Vent Scrubber	CM-301	_	PM	-	Average of data from	1.21	8,760	5.3	
Crystallizer Verit Scrubber	CIVI-30 I	-	PM ₁₀	-	Average of data from 12/14/04 source test	1.21	8,760	5.3	
			$PM_{2.5}$	-	12/14/04 Source test	1.21	8,760	5.3	
			PM	-	Average of data from	0.30	8,760	1.3	
Dryer Scrubber	CM-404A	-	PM ₁₀	-	Average of data from 2/95 source test	0.30	8,760	1.3	
			$PM_{2.5}$	=	2/93 300100 1031	0.30	8,760	1.3	
			PM	-	Average of data from	0.30	8,760	1.3	
Dryer Scrubber	CM-404B		PM ₁₀	-	Average of data from 2/95 source test	0.30	8,760	1.3	
			$PM_{2.5}$	=	2/93 300100 1031	0.30	8,760	1.3	
			PM	0.01	USEPA Handbook	0.42	8,760	1.9	
Day Silo Baghouse	CM-603A	4,950	PM ₁₀	0.01	USEPA Handbook	0.42	8,760	1.9	
			PM _{2.5}	0.01	USEPA Handbook	0.42	8,760	1.9	
			PM	0.01	USEPA Handbook	0.42	8,760	1.9	
Day Silo Baghouse	CM-603B	4,950	PM ₁₀	0.01	USEPA Handbook	0.42	8,760	1.9	
			PM _{2.5}	0.01	USEPA Handbook	0.42	8,760	1.9	
			PM	0.01	USEPA Handbook	0.01	8,760	0.04	
Rotary Lock A Dust Collector	CM-608A	100	PM ₁₀	0.01	USEPA Handbook	0.01	8,760	0.04	
			PM _{2.5}	0.01	USEPA Handbook	0.01	8,760	0.04	
			PM	0.01	USEPA Handbook	0.01	8,760	0.04	
Rotary Lock B Dust Collector	CM-608B	100	PM ₁₀	0.01	USEPA Handbook	0.01	8,760	0.04	
			PM _{2.5}	0.01	USEPA Handbook	0.01	8,760	0.04	

Table B-4 CR #1 PTA PSD Analysis

2010 Actuals									
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (cfm)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR (gr/cfm)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	ACTUAL OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
			PM	-	Average of data from	0.10	8,135	0.4	
Feed Slurry Drum Scrubber	CH-108	-	PM ₁₀	-	2/95 source test	0.10	8,135	0.4	
			PM _{2.5}	-		0.10	8,135	0.4	
			VOC	-	2/95 Source test	10.62	8,135	43.2	
Crystallizer Vent Scrubber	CM-301	_	PM	-	Average of data from	1.80	8,135	7.3	
	CIVI-301	-	PM ₁₀	=	12/14/04 source test	1.80	8,135	7.3	
			$PM_{2.5}$	-	12/14/04 30dicc test	1.80	8,135	7.3	
			PM	-	Average of data from	0.30	8,135	1.2	
Dryer Scrubber	CM-404A	-	PM ₁₀	-	2/95 source test	0.30	8,135	1.2	
			PM _{2.5}	-		0.30	8,135	1.2	
			PM	-	Average of data from 2/95 source test	0.30	8,135	1.2	
Dryer Scrubber	CM-404B		PM ₁₀	=		0.30	8,135	1.2	
			PM _{2.5}	-	2/33 300100 1031	0.30	8,135	1.2	
		4,950	PM	0.01	USEPA Handbook	0.42	8,135	1.7	
Day Silo Baghouse	CM-603A		PM ₁₀	0.01	USEPA Handbook	0.42	8,135	1.7	
			PM _{2.5}	0.01	USEPA Handbook	0.42	8,135	1.7	
			PM	0.01	USEPA Handbook	0.42	8,135	1.7	
Day Silo Baghouse	CM-603B	4,950	PM ₁₀	0.01	USEPA Handbook	0.42	8,135	1.7	
			PM _{2.5}	0.01	USEPA Handbook	0.42	8,135	1.7	
			PM	0.01	USEPA Handbook	0.01	8,135	0.03	
Rotary Lock A Dust Collector	CM-608A	100	PM ₁₀	0.01	USEPA Handbook	0.01	8,135	0.03	
			PM _{2.5}	0.01	USEPA Handbook	0.01	8,135	0.03	
			PM	0.01	USEPA Handbook	0.01	8,135	0.03	
Rotary Lock B Dust Collector	CM-608B	100	PM ₁₀	0.01	USEPA Handbook	0.01	8,135	0.03	
			PM _{2.5}	0.01	USEPA Handbook	0.01	8,135	0.03	

Table B-4 CR #1 PTA PSD Analysis

2011 Actuals									
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (cfm)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR (gr/cfm)	SSION FACTOR REFERENCE		ACTUAL OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
			PM	-	Average of data from	0.10	7,194	0.4	
Feed Slurry Drum Scrubber	CH-108	-	PM ₁₀	-	2/95 source test	0.10	7,194	0.4	
			PM _{2.5}	=		0.10	7,194	0.4	
			VOC	=	2/95 Source test	10.27	7,194	37.0	
Crystallizer Vent Scrubber	CM-301	_	PM	-	Average of data from	1.80	7,194	6.5	
orystamzer vent corasser	OW 00 1		PM ₁₀	-	12/14/04 source test	1.80	7,194	6.5	
			PM _{2.5}	-	12/11/01/0001001	1.80	7,194	6.5	
			PM	-	Average of data from	0.30	7,194	1.1	
Dryer Scrubber	CM-404A	-	PM ₁₀	-	2/95 source test	0.30	7,194	1.1	
			PM _{2.5}	-	2,00 000,00 1001	0.30	7,194	1.1	
			PM	-	Average of data from	0.30	7,194	1.1	
Dryer Scrubber	CM-404B		PM ₁₀	-	2/95 source test	0.30	7,194	1.1	
			PM _{2.5}	-		0.30	7,194	1.1	
			PM	0.01	USEPA Handbook	0.42	7,194	1.5	
Day Silo Baghouse	CM-603A	4,950	PM ₁₀	0.01	USEPA Handbook	0.42	7,194	1.5	
			PM _{2.5}	0.01	USEPA Handbook	0.42	7,194	1.5	
			PM	0.01	USEPA Handbook	0.42	7,194	1.5	
Day Silo Baghouse	CM-603B	4,950	PM ₁₀	0.01	USEPA Handbook	0.42	7,194	1.5	
			$PM_{2.5}$	0.01	USEPA Handbook	0.42	7,194	1.5	
			PM	0.01	USEPA Handbook	0.01	7,194	0.03	
Rotary Lock A Dust Collector	CM-608A	100	PM ₁₀	0.01	USEPA Handbook	0.01	7,194	0.03	
			PM _{2.5}	0.01	USEPA Handbook	0.01	7,194	0.03	
			PM	0.01	USEPA Handbook	0.01	7,194	0.03	
Rotary Lock B Dust Collector	CM-608B	100	PM ₁₀	0.01	USEPA Handbook	0.01	7,194	0.03	
			PM _{2.5}	0.01	USEPA Handbook	0.01	7,194	0.03	

Table B-4 CR #1 PTA PSD Analysis

ANNUAL EMISSIONS - PTE									
POLLUTANT	COMBUSTION SOURCES (tpy)	TOTALS							
NOx	0	NA	0						
VOC	46.5	NA	46.5						
CO	0	NA	0						
SO ₂	0	NA	0						
PM	12.1	NA	12.14						
PM ₁₀	12.1	NA	12.14						
PM _{2.5}	12.1	NA	12.14						

ANNUAL EMISSIONS - BASELINE ACTUAL									
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION SOURCES (tpy)	TOTALS						
NOx	0	NA	0						
VOC	40.1	NA	40.1						
CO	0	NA	0						
SO ₂	0	NA	0						
PM_9	12.9	NA	12.9						
PM ₁₀	12.9	NA	12.9						
PM _{2.5}	12.9	NA	12.9						

POLLUTANT	THRESHOLD	DELTA (PTE - ACTUAL)
NOx	40	0
VOC	40	6.4
CO	100	0
SO ₂	40	0
PM	25	-0.8
PM ₁₀	15	-0.8
PM _{2.5}	10	-0.8

Table B-5 CR #2 PTA PSD Analysis

PTE

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (lb/hr)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR (% Removal)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
			PM	99	BP Calcs based on	0.04	8,760	0.2	Maximum rate based
Feed Slurry Drum Scrubber	DH-518	4	PM ₁₀	99	2/95 test of CD101	0.04	8,760	0.2	on hourly emissions
			PM _{2.5}	99	2/95 test of OD 101	0.04	8,760	0.2	and % removal
			PM	99	BP Calcs & source	0.54	8,760	2.4	Maximum PM rates
Crystallizar Vant Sarubbar	DM-601	54	PM ₁₀	99	test of 4/98 & 12/04	0.54	8,760	2.4	based on hourly emissions and % removal
Crystallizer Vent Scrubber	DIVI-00 I	P	PM _{2.5}	99	1651 01 4/90 & 12/04	0.54	8,760	2.4	
		10.6	VOC	0	Source Test	10.62	8,760	46.5	
			PM	95	BP design calcs based on #1 PTA Scrubber	0.26	8,760	1.1	Maximum rate based
Dryer Scrubber	DM-704	5.2	PM ₁₀	95		0.26	8,760	1.1	on hourly emissions and % removal
			PM _{2.5}	95		0.26	8,760	1.1	
		A 265	PM	99.9	BP design calcs based on #1 PTA	0.27	8,760	1.2	Maximum rate based on hourly emissions and % removal
Day Silo Dust Collector	DM-797A		PM ₁₀	99.9		0.27	8,760	1.2	
			PM _{2.5}	99.9	Silo	0.27	8,760	1.2	
			PM	99.9	BP design calcs	0.27	8,760	1.2	Maximum rate based
Day Silo Dust Collector	DM-797B	265	PM ₁₀	99.9	based on #1 PTA	0.27	8,760	1.2	on hourly emissions
			PM _{2.5}	99.9	Silo	0.27	8,760	1.2	and % removal
			PM		BP Calcs	0.001	8,760	0.004	
Product Recovery Unit	MLSR-2		PM ₁₀		BP Calcs	0.001	8,760	0.004	
			PM _{2.5}		BP Calcs	0.001	8,760	0.004	

Table B-5 CR #2 PTA PSD Analysis

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (lb/hr)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR (% Removal)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
			PM	99	DD Coloo boood on	0.04	8,760	0.2	Maximum rate based
Feed Slurry Drum Scrubber	DH-518	4	PM ₁₀	99	BP Calcs based on 2/95 test of CD101	0.04	8,760	0.2	on hourly emissions
			PM _{2.5}	99	2/93 test of CD101	0.04	8,760	0.2	and % removal
			PM	99	DD Coloo 8 course	0.54	8,760	2.4	Maximum PM rates
Cryotallizar Vant Sarubbar	DM-601	54	PM ₁₀	99	BP Calcs & source test of 4/98 & 12/04 0.54 8,760 0.54 8,760	0.54	8,760	2.4	based on hourly
Crystallizer Vent Scrubber	DIVI-601		PM _{2.5}	99		8,760	2.4	emissions and %	
		10.6	VOC	0	Source Test	10.62	8,760	46.5	removal
	DM-704		PM	95	BP design calcs based on #1 PTA Scrubber	0.26	8,760	1.1	Maximum rate based
Dryer Scrubber		5.2	PM ₁₀	95		0.26	8,760	1.1	on hourly emissions and % removal
			PM _{2.5}	95		0.26	8,760	1.1	
			PM	99.9	BP design calcs based on #1 PTA	0.27	8,760	1.2	Maximum rate based on hourly emissions and % removal
Day Silo Dust Collector	DM-797A	265	PM ₁₀	99.9		0.27	8,760	1.2	
			PM _{2.5}	99.9	Silo	0.27	8,760	1.2	
			PM	99.9	BP design calcs	0.27	8,760	1.2	Maximum rate based
Day Silo Dust Collector	DM-797B	265	PM ₁₀	99.9	based on #1 PTA	0.27	8,760	1.2	on hourly emissions
·			PM _{2.5}	99.9	Silo	0.27	8,760	1.2	and % removal
Product Recovery Unit			PM		BP Calcs	0.001	8,760	0.004	
	MLSR-2		PM ₁₀		BP Calcs	0.001	8,760	0.004	
			PM _{2.5}		BP Calcs	0.001	8,760	0.004	

Table B-5 CR #2 PTA PSD Analysis

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (lb/hr)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR (% Removal)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
			PM	99	DD Color boood on	0.04	7,043	0.1	Maximum rate based
Feed Slurry Drum Scrubber	DH-518	4	PM ₁₀	99	BP Calcs based on 2/95 test of CD101	0.04	7,043	0.1	on hourly emissions
			PM _{2.5}	99	2/93 test of CD101	0.04	7,043	0.1	and % removal
			PM	99	DD Coloo 8 course	0.54	7,043	1.9	Maximum PM rates
Crustallizar Vant Carubbar	DM-601	54	PM ₁₀	99	BP Calcs & source	0.54	7,043	1.9	based on hourly
Crystallizer Vent Scrubber	DIVI-601		PM _{2.5}	99	test of 4/98 & 12/04 0.54 7,043	7,043	1.9	emissions and %	
		10.6	VOC	0	Source Test	10.62	7,043	37.4	removal
	DM-704		PM	95	BP design calcs based on #1 PTA Scrubber	0.26	7,043	0.9	Maximum rate based
Dryer Scrubber		5.2	PM ₁₀	95		0.26	7,043	0.9	on hourly emissions and % removal
			PM _{2.5}	95		0.26	7,043	0.9	
			PM	99.9	BP design calcs	0.27	7,043	0.9	Maximum rate based on hourly emissions and % removal
Day Silo Dust Collector	DM-797A	265	PM ₁₀	99.9	based on #1 PTA	0.27	7,043	0.9	
			PM _{2.5}	99.9	Silo	0.27	7,043	0.9	
			PM	99.9	BP design calcs	0.27	7,043	0.9	Maximum rate based
Day Silo Dust Collector	DM-797B	265	PM ₁₀	99.9	based on #1 PTA	0.27	7,043	0.9	on hourly emissions
•			PM _{2.5}	99.9	Silo	0.27	7,043	0.9	and % removal
		MLSR-2	PM		BP Calcs	0.001	7,043	0.004	
Product Recovery Unit	MLSR-2		PM ₁₀		BP Calcs	0.001	7,043	0.004	
			PM _{2.5}		BP Calcs	0.001	7,043	0.004	

Table B-5 CR #2 PTA PSD Analysis

ANNUAL EMISSIONS - PTE									
POLLUTANT	TOTALS								
NOx	0	NA	0						
VOC	46.5	NA	46.5						
СО	0	NA	0						
SO ₂	0	NA	0						
РМ	6.0	NA	6.0						
PM ₁₀	6.0	NA	6.0						
PM _{2.5}	6.0	NA	6.0						

ANNUAL	ANNUAL EMISSIONS - BASELINE ACTUAL									
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION SOURCES (tpy)	TOTALS							
NOx	0	NA	0							
VOC	42.0	NA	42.0							
CO	0	NA	0							
SO ₂	0	NA	0							
PM	5.4	NA	5.4							
PM ₁₀	5.4	NA	5.4							
PM _{2.5}	5.4	NA	5.4							

POLLUTANT	THRESHOLD	DELTA (PTE - ACTUAL)
NOx	40	0
VOC	40	4.6
CO	100	0
SO ₂	40	0
PM	25	0.6
PM ₁₀	15	0.6
PM _{2.5}	10	0.6

Table B-6 Cooling Towers PSD Analysis

PTE

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (gpm)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR (% Removal)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
	AT-201		PM	97	Table B-30	0.44	8,760	1.9	Reisman, Frisbie, 2002
Cooling Tower		97000	PM ₁₀	97	Table B-30	0.32	8,760	1.4	Reisman, Frisbie, 2002
			PM _{2.5}	97	Table B-30	0.001	8,760	0.004	Reisman, Frisbie, 2002
Cooling Tower	AT-202		PM	97	Table B-30	0.44	8,760	1.9	Reisman, Frisbie, 2002
		97000	PM ₁₀	97	Table B-30	0.32	8,760	1.4	Reisman, Frisbie, 2002
			PM _{2.5}	97	Table B-30	0.001	8,760	0.004	Reisman, Frisbie, 2002

2010 Actuals

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (gpm)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR (% Removal)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
	AT-201		PM	97	Table B-30	0.31	8,760	1.3	Reisman, Frisbie, 2002
Cooling Tower			PM ₁₀	97	Table B-30	0.22	8,760	1.0	Reisman, Frisbie, 2002
			PM _{2.5}	97	Table B-30	0.001	8,760	0.003	Reisman, Frisbie, 2002
		68000	PM	97	Table B-30	0.31	8,760	1.3	Reisman, Frisbie, 2002
Cooling Tower	AT-202		PM ₁₀	97	Table B-30	0.22	8,760	1.0	Reisman, Frisbie, 2002
			PM _{2.5}	97	Table B-30	0.001	8,760	0.003	Reisman, Frisbie, 2002

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (gpm)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR (% Removal)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
	AT-201	68000	PM	97	Table B-30	0.31	8,760	1.3	Reisman, Frisbie, 2002
Cooling Tower			PM ₁₀	97	Table B-30	0.22	8,760	1.0	Reisman, Frisbie, 2002
			PM _{2.5}	97	Table B-30	0.001	8,760	0.003	Reisman, Frisbie, 2002
	AT-202	68000	PM	97	Table B-30	0.31	8,760	1.3	Reisman, Frisbie, 2002
Cooling Tower			PM ₁₀	97	Table B-30	0.22	8,760	1.0	Reisman, Frisbie, 2002
			PM _{2.5}	97	Table B-30	0.001	8,760	0.003	Reisman, Frisbie, 2002

ANNU	AL EMISSIONS	- PTE	
POLLUTANT	UTANT PROCESS SOURCES (tpy)		TOTALS
NOx	0	NA	0
VOC	0	NA	0
СО	0	NA	0
SO ₂	0	NA	0
PM	3.8	NA	3.8
PM ₁₀	2.8	NA	2.8
PM _{2.5}	0.01	NA	0.01

ANNU	ANNUAL EMISSIONS - BASELINE ACTUAL								
POLLUTANT	PROCESS COMBUSTION SOURCES (tpy) (tpy)		TOTALS						
NOx	0	NA	0						
VOC	0	NA	0						
CO	0	NA	0						
SO ₂	0	NA	0						
PM	2.7	NA	2.7						
PM ₁₀	1.9	NA	1.9						
PM _{2.5}	0.01	NA	0.01						

POLLUTANT	THRESHOLD	DELTA (PTE - ACTUAL)
NOx	40	0
VOC	40	0
CO	100	0
SO ₂	40	0
PM	25	1.1
PM ₁₀	15	0.8
PM _{2.5}	10	0.003

Table B-7 Fugitive Emissions

Post-Project (After BACT)

	VALVES, LIQUID	VALVES, GAS	FLANGES DRAINS, VENTS & OTHERS	PUMPS	RELIEF VALVES	AGITATORS	COMPRESSORS	TOTAL HAPS EMISSIONS (lb/yr)	TOTAL STREAM (lb/yr)	TOTAL STREAM (tpy)
EF, lb/hr/item: (NSPS)	0.00347	0.00434	0.00270	0.01360	0.08942	0.01360	0.01360		() ,	(12)
EF, lb/hr/item: (HON)	0.00107	0.00105	0.00028	0.01097	0.02751	0.01097	0.01097			
#1 OX Unit (HON)	218	0	398	4	3	1	0	1266.82	4223	2.11
#1 OX (NSPS as HON)	2023	85	4215	34	17	18	5	494.73	39676	19.84
#2 OX (HON)	244	0	534	3	4	1	0	1485.18	4949	2.47
#2 OX (NSPS as HON)	1960	202	4325	37	13	15	4	491.14	39388	19.69
OSBL (HON)	303	1	588	6	4	0	0	5834.33	5834	2.92
Total	4748.10	288.11	10060.10	84.02	41.12	35.02	9.02	9,572	94,070	47.04

Project LDAR Impact 10.00%

	USEPA Factor		EF		Effectiveness Factor	
Factors	kg/hr	lb/kg	<u>lb/hr</u>		<u>HON</u>	NSPS
Valves, Liquid	0.00403	2.204623	0.00888		0.88	0.61
Valves, Gas	0.00597	2.204623	0.01316		0.92	0.67
Flanges , Drains, Vents, Other	0.00183	2.204623	0.00403		0.93	0.33
Pumps	0.01990	2.204623	0.04387		0.75	0.69
Relief Valves	0.10400	2.204623	0.22928		0.88	0.61
Agitators	0.01990	2.204623	0.04387		0.75	0.69
Compressors	0.01990	2.204623	0.04387		0.75	0.69
Sample Connection	0.01500	2.204623	0.03307		0.93	0.33

USEPA Factor is based on table 2-1 from USEPA Report of 1995 on LDAR Emission factors - Average Emission Factors Effectiveness factors - HON are based on Table 5-9 from 1995 USEPA Report, NSPS from EIIP Volume II, Table 4.2.2

Pre-Project

	VALVES, LIQUID	VALVES, GAS	FLANGES DRAINS, VENTS	PUMPS	RELIEF VALVES	AGITATORS	COMPRESSORS	TOTAL HAPS EMISSIONS	TOTAL STREAM	TOTAL STREAM
			& OTHERS					(lb/yr)	(lb/yr)	(tpy)
EF, lb/hr/item: (NSPS)	0.00347	0.00434	0.00270	0.01360	0.08942	0.01360	0.01360			
EF, lb/hr/item: (HON)	0.00107	0.00105	0.00028	0.01097	0.02751	0.01097	0.01097			
#1 OX Unit (HON)	198	0	362	4	3	1	0	1184.47	3948	1.97
#1 OX (NSPS)	1839	77	3832	34	17	18	5	2114.70	169595	84.80
#2 OX (HON)	222	0	485	3	4	1	0	1386.95	4622	2.31
#2 OX (NSPS)	1782	184	3932	37	13	15	4	2132.86	171052	85.53
OSBL (HON)	303	1	588	6	4	0	0	5834.33	5834	2.92
Total	4344.00	262.01	9199.00	84.02	41.12	35.02	9.02	12,653	355,051	177.53

Table B-8
Tank Farm (Unmodified/Debottlecked)

PTE

EQUIPMENT DESCRIPTION	EQUIPMENT ID NO.	STACK ID NO.	QUANTITY (gallons)	STANDING LOSS (lb/yr)	WORKING LOSS (lb/yr)	TOTAL LOSS (lb/yr)	ANNUAL TOTAL (tpy)
Denovadene	AF- 101	TK-1	108,974,400	694.89	172.20	867.09	0.43
Paraxylene Tank	AF- 102	TK-2	108,974,400	694.89	172.20	867.09	0.43
ranik	AF- 103	TK-3	108,974,400	694.89	172.20	867.09	0.43
TOTALS			326,923,200	2,084.67	516.60	2,601.27	1.30

2010 Actuals

EQUIPMENT DESCRIPTION	EQUIPMENT ID NO.	STACK ID NO.	QUANTITY (gallons)	STANDING LOSS (lb/yr)	WORKING LOSS (lb/yr)	TOTAL LOSS (lb/yr)	ANNUAL TOTAL (tpy)
Damandana	AF- 101	TK-1	78,733,394	694.89	124.41	819.30	0.41
Paraxylene Tank	AF- 102	TK-2	78,733,394	694.89	124.41	819.30	0.41
rank	AF- 103	TK-3	78,733,394	694.89	124.41	819.30	0.41
TOTALS			236,200,182	2,084.67	373.23	2,457.90	1.23

EQUIPMENT DESCRIPTION	EQUIPMENT ID NO.	STACK ID NO.	QUANTITY (gallons)	STANDING LOSS (lb/yr)	WORKING LOSS (lb/yr)	TOTAL LOSS (lb/yr)	ANNUAL TOTAL (tpy)
Develope	AF- 101	TK-1	73,912,058	694.89	116.79	811.68	0.41
Paraxylene Tank	AF- 102	TK-2	73,912,058	694.89	116.79	811.68	0.41
rank	AF- 103	TK-3	73,912,058	694.89	116.79	811.68	0.41
TOTALS			221,736,174	2,084.67	350.37	2,435.04	1.22

	PTE	Actuals	Delta
VOC	1.30	1.22	0.08

Table B-9
CR Shipping (Unmodified/Debottlenecked)

PTE

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	STACK ID NUMBER	MAXIMUM RATE (cfm)	POLLUTANT(S) EMITTED	POLLUTANT EMISSION FACTOR (gr/cfm)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hpy)	PTE EMISSIONS (tpy)	COMMENTS
				PM	0.01	USEPA Book	0.42	8,760	1.86	
Storage Silo A Baghouse	CM-701A	SL-1	4,950	PM ₁₀	0.01	USEPA Book	0.42	8,760	1.86	
				PM _{2.5}	0.01	USEPA Book	0.42	8,760	1.86	
				PM	0.01	USEPA Book	0.42	8,760	1.86	
Storage Silo B Baghouse	CM-701B	SL-2	4,950	PM ₁₀	0.01	USEPA Book	0.42	8,760	1.86	
				PM _{2.5}	0.01	USEPA Book	0.42	8,760	1.86	
				PM	0.01	USEPA Book	0.42	8,760	1.86	EPA/625/6-91/014:
Storage Silo C Baghouse	CM-701C	SL-3	4,950	PM ₁₀	0.01	USEPA Book	0.42	8,760	1.86	Control Technologies for
				PM _{2.5}	0.01	USEPA Book	0.42	8,760	1.86	HAPs
				PM	0.01	USEPA Book	0.42	8,760	1.86	
Storage Silo D Baghouse	CM-701D	SL-4	4,950	PM ₁₀	0.01	USEPA Book	0.42	8,760	1.86	
				PM _{2.5}	0.01	USEPA Book	0.42	8,760	1.86	
				PM	0.01	USEPA Book	0.42	8,760	1.86	
Storage Silo E Baghouse	CM-701E	SL-5	4,950	PM ₁₀	0.01	USEPA Book	0.42	8,760	1.86	
				PM _{2.5}	0.01	USEPA Book	0.42	8,760	1.86	
				PM	-	Average of	0.48	8,760	2.10	
Storage Silo F Baghouse	CM-720 A/B	SL-6A/B		PM ₁₀	-	06/11/02	0.48	8,760	2.10	
				PM _{2.5}	-	source test	0.48	8,760	2.10	
				PM	0.01	USEPA Book	0.10	8,760	0.45	
Loading Spout A Dust Collector	CP-705A	SL-7	1,200	PM ₁₀	0.01	USEPA Book	0.10	8,760	0.45	
				PM _{2.5}	0.01	USEPA Book	0.10	8,760	0.45	
				PM	0.01	USEPA Book	0.10	8,760	0.45	EPA/625/6-91/014:
Loading Spout B Dust Collcetor	CP-705B	SL-8	1,200	PM ₁₀	0.01	USEPA Book	0.10	8,760	0.45	Control Technologies for
				PM _{2.5}	0.01	USEPA Book	0.10	8,760	0.45	HAPs
				PM	0.01	USEPA Book	0.10	8,760	0.45	
Loading Spout C Dust Collector	CP-705C	SL-9	1,200	PM ₁₀	0.01	USEPA Book	0.10	8,760	0.45	
				PM _{2.5}	0.01	USEPA Book	0.10	8,760	0.45	
				PM	-	BP Calcs	0.20	8,760	0.88	
Bulk Truck Loading Bag Filter	CM-722	SL-10		PM ₁₀	-	BP Calcs	0.20	8,760	0.88	
				PM _{2.5}	-	BP Calcs	0.20	8,760	0.88	

Table B-9
CR Shipping (Unmodified/Debottlenecked)

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	STACK ID NUMBER	MAXIMUM RATE (cfm)	POLLUTANT(S) EMITTED	POLLUTANT EMISSION FACTOR (gr/cfm)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hpy)	PTE EMISSIONS (tpy)	COMMENTS
				PM	0.01	USEPA Book	0.42	8,760	1.86	
Storage Silo A Baghouse	CM-701A	SL-1	4,950	PM ₁₀	0.01	USEPA Book	0.42	8,760	1.86	
				PM _{2.5}	0.01	USEPA Book	0.42	8,760	1.86	
				PM	0.01	USEPA Book	0.42	8,760	1.86	
Storage Silo B Baghouse	CM-701B	SL-2	4,950	PM ₁₀	0.01	USEPA Book	0.42	8,760	1.86	
				PM _{2.5}	0.01	USEPA Book	0.42	8,760	1.86	
				PM	0.01	USEPA Book	0.42	8,760	1.86	EPA/625/6-91/014:
Storage Silo C Baghouse	CM-701C	SL-3	4,950	PM ₁₀	0.01	USEPA Book	0.42	8,760	1.86	Control Technologies for
				PM _{2.5}	0.01	USEPA Book	0.42	8,760	1.86	HAPs
				PM	0.01	USEPA Book	0.42	8,760	1.86	
Storage Silo D Baghouse	CM-701D	SL-4	4,950	PM ₁₀	0.01	USEPA Book	0.42	8,760	1.86	
				PM _{2.5}	0.01	USEPA Book	0.42	8,760	1.86	
				PM	0.01	USEPA Book	0.42	8,760	1.86	
Storage Silo E Baghouse	CM-701E	SL-5	4,950	PM ₁₀	0.01	USEPA Book	0.42	8,760	1.86	
				PM _{2.5}	0.01	USEPA Book	0.42	8,760	1.86	
				PM	-	Based on	0.48	8,760	2.10	
Storage Silo F Baghouse	CM-720 A/B	SL-6A/B		PM ₁₀	-	06/11/02	0.48	8,760	2.10	
				PM _{2.5}	-	source test	0.48	8,760	2.10	
				PM	0.01	USEPA Book	0.10	5,200	0.27	
Loading Spout A Dust Collector	CP-705A	SL-7	1,200	PM ₁₀	0.01	USEPA Book	0.10	5,200	0.27	
				PM _{2.5}	0.01	USEPA Book	0.10	5,200	0.27	
				PM	0.01	USEPA Book	0.10	5,200	0.27	EPA/625/6-91/014:
Loading Spout B Dust Collcetor	CP-705B	SL-8	1,200	PM ₁₀	0.01	USEPA Book	0.10	5,200	0.27	Control Technologies for
				PM _{2.5}	0.01	USEPA Book	0.10	5,200	0.27	HAPs
				PM	0.01	USEPA Book	0.10	5,200	0.27	
Loading Spout C Dust Collector	CP-705C	SL-9	1,200	PM ₁₀	0.01	USEPA Book	0.10	5,200	0.27	
				PM _{2.5}	0.01	USEPA Book	0.10	5,200	0.27	
				PM	-	BP Calcs	0.20	5,200	0.52	
Bulk Truck Loading Bag Filter	CM-722	SL-10		PM ₁₀	-	BP Calcs	0.20	5,200	0.52	
				PM _{2.5}	-	BP Calcs	0.20	5,200	0.52	

Table B-9 CR Shipping (Unmodified/Debottlenecked)

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	STACK ID NUMBER	MAXIMUM RATE (cfm)	POLLUTANT(S) EMITTED	POLLUTANT EMISSION FACTOR (gr/cfm)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hpy)	PTE EMISSIONS (tpy)	COMMENTS
				PM	0.01	USEPA Book	0.42	8,760	1.86	
Storage Silo A Baghouse	CM-701A	SL-1	4,950	PM ₁₀	0.01	USEPA Book	0.42	8,760	1.86	
				PM _{2.5}	0.01	USEPA Book	0.42	8,760	1.86	
				PM	0.01	USEPA Book	0.42	8,760	1.86	
Storage Silo B Baghouse	CM-701B	SL-2	4,950	PM ₁₀	0.01	USEPA Book	0.42	8,760	1.86	
				PM _{2.5}	0.01	USEPA Book	0.42	8,760	1.86	
				PM	0.01	USEPA Book	0.42	8,760	1.86	EPA/625/6-91/014:
Storage Silo C Baghouse	CM-701C	SL-3	4,950	PM ₁₀	0.01	USEPA Book	0.42	8,760	1.86	Control Technologies for
				PM _{2.5}	0.01	USEPA Book	0.42	8,760	1.86	HAPs
				PM	0.01	USEPA Book	0.42	8,760	1.86	
Storage Silo D Baghouse	CM-701D	SL-4	4,950	PM ₁₀	0.01	USEPA Book	0.42	8,760	1.86	
				PM _{2.5}	0.01	USEPA Book	0.42	8,760	1.86	
				PM	0.01	USEPA Book	0.42	8,760	1.86	
Storage Silo E Baghouse	CM-701E	SL-5	4,950	PM ₁₀	0.01	USEPA Book	0.42	8,760	1.86	
				PM _{2.5}	0.01	USEPA Book	0.42	8,760	1.86	
				PM	-	Based on	0.48	8,760	2.10	
Storage Silo F Baghouse	CM-720 A/B	SL-6A/B		PM ₁₀	-	06/11/02	0.48	8,760	2.10	
				PM _{2.5}	-	source test	0.48	8,760	2.10	
				PM	0.01	USEPA Book	0.10	3,500	0.18	
Loading Spout A Dust Collector	CP-705A	SL-7	1,200	PM ₁₀	0.01	USEPA Book	0.10	3,500	0.18	
				PM _{2.5}	0.01	USEPA Book	0.10	3,500	0.18	
				PM	0.01	USEPA Book	0.10	3,500	0.18	EPA/625/6-91/014:
Loading Spout B Dust Collcetor	CP-705B	SL-8	1,200	PM ₁₀	0.01	USEPA Book	0.10	3,500	0.18	Control Technologies for
				PM _{2.5}	0.01	USEPA Book	0.10	3,500	0.18	HAPs
				PM	0.01	USEPA Book	0.10	3,500	0.18	
Loading Spout C Dust Collector	CP-705C	SL-9	1,200	PM ₁₀	0.01	USEPA Book	0.10	3,500	0.18	
				PM _{2.5}	0.01	USEPA Book	0.10	3,500	0.18	
				PM	-	BP Calcs	0.20	3,500	0.35	
Bulk Truck Loading Bag Filter	CM-722	SL-10		PM ₁₀	-	BP Calcs	0.20	3,500	0.35]
				PM _{2.5}	-	BP Calcs	0.20	3,500	0.35	

SHIPPING AND LOADING PTE EMISSIONS								
POLLUTANT	PROCESS SOURCES (tpy)	TOTALS						
PM	9.91	9.91						
PM ₁₀	9.91	9.91						
PM _{2.5}	9.91	9.91						

S&L BASELINE ACTUAL EMISSIONS							
POLLUTANT	PROCESS SOURCES (tpy)	TOTALS					
PM	8.78	8.78					
PM ₁₀	8.78	8.78					
PM _{2.5}	8.78	8.78					

POLLUTANT	THRESHOLD	DELTA (PTE - ACTUAL)
PM	25	1.12
PM ₁₀	15	1.12
PM _{2.5}	10	1.12

Table B-10 Incremental Boiler Steam Production

Emission Equipment
Equipment ID Number
Stack ID No.

Boiler 3 or 4 350 - A or B U-10 or 11

		NATURAL GAS						
MAXIMUM FIRE RATE	POLLUTANT EMITTED	AP-42 EF (lb/MMscf)	NG EF (lb/MMBtu)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	OPERATE (hrs/yr)	ANNUAL EMISSION (tpy)	COMMENTS
49.30	NOx		0.0800	Vendor Data	3.944	8,760	17.28	
	VOC	5.5	0.0054	AP-42 1.4 (7/98)	0.266	8,760	1.16	
	СО	84	0.0824	AP-42 1.4 (7/98)	4.060	8,760	17.78	*Boiler has firm
,hr	SO ₂	0.6	0.0006	AP-42 1.4 (7/98)	0.029	8,760	0.13	gas and only
MMBtu/hr	PM	5.1	0.0050	Vendor Data	0.247	8,760	1.08	burns oil in force
≥	PM ₁₀	5.1	0.0050	Vendor Data	0.247	8,760	1.08	majeur.
	PM _{2.5}	5.1	0.0050	Vendor Data	0.247	8,760	1.08]
	CO ₂ e		117	USEPA Data	5,768.26	8,760	25,265	

	INCREMENTAL STEAM PRODUCTION								
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION SOURCES (tpy)	TOTALS (tpy)						
NOx	N/A	17.28	17.28						
VOC	N/A	1.16	1.16						
CO	N/A	17.78	17.78						
SO ₂	N/A	0.13	0.13						
PM	N/A	1.08	1.08						
PM ₁₀	N/A	1.08	1.08						
PM _{2.5}	N/A	1.08	1.08						
CO₂e	N/A	25,264.98	25,265						

Incremental Process Steam Usage 40 M lbs/hr

Incremental Turbine Steam Usage 0.41

Incremental Fuel Burned 1220.00 Btu/lb of steam

Fuel 49.30 MMBtu/hr

Assume fuel is gas since asked to be gas boiler for MACT

Table B-11
Post-Project Facility-Wide Controlled Emissions

Controlled Emissions - Modified Units (tpy)

POLLUTANTS	CR #1 OX	CR #2 OX	CR #1 PTA	CR #2 PTA	COOLING TOWER	TOTAL
NOx	0.5	12.9	0	0	0	13.4
VOC	157.0	150.3	46.5	46.5	0	400.3
CO	403.1	351.1	0	0	0	754.2
SO ₂	0.03	0.1	0	0	0	0.2
PM	6.6	1.1	12.1	6.0	3.8	29.7
PM ₁₀	6.6	1.1	12.1	6.0	2.8	28.7
PM _{2.5}	6.6	1.1	12.1	6.0	0.01	25.9
CO ₂ e	42,947	18,886	0	0	0	61,833

Controlled Emissions - Unmodified Units (tpy)

POLLUTANTS	SHIP & LOAD	UTILITY	WWT	TOTAL
NOx	0	311.2	0	311.2
VOC	0	21.2	69	89.8
CO	0	286.1	0	286.1
SO ₂	0	188.9	0	188.9
PM	13.6	33.8	0	47.4
PM ₁₀	13.6	30.7	0	44.3
PM _{2.5}	13.6	28.4	0	42.0
CO ₂ e	0	418,175	0	418,174.8

Facility-Wide - Post Project (tpy)

Tuomity Triad Tuoti Tuoti (ipy)								
POLLUTANTS	MODIFIED UNITS	UNMODIFIED UNITS	FACILITY-WIDE TOTAL					
NOx	13.4	311.2	324.6					
VOC	400.3	89.8	490.2					
CO	754.2	286.1	1040.3					
SO ₂	0.2	188.9	189.1					
PM	29.7	47.4	77.1					
PM ₁₀	28.7	44.3	73.0					
PM _{2.5}	25.9	42.0	67.9					
CO ₂ e	61,833	418,175	480,008					

Uncontrolled Emissions

Table B-12
Facility Uncontrolled Pre- and Post-Project PTE EmissionsSummary

Modified Units Post-Project Uncontrolled Emissions (tpy)

POLLUTANTS	CR #1 OX	CR #2 OX	CR #1 PTA	CR #2 PTA	COOLING TOWER	TOTAL
NOx	45.5	119.2	0	0	0	164.7
VOC	1,276.3	1,020.5	46.5	46.4	0	2,389.7
CO	7,715.4	6,617.9	0	0	0	14,333.3
SO ₂	3.0	1.9	0	0	0	4.9
PM	9.8	49.2	1,215.8	2598.7	127.6	4,001.0
PM ₁₀	9.8	49.2	1,215.8	2598.7	92.6	3,966.0
PM _{2.5}	9.8	49.2	1,215.8	2598.7	0.3	3,873.7
CO ₂ e	43,543	20,706	0	0	0	64,249

Modified Units Pre-Project Uncontrolled Emissions (tpy)

POLLUTANTS	CR #1 OX	CR #2 OX	CR #1 PTA	CR #2 PTA	COOLING TOWER	TOTAL
NOx	45.5	119.2	0	0	0	164.7
VOC	1,325.3	1,008.8	30.7	30.7	0.0	2,395.4
CO	10,210.9	6,616.9	0	0	0	16,827.7
SO ₂	3.0	1.9	0	0	0	4.9
PM	9.8	49.2	1,474.2	2,598.7	89.4	4,221.3
PM ₁₀	9.8	49.2	1,474.2	2,598.7	64.9	4,196.7
PM _{2.5}	9.8	49.2	1,474.2	2,598.7	0.2	4,132.0
CO ₂ e	49,315	20,706	0	0	0	70,021

Uncontrolled Facility-Wide Totals - Post-Project

Uncontrolled Facility-Wide Totals - Pre-Project

POLLUTANTS	MODIFIED	UNMODIFIED	TOTAL	PRE	UNMODIFIED	TOTAL
NOx	164.7	311.2	475.9	164.7	311.2	475.9
VOC	2,389.7	89.8	2,479.5	2,395.4	89.8	2,485.2
CO	14,333.3	286.1	14,619.4	16,827.7	286.1	17,113.9
SO ₂	4.9	188.9	193.8	4.9	188.9	193.8
PM	4,001.0	1,396.0	5,396.9	4,221.3	1,396.0	5,617.2
PM ₁₀	3,966.0	1,392.9	5,359.0	4,196.7	1,392.9	5,589.7
PM _{2.5}	3,873.7	1,390.7	5,264.4	4,132.0	1,390.7	5,522.7
CO ₂ e	64,249	418,175	482,424	70,021.2	418,175	488,196

Table B-13
CR #1 OX Uncontrolled Pre- and Post-Project PTE Emissions

PTE - Uncontrolled Post-Project

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (HP)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR	UNITS	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	OPERATING HOURS (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
			NOx	0.031	lb/hp-hr	AP-42 3.3 (10/96)	10.385	8,760	45.5	
			VOC	0.00251	lb/hp-hr	AP-42 3.3 (10/96)	0.842	8,760	3.7	
			CO	0.00668	lb/hp-hr	AP-42 3.3 (10/96)	2.238	8,760	9.8	
Emergency Generator #2	BM-1201	335	SO ₂	0.00205	lb/hp-hr	AP-42 3.3 (10/96)	0.687	8,760	3.0	Diesel Fuel Sulfur = 0.05%.
Emergency Generator #2	DIVI-1201	333	PM	0.0022	lb/hp-hr	AP-42 3.3 (10/96)	0.737	8,760	3.2	Diesei Fuel Sullul = 0.05%,
			PM ₁₀	0.0022	lb/hp-hr	AP-42 3.3 (10/96)	0.737	8,760	3.2	
			PM _{2.5}	0.0022	lb/hp-hr	AP-42 3.3 (10/96)	0.737	8,760	3.2	
			CO ₂ e	163.6	lb/MMBtu	USEPA Data	137.634	8,760	602.8	
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (lbs/hr)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR	UNITS	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	OPERATING HOURS (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
		234	VOC	0.0	% Removal	Based on controlled &	234.00	8,760	1024.9	Assume 0 Removal for
HPVGTS	HPVGTS-1	1755	CO	0.0	% Removal	efficiency	1755.00	8,760	7687.6	control device
		9510.6	CO ₂ e	0	% Removal	emciency	9510.6	8,760	41700.0	control device
		9.6	VOC			D d i b d	9.6	8,760	42.0	
Low Pressure Absorber	BT-603	4.1	СО			Recovery device so based on controlled emissions	4.1	8,760	18.0	Recovery Device
		283.0	CO ₂ e			or controlled emissions	283.0	8,760	1239.9	
CRU Extraction Drum	BD-625	CRU	VOC							
CRU Surge Drum	BD-631	removed	VOC							CRU is being removed
CRU Waste Slurry Drum	BD-632	Tomovou	VOC							
			PM	0	% Removal	Based on controlled &	1.50	8,760	6.6	Assume 0 Removal for
Silo Scrubber	BT-501		PM ₁₀	0.0	% Removal	efficiency	1.50	8,760	6.6	control device
			PM _{2.5}	0	% Removal	omolorioy	1.50	8,760	6.6	CONTROL COVICE
CRU Evaporator Overhd Condenser	BE-645	CRU removed	voc							CRU being removed
		Vent	VOC							
DHT Ovhd Scrubber	BT-702	Removed	СО							Vent Removed
		Removed	CO ₂ e							
Process Fugitives			VOC			USEPA LDAR EF	46.9	8,760	205.6	No LDAR program

Table B-13
CR #1 OX Uncontrolled Pre- and Post-Project PTE Emissions

PTE - Uncontrolled Pre-Project

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM FIRE RATE (HP)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR	UNITS	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	UNCONTROLLED OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
			NOx	0.031	lb/hp-hr	AP-42 3.3 (10/96)	10.385	8,760	45.5	
			VOC	0.00251	lb/hp-hr	AP-42 3.3 (10/96)	0.842	8,760	3.7	1
			CO	0.00668	lb/hp-hr	AP-42 3.3 (10/96)	2.238	8,760	9.8	1
Emergency Generator #2	BM-1201	335	SO ₂	0.00205	lb/hp-hr	AP-42 3.3 (10/96)	0.687	8,760	3.0	Diesel Fuel Sulfur = 0.05%.
Emergency Generator #2	DIVI-1201	333	PM	0.0022	lb/hp-hr	AP-42 3.3 (10/96)	0.737	8,760	3.2	Diesei Fuel Sullul = 0.05%,
			PM ₁₀	0.0022	lb/hp-hr	AP-42 3.3 (10/96)	0.737	8,760	3.2	1
			PM _{2.5}	0.0022	lb/hp-hr	AP-42 3.3 (10/96)	0.737	8,760	3.2	
			CO ₂ e	163.6	lb/MMBtu	USEPA Data	137.634	8,760	602.8	
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (lbs/hr)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR	UNITS	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	OPERATING HOURS (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
		131	VOC	0.0	% Removal	Based on controlled &	131.00	8,760	573.8	Assume 0 Removal for
HPVGTS	HPVGTS-1	2233	CO	0.0	% Removal	efficiency	2233.00	8,760	9781.2	control device
		10000.0	CO₂e	0	% Removal	eniciency	10000.0	8,760	43843.6	control device
		20	VOC			Danis da	20.00	8,760	87.6	
Low Pressure Absorber	BT-603	9.0	CO			Recovery device so based on controlled emissions	9.00	8,760	39.8	Recovery Device
		400.0	CO ₂ e			on controlled enticolorie	400.0	8,760	1752.4	
CRU Extraction Drum	BD-625		VOC			BP Calcs	1.0	8,760	4.4	
CRU Surge Drum	BD-631		VOC			BP Calcs	4.0	8,760	17.5	CRU is being removed
CRU Waste Slurry Drum	BD-632		VOC			BP Calcs	0.003	8,760	0.01	
			PM	0	% Removal	Based on controlled &	1.50	8,760	6.6	Assume 0 Removal for
Silo Scrubber	BT-501		PM ₁₀	0.0	% Removal	efficiency	1.50	8,760	6.6	control device
			PM _{2.5}	0	% Removal	omolorioy	1.50	8,760	6.6	control device
CRU Evaporator Overhd Condenser	BE-645	CRU removed	voc				0.3	8,760	1.3	CRU being removed
		Vent	VOC				60.0	8,760	262.8	
DHT Ovhd Scrubber	BT-702	Removed	CO				87.0	8,760	380.0	Vent Removed
		Removed	CO ₂ e				711.4	8,760	3115.9	
Process Fugitives			VOC			USEPA LDAR EF	42.7	8,760	187.1	No LDAR program

TOTAL POS	ST PROJECT E	MISSIONS - #1 C	X PTE (tpy)		
POLLUTANT	PROCESS SOURCES	COMBUSTION SOURCES	FUGITIVE SOURCES	TOTALS	
NOx	0.0	45.5	N/A	45.5	
VOC	1067.0	3.7	205.6	1276.3	
CO	7705.6	9.8	N/A	7715.4	
SO ₂	0.0	3.0	N/A	3.0	
PM	6.6	3.2	N/A	9.8	
PM ₁₀	6.6	3.2	N/A	9.8	
PM _{2.5}	6.6	3.2	N/A	9.8	
CO₂e	42,940.0	602.8	N/A	43,542.8	

	TOTAL PRE P	ROJECT EMISSION	S - #1 OX PTE (tpy)
POLLUTANT	PROCESS SOURCES	COMBUSTION SOURCES	FUGITIVE SOURCES	TOTALS
NOx	0.0	45.5	N/A	45.5
VOC	1134.5	3.7	187.1	1325.3
CO	10201.1	9.8	N/A	10210.9
SO ₂	0.0	3.0	N/A	3.0
PM	6.6	3.2	N/A	9.8
PM ₁₀	6.6	3.2	N/A	9.8
PM _{2.5}	6.6	3.2	N/A	9.8
CO₂e	48,711.9	602.8	N/A	49,314.8

Table B-14
#2 OX Uncontrolled Pre- and Post-Project PTE Emissions

PTE - Uncontrolled Post-Project

				NATURAL GAS DIESEL FUEL (SULFUR = 0.05%)							%)			
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM FIRE RATE	POLLUTANT EMITTED	AP-42 1.4 FACTOR (Ib/MM scf)	NATURAL GAS EF (lb/MMBtu)	HOURLY EMISSION (lb/hr)	UNCONTROL OPERATE (hpy)	ANNUAL EMISSION (tpy)	AP-42 FACTOR (lb/hp-hr)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	UNCONTROL OPERATE (hpy)	ANNUAL EMISSION (tpy) - Oil	
			NOx						0.024	AP-42 3.4 (10/96)	25.75	8,760	112.77	
		1072.8	VOC						0.000642	AP-42 3.4 (10/96)	0.69	8,760	3.01	
			CO						0.0055	AP-42 3.4 (10/96)	5.90	8,760	25.84	
Emergency Generator #3	DM-135		SO ₂						0.00040	AP-42 3.4 (10/96)	0.43	8,760	1.90	
zmergeney contention we	D.III 100		PM						0.0007	AP-42 3.4 (10/96)	0.75	8,760	3.29	
		hp	PM ₁₀						0.0007	AP-42 3.4 (10/96)	0.75	8,760	3.29	
			PM _{2.5}						0.0007	AP-42 3.4 (10/96)	0.75	8,760	3.29	
			CO₂e						163.6	lb/MMBtu-USEPA	440.76	8,760	1930.52	
			NOx	100	0.098	1.47	8,760	6.4						
		15.0	VOC	5.5	0.005	0.08	8,760	0.4						
			CO	84	0.082	1.24	8,760	5.4						
HPVGTS Heater	DB-1813		SO ₂	0.6	0.001	0.01	8,760	0.04						
THE VOTO TICALO	DD 1010		PM	7.6	0.007	0.11	8,760	0.5						
		MMBtu/hr	PM ₁₀	7.6	0.007	0.11	8,760	0.5						
			PM _{2.5}	7.6	0.007	0.11	8,760	0.5						
			CO₂e		117.000	1,755.00	8,760	7,687.0						
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (lb/hr)	POLLUTANT EMITTED	POLLUTANT EF (% Removal)	EMISSION FACTOR REFERENCE	HOURLY EMISSION (lb/hr)	PERMIT OPERATE (hpy)	ANNUAL EMISSION (tpy)		С	OMMENTS			
	DR-1814/ DT-	175	VOC	0%	Decedes controlled 9	175.00	8,760	766.5						
HPVGTS	1821	1500	CO	0%	Based on controlled & efficiency	1,500.2	8,760	6,571.5		Assume 0 Ren	noval for control	devic		
	1021	2300	CO ₂ e	0	eniciency	2,300	8,760	10,074.0						
		8.9	VOC			8.85	8,760	38.8						
Low Pressure Absorber	DT-302	3.5	CO		Recovery device so based on controlled emissions	3.47	8,760	15.2	Recovery Device	e				
		231.7	CO ₂ e		on controlled enticelene	231.7	8,760	1,014.9						
			PM	0	Based on controlled &	10.37	8,760	45.4						
Intermediate Silo Scrubber	DT-500	10.4	PM ₁₀	0	efficiency	10.37	8,760	45.4		Assume 0 Ren	noval for control	devic		
			PM _{2.5}	0	cincional	10.37	8,760	45.4						
CRU Extraction Drum	DD-412		VOC											
CRU Waste Slurry Drum	DD-413	CRU removed	VOC						CRU is being removed					
CRU Mother Liquor Drum	DD-414	CIVO TETHOVEG	VOC											
CRU Evaporation Drum	DE-416		VOC											
Process Fugitives			VOC		USEPA LDAR EF	48.38	8,760	211.9		Assumes	No LDAR progra	m		

Table B-14
#2 OX Uncontrolled Pre- and Post-Project PTE Emissions

PTE - Uncontrolled Pre-Project

1 TE - Official folied 1 Te-1					NATURAL GAS					DIESEL FUE	L (SULFUR = 0.05	%)		
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM FIRE RATE	POLLUTANT EMITTED	AP-42 1.4 FACTOR (Ib/MM scf)	NATURAL GAS EF (lb/MMBtu)	HOURLY EMISSION (lb/hr)	UNCONTROL OPERATE (hpy)	ANNUAL EMISSION (tpy)	AP-42 FACTOR (lb/hp-hr)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	UNCONTROL OPERATE (hpy)	ANNUAL EMISSION (tpy) - Oil	
			NOx						0.024	AP-42 3.4 (10/96)	25.75	8,760	112.77	
		1072.8	VOC						0.000642	AP-42 3.4 (10/96)	0.69	8,760	3.01	
			CO						0.0055	AP-42 3.4 (10/96)	5.90	8,760	25.84	
Emergency Generator #3	DM-135		SO ₂						0.00040	AP-42 3.4 (10/96)	0.43	8,760	1.90	
zmergeney contrate: "c	2 100		PM						0.0007	AP-42 3.4 (10/96)	0.75	8,760	3.29	
		hp	PM ₁₀						0.0007	AP-42 3.4 (10/96)	0.75	8,760	3.29	
			PM _{2.5}						0.0007	AP-42 3.4 (10/96)	0.75	8,760	3.29	
			CO₂e						163.6	lb/MMBtu-USEPA	440.76	8,760	1930.52	
			NOx	100	0.098	1.47	8,760	6.4						
		15.0	VOC	5.5	0.005	0.08	8,760	0.4						
			CO	84	0.082	1.24	8,760	5.4						
HPVGTS Heater	DB-1813		SO ₂	0.6	0.001	0.01	8,760	0.04						
TH VOTO HOUSE	DD 1010		PM	7.6	0.007	0.11	8,760	0.5						
		MMBtu/hr	PM ₁₀	7.6	0.007	0.11	8,760	0.5						
			PM _{2.5}	7.6	0.007	0.11	8,760	0.5						
			CO₂e		117.000	1,755.00	8,760	7,687.0						
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (lb/hr)	POLLUTANT EMITTED	POLLUTANT EF (% Removal)	EMISSION FACTOR REFERENCE	HOURLY EMISSION (lb/hr)	PERMIT OPERATE (hpy)	ANNUAL EMISSION (tpy)		С	OMMENTS			
	DR-1814/ DT-	175	VOC	0%	Decedes controlled 9	175.0	8,760	766.5						
HPVGTS	1821	1500	CO	0%	Based on controlled & efficiency	1,500.0	8,760	6,570.4		Assume 0 Ren	noval for control	devic		
	1021	2300	CO ₂ e	0	cilicioney	2,300	8,760	10,074.0						
		8.9	VOC		D	8.85	8,760	38.8						
Low Pressure Absorber	DT-302	3.5	CO		Recovery device so based on controlled emissions	3.47	8,760	15.2	Recovery Device	Э				
		231.7	CO ₂ e		on controlled entilectors	231.7	8,760	1,014.9						
			PM	0	Based on controlled &	10.37	8,760	45.4						
Intermediate Silo Scrubber	DT-500	10.4	PM ₁₀	0	efficiency	10.37	8,760	45.4		Assume 0 Ren	noval for control	devic		
			PM _{2.5}	0	cilicioney	10.37	8,760	45.4						
CRU Extraction Drum	DD-412		VOC			0.01	8,760	0.02						
CRU Waste Slurry Drum	DD-413	CRU removed	VOC			0.04	8,760	0.2	CRIL is being removed					
CRU Mother Liquor Drum	DD-414	CIVO TETHOVEO	VOC			0.04	8,760	0.2	CRU is being removed					
CRU Evaporation Drum	DE-416		VOC			1.04	8,760	4.5						
Process Fugitives			VOC		USEPA LDAR EF	44.58	8,760	195.2		Assumes	No LDAR progra	m		

	TOTAL POST-	PROJECT EMISSI	ONS - #2 OX PTE	(tpy)
POLLUTANT	PROCESS SOURCES (tpy)	S SOURCES SOURCES (tpy) (tpy)		TOTALS
NOx	0	119.2	N/A	119.2
VOC	805.3	3.4	211.9	1,020.5
CO	6,586.7	31.3	N/A	6,617.9
SO ₂	0	1.9	N/A	1.9
PM	45.4	3.8	N/A	49.2
PM ₁₀	45.4	3.8	N/A	49.2
PM _{2.5}	45.4	3.8	N/A	49.2
CO ₂ e	11,088.9	9,617.5	N/A	20,706.5

	TOTAL PRE	E-PROJECT EMIS	SIONS - #2 OX PTE (tp	y)
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION SOURCES (tpy)	FUGITIVE SOURCES (tpy)	TOTALS
NOx	0	119.2	N/A	119.2
VOC	810.2	3.4	195.2	1,008.8
CO	6,585.6	31.3	N/A	6,616.9
SO ₂	0	1.9	N/A	1.9
PM	45.4	3.8	N/A	49.2
PM ₁₀	45.4	3.8	N/A	49.2
PM _{2.5}	45.4	3.8	N/A	49.2
CO ₂ e	11,088.9	9,617.5	N/A	20,706.5

Table B-15
CR #1 PTA Uncontrolled Pre- and Post-Project PTE Emissions

PTE - Uncontrolled Post-Project

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (cfm)	POLLUTANT EMITTED	UNCONTROL EMISSION FACTOR (gr/cfm)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS * (lb/hr)	PERMITTED OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
			PM	-	Deced on controlled	10.00	8,760	43.8	Assume 0
Feed Slurry Drum Scrubber	CH-108	-	PM ₁₀	-	Based on controlled & efficiency	10.00	8,760	43.8	removal for
			PM _{2.5}	-	a chloichey	10.00	8,760	43.8	control device
			VOC	-	Source Test	10.62	8,760	46.5	
Crystallizer Vent Scrubber	CM-301		PM	-	Daged on controlled	121.00	8,760	530.0	Assume 0
Crystallizer Verit Scrubbei	CIVI-30 I	-	PM ₁₀	-	Based on controlled & efficiency	121.00	8,760	530.0	removal for
			PM _{2.5}	-	α emclency	121.00	8,760	530.0	control device
			PM	-	D 1 (1	30.00	8,760	131.4	Assume 0
Dryer Scrubber	CM-404A	-	PM ₁₀	-	Based on controlled & efficiency	30.00	8,760	131.4	removal for
			PM _{2.5}	-	30.00	30.00	8,760	131.4	control device
			PM	-	Danadan andrallad	30.00	8,760	131.4	Assume 0
Dryer Scrubber	CM-404B	-	PM ₁₀	-	Based on controlled & efficiency	30.00	8,760	131.4	removal for
			PM _{2.5}	-	& efficiency	30.00	8,760	131.4	control device
			PM	1.00	USEPA Handbook	42.43	8,760	185.8	Assume 0
Day Silo Baghouse	CM-603A	4,950	PM ₁₀	1.00	USEPA Handbook	42.43	8,760	185.8	removal for
			PM _{2.5}	1.00	USEPA Handbook	42.43	8,760	185.8	control device
			PM	1.00	USEPA Handbook	42.43	8,760	185.8	Assume 0
Day Silo Baghouse	CM-603B	4,950	PM ₁₀	1.00	USEPA Handbook	42.43	8,760	185.8	removal for
			PM _{2.5}	1.00	USEPA Handbook	42.43	8,760	185.8	control device
			PM	1.00	USEPA Handbook	0.86	8,760	3.8	Assume 0
Rotary Lock A Dust Collector	CM-608A	100	PM ₁₀	1.00	USEPA Handbook	0.86	8,760	3.8	removal for
			PM _{2.5}	1.00	USEPA Handbook	0.86	8,760	3.8	control device
			PM	1.00	USEPA Handbook	0.86	8,760	3.8	Assume 0
Rotary Lock B Dust Collector	CM-608B	100	PM ₁₀	1.00	USEPA Handbook	0.86	8,760	3.8	removal for
			PM _{2.5}	1.00	USEPA Handbook	0.86	8,760	3.8	control device

Table B-15
CR #1 PTA Uncontrolled Pre- and Post-Project PTE Emissions

PTE - Uncontrolled Pre-Project

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (cfm)	POLLUTANT EMITTED	UNCONTROL EMISSION FACTOR (gr/cfm)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS* (lb/hr)	PERMITTED OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS	
			PM	-	Based on controlled	10.00	8,760	43.8	Assume 0	
Feed Slurry Drum Scrubber	CH-108	-	PM ₁₀	•	& efficiency	10.00	8,760	43.8	removal for	
			PM _{2.5}	-		10.00	8,760	43.8	control device	
			VOC	-	Source Test	7.00	8,760	30.7		
Crystallizer Vent Scrubber	CM-301	_	PM	•	Based on controlled	180.00	8,760	788.4	Assume 0	
Crystallizer Verit Scrubbei	CIVI-301	_	PM ₁₀	•	& efficiency	180.00	8,760	788.4	removal for	
			PM _{2.5}	-	& efficiency	180.00	8,760	788.4	control device	
			PM	-	Decedes controlled	30.00	8,760	131.4	Assume 0	
Dryer Scrubber	CM-404A	-	PM ₁₀	-	Based on controlled & efficiency	30.00	8,760	131.4	removal for	
			PM _{2.5}	-		30.00	8,760	131.4	control device	
			PM	-	Based on controlled & efficiency	30.00	8,760	131.4	Assume 0 removal for control device	
Dryer Scrubber	CM-404B	-	PM ₁₀	-		30.00	8,760	131.4		
			PM _{2.5}	-		30.00	8,760	131.4		
		4,950	PM	1.00	USEPA Handbook	42.43	8,760	185.8	Assume 0 removal for control device	
Day Silo Baghouse	CM-603A		PM ₁₀	1.00	USEPA Handbook	42.43	8,760	185.8		
			PM _{2.5}	1.00	USEPA Handbook	42.43	8,760	185.8		
			PM	1.00	USEPA Handbook	42.43	8,760	185.8	Assume 0	
Day Silo Baghouse	CM-603B	4,950	PM ₁₀	1.00	USEPA Handbook	42.43	8,760	185.8	removal for	
			PM _{2.5}	1.00	USEPA Handbook	42.43	8,760	185.8	control device	
			PM	1.00	USEPA Handbook	0.86	8,760	3.8	Assume 0	
Rotary Lock A Dust Collector	CM-608A	100	PM ₁₀	1.00	USEPA Handbook	0.86	8,760	3.8	removal for control device	
			PM _{2.5}	1.00	USEPA Handbook	0.86	8,760	3.8		
			PM	1.00	USEPA Handbook	0.86	8,760	3.8	Assume 0	
Rotary Lock B Dust Collector	CM-608B	100 F	PM ₁₀	1.00	USEPA Handbook	0.86	8,760	3.8	removal for	
			PM _{2.5}	1.00	USEPA Handbook	0.86	8,760	3.8	control device	

TOTAL POST-PROJECT EMISSIONS - #1 PTA (tpy)									
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION SOURCES (tpy)	TOTALS						
NOx	0	NA	0						
VOC	46.5	NA	46.5						
CO	0	NA	0						
SO ₂	0	NA	0						
PM	1,215.8	NA	1,215.8						
PM ₁₀	1,215.8	NA	1,215.8						
PM _{2.5}	1,215.8	NA	1,215.8						

*Using stack test data and a 99% control device efficiency for PM

TOTAL PI	RE-PROJECT EMIS	SSIONS - #1 PTA (t	py)
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION SOURCES (tpy)	TOTALS
NOx	0	NA	0
VOC	30.7	NA	30.7
CO	0	NA	0
SO ₂	0	NA	0
PM	1,474.2	NA	1,474.2
PM ₁₀	1,474.2	NA	1,474.2
PM _{2.5}	1,474.2	NA	1,474.2

Table B-16 CR #2 PTA Uncontrolled Pre- and Post-Project PTE Emissions

PTE - Uncontrolled Post-Project

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (lb/hr)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR (% Removal)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS* (lb/hr)	PERMITTED OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
			PM	0	Based on	4.00	8,760	17.5	Assume 0
Feed Slurry Drum Scrubber	DH-518	4	PM ₁₀	0	controlled & efficiency	4.00	8,760	17.5	removal for control device
			PM _{2.5}	0		4.00	8,760	17.5	
		54	PM	0	Based on	54.00	8,760	236.5	Assume 0
Crystallizer Vent Scrubber	DM-601	54	PM ₁₀	0	controlled &	54.00	8,760	236.5	removal for
Crystallizer verit octubber		54	PM _{2.5}	0	efficiency	54.00	8,760	236.5	control device
		10.6	VOC	0	Source Test	10.60	8,760	46.4	
			PM	0	Based on	5.20	8,760	22.8	Assume 0
Dryer Scrubber	DM-704	5.2	PM ₁₀	0	controlled & efficiency	5.20	8,760	22.8	removal for control device
			PM _{2.5}	0		5.20	8,760	22.8	
			PM	0	Based on	265.00	8,760	1,160.7	Assume 0 removal for
Day Silo Dust Collector	DM-797A	265	PM ₁₀	0	controlled &	265.00	8,760	1,160.7	
			PM _{2.5}	0	efficiency	265.00	8,760	1,160.7	control device
			PM	0	Based on	265.00	8,760	1,160.7	Assume 0
Day Silo Dust Collector	DM-797B	265	PM ₁₀	0	controlled &	265.00	8,760	1,160.7	removal for
			PM _{2.5}	0	efficiency	265.00	8,760	1,160.7	control device
			PM	0	Based on controlled & efficiency	0.100	8,760	0.4	Assume 0 removal for control device
Product Recovery Unit	MLSR-2		PM ₁₀	0		0.100	8,760	0.4	
			PM _{2.5}	0		0.100	8,760	0.4	

Table B-16 CR #2 PTA Uncontrolled Pre- and Post-Project PTE Emissions

PTE - Uncontrolled Pre-Project

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (lb/hr)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR (% Removal)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS* (lb/hr)	PERMITTED OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
			PM	0	Based on	4.00	8,760	17.5	Assume 0
Feed Slurry Drum Scrubber	DH-518	4	PM ₁₀	0	controlled &	4.00	8,760	17.5	removal for control device
			PM _{2.5}	0	efficiency	4.00	8,760	17.5	
		54	PM	0	Based on	54.00	8,760	236.5	Assume 0
Crystallizer Vent Scrubber	DM-601	54	PM ₁₀	0	controlled &	54.00	8,760	236.5	removal for
	DIVI-00 I	54	PM _{2.5}	0	efficiency	54.00	8,760	236.5	control device
		7	VOC	0	Source Test	7.00	8,760	30.7	
			PM	0	Based on controlled & efficiency	5.20	8,760	22.8	Assume 0 removal for control device
Dryer Scrubber	DM-704	5.2	PM ₁₀	0		5.20	8,760	22.8	
			PM _{2.5}	0		5.20	8,760	22.8	
			PM	0	Based on	265.00	8,760	1,160.7	Assume 0 removal for
Day Silo Dust Collector	DM-797A	265	PM ₁₀	0	controlled &	265.00	8,760	1,160.7	
			PM _{2.5}	0	efficiency	265.00	8,760	1,160.7	control device
			PM	0	Based on	265.00	8,760	1,160.7	Assume 0
Day Silo Dust Collector	DM-797B	265	PM ₁₀	0	controlled &	265.00	8,760	1,160.7	removal for
,			PM _{2.5}	0	efficiency	265.00	8,760	1,160.7	control device
			PM	0	Based on controlled &	0.100	8,760	0.4	Assume 0 removal for
Product Recovery Unit	MLSR-2		PM ₁₀	0		0.100	8,760	0.4	
			PM _{2.5}	0	efficiency	0.100	8,760	0.4	control device

TOTAL POST-PROJECT EMISSIONS - #2 PTA (tpy)									
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION SOURCES (tpy)	TOTALS						
NOx	0	NA	0						
VOC	46.4	NA	46.4						
CO	0	NA	0						
SO ₂	0	NA	0						
PM	2,598.7	NA	2,598.7						
PM ₁₀	2,598.7	NA	2,598.7						
PM _{2.5}	2,598.7	NA	2,598.7						

^{*}Using stack test data and a 99% control device efficiency for PM

TOTAL F	TOTAL PRE-PROJECT EMISSIONS - #2 PTA (tpy)									
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION SOURCES (tpy)	TOTALS							
NOx	0	NA	0							
VOC	30.7	NA	30.7							
CO	0	NA	0							
SO ₂	0	NA	0							
PM	2,598.7	NA	2,598.7							
PM ₁₀	2,598.7	NA	2,598.7							
PM _{2.5}	2,598.7	NA	2,598.7							

Table B-17
Cooling Towers Uncontrolled Pre- and Post-Project PTE Emissions

PTE - Uncontrolled Post-Project

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (gpm)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR (% Removal)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
		97000	PM	0	Table B-30	14.56	8,760	63.8	Reisman, Frisbie, 2002
Cooling Tower	AT-201		PM ₁₀	0	Table B-30	10.57	8,760	46.3	Reisman, Frisbie, 2002
			PM _{2.5}	0	Table B-30	0.03	8,760	0.1	Reisman, Frisbie, 2002
		97000	PM	0	Table B-30	14.56	8,760	63.8	Reisman, Frisbie, 2002
Cooling Tower	AT-202		PM ₁₀	0	Table B-30	10.57	8,760	46.3	Reisman, Frisbie, 2002
			PM _{2.5}	0	Table B-30	0.03	8,760	0.1	Reisman, Frisbie, 2002

PTE - Uncontrolled Pre-Project

			PM	0	Table B-30	10.21	8,760	44.7	Reisman, Frisbie, 2002
Cooling Tower	ower AT-201 68000	PM ₁₀	0	Table B-30	7.41	8,760	32.5	Reisman, Frisbie, 2002	
			PM _{2.5}	0	Table B-30	0.02	8,760	0.1	Reisman, Frisbie, 2002
Cooling Tower AT-			PM	0	Table B-30	10.21	8,760	44.7	Reisman, Frisbie, 2002
	AT-202	68000	PM ₁₀	0	Table B-30	7.41	8,760	32.5	Reisman, Frisbie, 2002
			PM _{2.5}	0	Table B-30	0.02	8,760	0.1	Reisman, Frisbie, 2002

TOTAL POST-P	TOTAL POST-PROJECT EMISSIONS - #2 PTA (tpy)									
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION SOURCES (tpy)	TOTALS							
NOx	0	NA	0							
VOC	0	NA	0							
CO	0	NA	0							
SO_2	0	NA	0							
PM	127.6	NA	127.6							
PM ₁₀	92.6	NA	92.6							
PM _{2.5}	0.3	NA	0.3							

TOTAL PI	RE-PROJECT EN	MISSIONS - #2 PT	A (tpy)
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION SOURCES (tpy)	TOTALS
NOx	0	NA	0
VOC	0	NA	0
CO	0	NA	0
SO ₂	0	NA	0
PM	89.4	NA	89.4
PM ₁₀	64.9	NA	64.9
PM _{2.5}	0.2	NA	0.2

Table B-18 Fugitive Uncontrolled Pre- and Post-Project PTE Emissions

Post-Project-Uncontrolled (No LDAR Program)

	VALVES, LIQUID	VALVES, GAS	FLANGES DRAINS, VENTS & OTHERS	PUMPS	RELIEF VALVES	AGITATORS	COMPRESSORS	TOTAL HAPS EMISSIONS (lb/yr)	TOTAL STREAM (lb/yr)	TOTAL STREAM (tpy)
EF, lb/hr/item	0.0089	0.0132	0.0040	0.0439	0.2293	0.0439	0.0439			
#1 OX Unit (HON)	218	0	398	4	3	1	0	11691.44	38971	19.49
#1 OX (NSPS as HON)	2023	85	4215	34	17	18	5	4641.39	372230	186.12
#2 OX (HON)	244	0	534	3	4	1	0	14234.37	47432	23.72
#2 OX (NSPS as HON)	1960	202	4325	37	13	15	4	4693.26	376390	188.19
OSBL (HON)	303	1	588	6	4	0	0	54818.52	54819	27.41
Total	4748.11	288.11	10060.10	84.04	41.23	35.04	9.04	90,079	889,842	444.92

Project LDAR Impact 10.00%

	USEPA Factor		EF
Factors	kg/hr	lb/kg	<u>lb/hr</u>
Valves, Liquid	0.00403	2.204623	0.00888
Valves, Gas	0.00597	2.204623	0.01316
Flanges , Drains, Vents, Other	0.00183	2.204623	0.00403
Pumps	0.01990	2.204623	0.04387
Relief Valves	0.10400	2.204623	0.22928
Agitators	0.01990	2.204623	0.04387
Compressors	0.01990	2.204623	0.04387
Sample Connection	0.01500	2.204623	0.03307

USEPA Factor is based on table 2-1 from USEPA Report of 1995 on LDAR Emission factors - Average Emission Factors Effectiveness factors - HON are based on Table 5-9 from 1995 USEPA Report, NSPS from EIIP Volume II, Table 4.2.2

Pre-Project-Uncontrolled (No LDAR Program)

	VALVES,	VALVES,	FLANGES		RELIEF			TOTAL HAPS	TOTAL	TOTAL
	LIQUID	GAS	DRAINS, VENTS	PUMPS	VALVES	AGITATORS	COMPRESSORS	EMISSIONS	STREAM	STREAM
			& OTHERS					(lb/yr)	(lb/yr)	(tpy)
EF, lb/hr/item	0.0089	0.0132	0.0040	0.0439	0.2293	0.0439	0.0439			
#1 OX Unit (HON)	198	0	362	4	3	1	0	10845.32	36151	18.08
#1 OX (NSPS as HON)	1839	77	3678	34	17	18	5	4215.12	338044	169.02
#2 OX (HON)	222	0	485	3	4	1	0	13201.46	43990	22.00
#2 OX (NSPS as HON)	1782	184	3932	37	13	15	4	4320.59	346503	173.25
OSBL (HON)	303	1	588	6	4	0	0	54818.52	54819	27.41
Total	4344.01	262.01	9045.00	84.04	41.23	35.04	9.04	87,401	819,507	409.75

Pre-Project Controlled Emissions

Table B-19
Facility Pre-Project Controlled PTE Data Summary

Pre-Project Controlled PTE Emissions (tpy)

POLLUTANTS	CR #1 OX	CR #2 OX	CR #1 PTA	CR #2 PTA	COOLING TOWER	TOTAL
NOx	0.5	12.9	0	0	0	13.4
VOC	441.8	164.1	30.7	30.7	0	667.2
CO	1,890.1	357.6	0	0	0	2,247.7
SO ₂	0.03	0.1	0	0	0	0.2
PM	9.5	1.1	15.1	6.0	2.7	34.4
PM ₁₀	9.5	1.1	15.1	6.0	1.9	33.7
PM _{2.5}	9.5	1.1	15.1	6.0	0.01	31.8
CO ₂ e	54,143	40,713	•	-	-	94,856

Pre-Project Facility-Wide PTE

POLLUTANTS	MODIFIED UNITS	UNMODIFIED UNITS	FACILITY TOTAL
NOx	13.4	311.2	324.6
VOC	667.2	89.8	757.0
CO	2,247.7	286.1	2,533.8
SO ₂	0.2	188.9	189.1
PM	34.4	47.4	81.8
PM ₁₀	33.7	44.3	78.0
PM _{2.5}	31.8	42.0	73.8
CO ₂ e	94,856	418,175	513,031

Table B-20 CR #1 OX Pre-Project PTE Emissions

#1 OX PTE - Pre-Project Emissions

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM FIRE RATE (HP)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR	UNITS	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
			NOx	0.031	lb/hp-hr	AP-42 3.3 (10/96)	10.385	100	0.5	
			VOC	0.00251	lb/hp-hr	AP-42 3.3 (10/96)	0.842	100	0.04	
			CO	0.00668	lb/hp-hr	AP-42 3.3 (10/96)	2.238	100	0.1	
Emergency Generator #2	BM-1201	335	SO ₂	0.00205	lb/hp-hr	AP-42 3.3 (10/96)	0.687	100	0.03	Diesel Fuel Sulfur = 0.05%,
Emergency Generator #2	DIVI-1201	333	PM	0.0022	lb/hp-hr	AP-42 3.3 (10/96)	0.737	100	0.04	Hours per RICE MACT limit
			PM ₁₀	0.0022	lb/hp-hr	AP-42 3.3 (10/96)	0.737	100	0.04	
			PM _{2.5}	0.0022	lb/hp-hr	AP-42 3.3 (10/96)	0.737	100	0.04	
			CO ₂ e	163.6	lb/MMBtu	USEPA Data	137.634	100	6.9	
		131	VOC	85.0	% Removal	Vendor Data	19.65	8,760	87.0	Llauniu vataa alamit maatab
HPVGTS	HPVGTS-1	234	CO	85.0	% Removal	Vendor Data	35.10	8,760	1,470.0	annual emissions.
		10000.0	CO ₂ e	0	% Removal	BP calc/USEPA Data	11250	8,760	49,275.0	
	1.000	80								
Low Pressure Absorber		9	CO			BP Calcs	9.13	8,760	40.0	Recovery Device
		400.0	CO ₂ e			USEPA Data	400.0	8,760	1,752.0	
CRU Extraction Drum	BD-625	CRU will be	VOC			BP Calcs	1.0	8,760	4.4	
CRU Surge Drum	BD-631	removed	VOC			BP Calcs	4.0	8,760	17.5	Project will remove CRU
CRU Waste Slurry Drum	BD-632	Tellioved	VOC			BP Calcs	0.003	8,760	0.01	
			PM	98	% Removal	Source Test	2.16	8,760	9.5	
Silo Scrubber	BT-501		PM ₁₀	98	% Removal	Source Test	2.16	8,760	9.5	
			PM _{2.5}	98	% Removal	Source Test	2.16	8,760	9.5	
CRU Evaporator Overhd Condenser	BE-645	CRU will be removed	VOC			BP Calcs	0.3	8,760	1.3	Project will remove CRU
		Vant will be	VOC			BP Calcs	60.0	8,760	165.0	Project will remove vent -
DHT Ovhd Scrubber	BT-702	Vent will be removed	СО			BP Calcs	87.0	8,760	380.0	VOC hourly rates don't
		removed	CO ₂ e			BP calc/USEPA Data	711.4	8,760	3,115.9	match annual
Process Fugitives			VOC			USEPA LDAR EF	19.8	8,760	86.8	

TOTAL P	RE-PROJECT EM	IISSIONS - #1 OX	PTE (tpy)	
POLLUTANT	PROCESS SOURCES	COMBUSTION SOURCES	FUGITIVE SOURCES	TOTALS
NOx	0	0.5	N/A	0.5
VOC	354.9	0.04	86.8	441.8
CO	1,890.0	0.1	N/A	1,890.1
SO ₂	0	0.03	N/A	0.03
PM	9.5	0.04	N/A	9.5
PM ₁₀	9.5	0.04	N/A	9.5
PM _{2.5}	9.5	0.04	N/A	9.5
CO₂e	54,142.9	6.9	N/A	54,149.8

Table B-21 #2 OX Pre-Project PTE Emissions

#2 OX PTE - Pre-Project Emissions

#2 OX FIL - FIE-FIOJECT L					NATURAL GAS					DIESEL FUE	L (SULFUR = 0.05%)	
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM FIRE RATE	POLLUTANT EMITTED	AP-42 1.4 FACTOR (lb/MM scf)	NATURAL GAS EF (lb/MMBtu)	HOURLY EMISSION (lb/hr)	PERMIT OPERATE (hpy)	ANNUAL EMISSION (tpy)	AP-42 FACTOR (lb/hp-hr)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMIT OPERATE (hpy)	Annual Emission (tpy) - Oil
			NOx						0.024	AP-42 3.4 (10/96)	25.75	500	6.44
		1072.8	VOC						0.000642	AP-42 3.4 (10/96)	0.69	500	0.17
			CO						0.0055	AP-42 3.4 (10/96)	5.90	500	1.48
Emergency Generator #3	DM-135		SO ₂						0.00040	AP-42 3.4 (10/96)	0.43	500	0.11
Efficiency Generator #3	DIVI-133		PM						0.0007	AP-42 3.4 (10/96)	0.75	500	0.19
		hp	PM ₁₀						0.0007	AP-42 3.4 (10/96)	0.75	500	0.19
			PM _{2.5}						0.0007	AP-42 3.4 (10/96)	0.75	500	0.19
			CO ₂ e						163.6	lb/MMBtu-USEPA	440.76	500	110.19
			NOx	100	0.098	1.47	8,760	6.4					
		15.0	VOC	5.5	0.005	0.08	8,760	0.4					
			CO	84	0.082	1.24	8,760	5.4					
HPVGTS Heater	DB-1813		SO ₂	0.6	0.001	0.01	8,760	0.04					
TH VOTO Ficator	Ticater BB 1010		PM	7.6	0.007	0.11	8,760	0.5					
	MMBtu/hr	PM ₁₀	7.6	0.007	0.11	8,760	0.5						
			PM _{2.5}	7.6	0.007	0.11	8,760	0.5					
			CO ₂ e		117.000	1,755.00	8,760	7,687.0					
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (lb/hr)	POLLUTANT EMITTED	POLLUTANT EF (% Removal)	EMISSION FACTOR REFERENCE	HOURLY EMISSION (lb/hr)	PERMIT OPERATE (hpy)	ANNUAL EMISSION (tpy)		Co	OMMENTS		
	DR-1814/ DT-	285	VOC	98%	Vendor Data	5.70	8,760	25.0					
HPVGTS	1821	1589	CO	95%	BP Calcs	79.5	8,760	348.4					
	1021	5000	CO ₂ e	0	BP calc/USEPA Data	7,500.00	8,760	32,850.0					
		10.5	VOC		BP Calcs	10.48	8,760	45.9					
Low Pressure Absorber	DT-302	0.5	CO		BP Calcs	0.52	8,760	2.3					
		15.0	CO ₂ e		BP calc/USEPA Data	15.0	8,760	65.8					
			PM	99	BP Calcs	0.10	8,760	0.5					
Intermediate Silo Scrubber	DT-500	10.4	PM ₁₀	99	BP Calcs	0.10	8,760	0.5					
			PM _{2.5}	99	BP Calcs	0.10	8,760	0.5					
CRU Extraction Drum	DD-412		VOC		BP Calcs	0.01	8,760	0.02					
CRU Waste Slurry Drum	DD-413	CRU will be	VOC		BP Calcs	0.04	8,760	0.2	Project will re	move CRII			
CRU Mother Liquor Drum	DD-414	removed	VOC		BP Calcs	0.04	8,760	0.2	Ojece will re				
CRU Evaporation Drum	DE-416	· 	VOC		BP Calcs	1.04	8,760	4.5					
Process Fugitives			VOC		USEPA LDAR EF	20.1	8,760	87.8					

	TOTAL PRE-F	ROJECT EMISSION	ONS - #2 OX PTE	(tpy)
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION SOURCES (tpy)	FUGITIVE SOURCES (tpy)	TOTALS
NOx	0	12.9	N/A	12.9
VOC	75.8	0.5	87.8	164.1
CO	350.7	6.9	N/A	357.6
SO ₂	0	0.1	N/A	0.1
PM	0.5	0.7	N/A	1.1
PM ₁₀	0.5	0.7	N/A	1.1
PM _{2.5}	0.5	0.7	N/A	1.1
CO ₂ e	32,915.8	7797.2	N/A	40,713.0

Table B-22 CR #1 PTA Pre-Project PTE Emissions

#1 PTA PTE - Pre-Project Emissions

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (cfm)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR (gr/cfm)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
			PM	=	Source Test	0.10	8,760	0.4	
Feed Slurry Drum Scrubber	CH-108	=	PM ₁₀	-	Source Test	0.10	8,760	0.4	
			$PM_{2.5}$	-	Source Test	0.10	8,760	0.4	
			VOC	-	Source Test	7.00	8,760	30.7	
Crystallizer Vent Scrubber	CM-301		PM	-	Source Test	1.80	8,760	7.9	
Crystallizer verit Scrubber	CIVI-30 I	-	PM ₁₀	-	Source Test	1.80	8,760	7.9	
			$PM_{2.5}$	-	Source Test	1.80	8,760	7.9	
			PM	-	Source Test	0.30	8,760	1.3	
Dryer Scrubber	CM-404A	-	PM ₁₀	-	Source Test	0.30	8,760	1.3	
			PM _{2.5}	-	Source Test	0.30	8,760	1.3	
			PM	-	Source Test	0.30	8,760	1.3	
Dryer Scrubber	CM-404B		PM ₁₀	-	Source Test	0.30	8,760	1.3	
			PM _{2.5}	-	Source Test	0.30	8,760	1.3	
			PM	0.01	USEPA Handbook	0.42	8,760	1.9	
Day Silo Baghouse	CM-603A	4,950	PM ₁₀	0.01	USEPA Handbook	0.42	8,760	1.9	
			$PM_{2.5}$	0.01	USEPA Handbook	0.42	8,760	1.9	
			PM	0.01	USEPA Handbook	0.42	8,760	1.9	
Day Silo Baghouse	CM-603B	4,950	PM ₁₀	0.01	USEPA Handbook	0.42	8,760	1.9	
			$PM_{2.5}$	0.01	USEPA Handbook	0.42	8,760	1.9	
			PM	0.01	USEPA Handbook	0.05	8,760	0.2	
Rotary Lock A Dust Collector	CM-608A	600	PM ₁₀	0.01	USEPA Handbook	0.05	8,760	0.2	
			$PM_{2.5}$	0.01	USEPA Handbook	0.05	8,760	0.2	
			PM	0.01	USEPA Handbook	0.05	8,760	0.2	
Rotary Lock B Dust Collector	CM-608B	600	PM ₁₀	0.01	USEPA Handbook	0.05	8,760	0.2	
			$PM_{2.5}$	0.01	USEPA Handbook	0.05	8,760	0.2	

TOTAL PRE-PROJE	CT EMISSIONS - #	f1 PTA PTE (tpy)	
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION SOURCES (tpy)	TOTALS
NOx	0	NA	0
VOC	30.7	NA	30.7
CO	0	NA	0
SO ₂	0	NA	0
РМ	15.1	NA	15.12
PM ₁₀	15.1	NA	15.12
PM _{2.5}	15.1	NA	15.12

Table B-23 CR #2 PTA Pre-Project PTE Emissions

#2 PTA PTE - Pre-Project Emissions

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (lb/hr)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR (% Removal)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
			PM	99	Vendor Data	0.04	8,760	0.2	Maximum rate based
Feed Slurry Drum Scrubber	DH-518	4	PM ₁₀	99	Vendor Data	0.04	8,760	0.2	on hourly emissions
			PM _{2.5}	99	Vendor Data	0.04	8,760	0.2	and % removal
		54	PM	99	Vendor Data	0.54	8,760	2.4	Maximum PM rates
Crystallizar Vant Sarubbar	Vent Scrubber DM-601 54 PM ₁₀ 99 Vendor Data 54 PM _{2.5} 99 Vendor Data 25.5 VOC 0 Source Test	0.54	8,760	2.4	based on hourly				
Crystallizer Vent Scrubber		54	PM _{2.5}	99	Vendor Data	0.54	8,760	2.4	emissions and %
		25.5	VOC	0	Source Test	7.00	8,760	30.7	removal
	DM-704		PM	95	Vendor Data	0.26	8,760	1.1	Maximum rate based
Dryer Scrubber		5.2	PM ₁₀	95	Vendor Data	0.26	8,760	1.1	on hourly emissions and % removal
			PM _{2.5}	95	Vendor Data	0.26	8,760	1.1	
			PM	99.9	Vendor Data	0.27	8,760	1.2	Maximum rate based
Day Silo Dust Collector	DM-797A	265	PM ₁₀	99.9	Vendor Data	0.27	8,760	1.2	on hourly emissions
			PM _{2.5}	99.9	Vendor Data	0.27	8,760	1.2	and % removal
			PM	99.9	Vendor Data	0.27	8,760	1.2	Maximum rate based
Day Silo Dust Collector	DM-797B	265	PM ₁₀	99.9	Vendor Data	0.27	8,760	1.2	on hourly emissions
	<u> </u>		PM _{2.5}	99.9	Vendor Data	0.27	8,760	1.2	and % removal
			PM		BP Calcs	0.001	8,760	0.004	
Product Recovery Unit	MLSR-2		PM ₁₀		BP Calcs	0.001	8,760	0.004	
			PM _{2.5}		BP Calcs	0.001	8,760	0.004	

TOTAL PRE-PROJE	CT EMISSIONS	- #1 PTA PTE (tp	y)
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION SOURCES (tpy)	TOTALS
NOx	0	NA	0
VOC	30.7	NA	30.7
CO	0	NA	0
SO ₂	0	NA	0
PM	6.0	NA	6.0
PM ₁₀	6.0	NA	6.0
PM _{2.5}	6.0	NA	6.0

Table B-24 Cooling Towers Pre-Project PTE Emissions

Cooling Tower Pre-Project Controlled PTE Emissions (tpy)

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	MAXIMUM RATE (gpm)	POLLUTANT EMITTED	POLLUTANT EMISSION FACTOR (% Removal)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hpy)	ANNUAL EMISSIONS (tpy)	COMMENTS
			PM	97	Table B-30	0.31	8,760	1.3	Reisman, Frisbie, 2002
Cooling Tower	AT-201	68000	PM ₁₀	97	Table B-30	0.22	8,760	1.0	Reisman, Frisbie, 2002
			PM _{2.5}	97	Table B-30	0.001	8,760	0.003	Reisman, Frisbie, 2002
			PM	97	Table B-30	0.31	8,760	1.3	Reisman, Frisbie, 2002
Cooling Tower	AT-202	68000	PM ₁₀	97	Table B-30	0.22	8,760	1.0	Reisman, Frisbie, 2002
			PM _{2.5}	97	Table B-30	0.001	8,760	0.003	Reisman, Frisbie, 2002

TOTAL PRE-PROJE	CT EMISSIONS -	COOLING TOWER	R (tpy)
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION SOURCES (tpy)	TOTALS
NOx	0	NA	0
VOC	0	NA	0
CO	0	NA	0
SO ₂	0	NA	0
PM	2.7	NA	2.7
PM ₁₀	1.9	NA	1.9
PM _{2.5}	0.01	NA	0.01

Table B-25 Fugitive Pre-Project PTE Emissions

Facility Fugitives PTE - Pre-Project

	VALVES,	VALVES,	FLANGES		RELIEF			%	TOTAL HAPS	TOTAL	TOTAL
	LIQUID	GAS	DRAINS, VENTS	PUMPS	VALVES	AGITATORS	COMPRESSORS	voc	EMISSIONS	STREAM	STREAM
			& OTHERS						(lb/yr)	(lb/yr)	(tpy)
EF, lb/hr/item: (NSPS)	0.00347	0.00434	0.00270	0.01360	0.08942	0.01360	0.01360				
EF, lb/hr/item: (HON)	0.00107	0.00105	0.00028	0.01097	0.02751	0.01097	0.01097				
#1 OX Unit (HON)	198	0	362	4	3	1	0	100.0	1184.47	3948	1.97
#1 OX (NSPS)	1839	77	3832	34	17	18	5	100.0	2114.70	169595	84.80
#2 OX (HON)	222	0	485	3	4	1	0	100.0	1386.95	4622	2.31
#2 OX (NSPS)	1782	184	3932	37	13	15	4	100.0	2132.86	171052	85.53
OSBL (HON)	303	1	588	6	4	0	0	100.0	5834.33	5834	2.92
Total	4344.00	262.01	9199.00	84.02	41.12	35.02	9.02		12,653	355,051	177.53

	USEPA Factor		EF	Effectiven	ess Factor
Factors	kg/hr	lb/kg	<u>lb/hr</u>	HON	NSPS
Valves, Liquid	0.00403	2.204623	0.00888	0.88	0.61
Valves, Gas	0.00597	2.204623	0.01316	0.92	0.67
Flanges , Drains, Vents, Other	0.00183	2.204623	0.00403	0.93	0.33
Pumps	0.01990	2.204623	0.04387	0.75	0.69
Relief Valves	0.10400	2.204623	0.22928	0.88	0.61
Agitators	0.01990	2.204623	0.04387	0.75	0.69
Compressors	0.01990	2.204623	0.04387	0.75	0.69
Sample Connection	0.01500	2.204623	0.03307	0.93	0.33

USEPA Factor is based on table 2-1 from USEPA Report of 1995 on LDAR Emission factors - Average Emission Factors Effectiveness factors - HON are based on Table 5-9 from 1995 USEPA Report, NSPS from EIIP Volume II, Table 4.2.2

Unmodified Units

Table B-26 Unmodified Units Controlled and Uncontrolled PTE Emissions

Controlled Emissions - tpy

POLLUTANTS	SHIP AND LOAD	UTILITY	WWT	TOTAL
NOx	0	311.2	0	311.2
VOC	0	21.2	68.6	89.8
CO	0	286.1	0	286.1
SO ₂	0	188.9	0	188.9
PM	13.6	33.8	0	47.4
PM ₁₀	13.6	30.7	0	44.3
PM _{2.5}	13.6	28.4	0	42.0
CO ₂ e	0	418,174.8	0	418,174.8

Uncontrolled Emissions - tpy

POLLUTANTS	SHIP AND LOAD	UTILITY	WWT	TOTAL
NOx	0	311.2	0	311.2
VOC	0	21.2	68.6	89.8
CO	0	286.1	0	286.1
SO ₂	0	188.9	0	188.9
PM	1,362.2	33.8	0	1,396.0
PM ₁₀	1,362.2	30.7	0	1,392.9
PM _{2.5}	1,362.3	28.4	0	1,390.7
CO ₂ e	0	418,174.8	0	418,174.8

Table B-27
Shipping -Loading Controlled and Uncontrolled PTE Emissions

Ship and Load - Controlled

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	STACK ID NUMBER	MAXIMUM RATE (cfm)	POLLUTANT EMITTED	POLLUTANT EF (gr/cfm)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hours/yr)	ANNUAL EMISSIONS (tpy)	COMMENTS
				PM	0.01	USEPA Handbook	0.42	8,760	1.9	EPA/625/6-91/014: Control Technologies for
Storage Silo A Baghouse	CM-701A	SL-1	4,950	PM ₁₀	0.01	USEPA Handbook	0.42	8,760	1.9	HAPs
				$PM_{2.5}$	0.01	USEPA Handbook	0.42	8,760	1.9	TIAF 3
				PM	0.01	USEPA Handbook	0.42	8,760	1.9	EPA/625/6-91/014: Control Technologies for
Storage Silo B Baghouse	CM-701B	SL-2	4,950	PM ₁₀	0.01	USEPA Handbook	0.42	8,760	1.9	HAPs
				PM _{2.5}	0.01	USEPA Handbook	0.42	8,760	1.9	IIAI 3
				PM	0.01	USEPA Handbook	0.42	8,760	1.9	EPA/625/6-91/014: Control Technologies for
Storage Silo C Baghouse	CM-701C	SL-3	4,950	PM ₁₀	0.01	USEPA Handbook	0.42	8,761	1.9	HAPs
				PM _{2.5}	0.01	USEPA Handbook	0.42	8,762	1.9	TIAL 3
				PM	0.01	USEPA Handbook	0.42	8,760	1.9	EPA/625/6-91/014: Control Technologies for
Storage Silo D Baghouse	CM-701D	SL-4	4,950	PM ₁₀	0.01	USEPA Handbook	0.42	8,760	1.9	HAPs
				PM _{2.5}	0.01	USEPA Handbook	0.42	8,760	1.9	11/11/3
				PM	0.01	USEPA Handbook	0.42	8,760	1.9	EPA/625/6-91/014: Control Technologies for
Storage Silo E Baghouse	CM-701E	SL-5	4,950	PM ₁₀	0.01	USEPA Handbook	0.42	8,761	1.9	HAPs
				PM _{2.5}	0.01	USEPA Handbook	0.42	8,762	1.9	11/11/3
				PM	-	Source Test	0.48	8,760	2.1	
Storage Silo F Baghouse	CM-720 A/B	SL-6A/B		PM ₁₀	-	Source Test	0.48	8,760	2.1	
				PM _{2.5}	-	Source Test	0.48	8,760	2.1	
				PM	0.01	USEPA Handbook	0.10	8,760	0.5	EPA/625/6-91/014: Control Technologies for
Load Spout A Dust Collector	CM-705A	SL-7	1,200	PM ₁₀	0.01	USEPA Handbook	0.10	8,760	0.5	HAPs
				PM _{2.5}	0.01	USEPA Handbook	0.10	8,760	0.5	
				PM	0.01	USEPA Handbook	0.10	8,760	0.5	EPA/625/6-91/014: Control Technologies for
Load Spout B Dust Collcetor	CM-705B	SL-8	1,200	PM ₁₀	0.01	USEPA Handbook	0.10	8,760	0.5 0.5	HAPs
				PM _{2.5}	0.01	USEPA Handbook	0.10	8,760		
Land On and O Durat Oallandan	014 7050	01.0	4.000	PM	0.01	USEPA Handbook	0.10	8,760	0.5	EPA/625/6-91/014: Control Technologies for
Load Spout C Dust Collector	CM-705C	SL-9	1,200	PM ₁₀	0.01 0.01	USEPA Handbook USEPA Handbook	0.10 0.10	8,760 8,760	0.5 0.5	HAPs
		<u> </u>		PM _{2.5}	0.01	BP Calcs	0.10	,		
Bulk Truck Loading Bog Filter	CM-722	SL-10		PM	-	BP Calcs BP Calcs		8,760	0.9	4
Bulk Truck Loading Bag Filter	CIVI-722	SL-10		PM ₁₀ PM _{2.5}	-	BP Calcs	0.20 0.20	8,760 8,760	0.9 0.9	4
				1111 _{2.5}	_	Dr Caics	0.20	0,700	0.9	

Table B-27
Shipping -Loading Controlled and Uncontrolled PTE Emissions

Ship and Load - Uncontrolled

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	STACK ID NUMBER	MAXIMUM RATE (cfm)	POLLUTANT EMITTED	POLLUTANT EF (gr/cfm)	EMISSION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hours/yr)	ANNUAL EMISSIONS (tpy)	COMMENTS
				PM	1	USEPA Handbook	42.43	8,760	185.8	EPA/625/6-91/014: Control Technologies for
Storage Silo A Baghouse	CM-701A	SL-1	4,950	PM ₁₀	1	USEPA Handbook	42.43	8,760	185.8	HAPs
				PM _{2.5}	1	USEPA Handbook	42.43	8,760	185.8	TIALS
				PM	1	USEPA Handbook	42.43	8,760	185.8	EPA/625/6-91/014: Control Technologies for
Storage Silo B Baghouse	CM-701B	SL-2	4,950	PM ₁₀	1	USEPA Handbook	42.43	8,760	185.8	HAPs
				PM _{2.5}	1	USEPA Handbook	42.43	8,760	185.8	174 3
				PM	1	USEPA Handbook	42.43	8,760	185.8	EPA/625/6-91/014: Control Technologies for
Storage Silo C Baghouse	CM-701C	SL-3	4,950	PM ₁₀	1	USEPA Handbook	42.43	8,761	185.9	HAPs
				PM _{2.5}	1	USEPA Handbook	42.43	8,762	185.9	17/1 3
				PM	1	USEPA Handbook	42.43	8,760	185.8	EPA/625/6-91/014: Control Technologies for
Storage Silo D Baghouse	CM-701D	SL-4	4,950	PM ₁₀	1	USEPA Handbook	42.43	8,760	185.8	HAPs
				PM _{2.5}	1	USEPA Handbook	42.43	8,760	185.8	17/1 3
				PM	1	USEPA Handbook	42.43	8,760	185.8	EPA/625/6-91/014: Control Technologies for
Storage Silo E Baghouse	CM-701E	SL-5	4,950	PM ₁₀	1	USEPA Handbook	42.43	8,761	185.9	HAPs
				PM _{2.5}	1	USEPA Handbook	42.43	8,762	185.9	17/1 3
				PM	-	Source Test	48.00	8,760	210.2	
Storage Silo F Baghouse	CM-720 A/B	SL-6A/B		PM ₁₀	-	Source Test	48.00	8,760	210.2	
				PM _{2.5}	-	Source Test	48.00	8,760	210.2	
				PM	1	USEPA Handbook	10.29	8,760	45.1	EPA/625/6-91/014: Control Technologies for
Load Spout A Dust Collector	CM-705A	SL-7	1,200	PM ₁₀	1	USEPA Handbook	10.29	8,760	45.1	HAPs
				PM _{2.5}	1	USEPA Handbook	10.29	8,760	45.1	17.11 3
				PM	1	USEPA Handbook	10.29	8,760	45.1	EPA/625/6-91/014: Control Technologies for
Load Spout B Dust Collcetor	CM-705B	SL-8	1,200	PM ₁₀	1	USEPA Handbook	10.29	8,760	45.1	HAPs
				PM _{2.5}	1	USEPA Handbook	10.29	8,760	45.1	
				PM	1	USEPA Handbook	10.29	8,760	45.1	EPA/625/6-91/014: Control Technologies for
Load Spout C Dust Collector	CM-705C	SL-9	1,200	PM ₁₀	1	USEPA Handbook	10.29	8,760	45.1	HAPs
				PM _{2.5}	1	USEPA Handbook	10.29	8,760	45.1	
				PM	-	BP Calcs	20.00	8,760	87.6	
Bulk Truck Loading Bag Filter	CM-722	SL-10		PM ₁₀	-	BP Calcs	20.00	8,760	87.6	
				$PM_{2.5}$	-	BP Calcs	20.00	8,760	87.6	

Can only have flow to 4 of 6 silos at any one time.

TOTAL ANNU	AL SHIPPING A	AND LOADING EI	MISSIONS - CO	NTROLLED
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION SOURCES (tpy)	FUGITIVE SOURCES (tpy)	TOTALS
NO _x	0	NA	N/A	0
VOC	0	NA	N/A	0
CO	0	NA	N/A	0
SO ₂	0	NA	N/A	0
PM	13.6	NA	N/A	13.6
PM ₁₀	13.6	NA	N/A	13.6
PM _{2.5}	13.6	NA	N/A	13.6
CO ₂ e	NA	NA	N/A	0

TOTAL	ANNUAL SHIPPI	NG AND LOADIN	G EMISSIONS - UNC	ONTROLLED
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION SOURCES (tpy)	FUGITIVE SOURCES (tpy)	TOTALS
NO_x	0	NA	N/A	0
VOC	0	NA	N/A	0
CO	0	NA	N/A	0
SO ₂	0	NA	N/A	0
PM	1,362.2	NA	N/A	1,362.2
PM ₁₀	1,362.2	NA	N/A	1,362.2
PM _{2.5}	1,362.3	NA	N/A	1,362.3
CO ₂ e	NA	NA	N/A	0

Table B-28 Utility Controlled and Uncontrolled PTE Emissions

Combustion Sources

Part	Combustion Sources NATURAL GAS											DIESEL				NATURAL GAS REST OF YEAR									
Marcha M							NATORALOA				(Engines 0.05% Sulfur/Boilers at 0.5% Sulfur)														
Marchan Marc	EQUIPMENT	ID	ID		POLLUTANT		FACTOR	EMISSION		EMISSION	POLLUTANT	EMISSION	UNITS	FACTOR	EMISSION	-	EMISSION		EMISSION FACTOR	EMISSIONS	-	EMISSIONS	ANNUAL EMISSIONS	ANNUAL EMISSION	COMMENTS
Mart	DESCRIPTION	HOMBER	HOMBER	KAIL			-				NO.,		lb/MMBtu		, ,										COMMENTO
*** *** *** *** *** *** *** *** *** **				390					+	-			-												0 5 1 1 1
- Many Region of the part of t							. ,				+			` '											
Marchange Marc	Poilor #2	A D 250A	11.11		SO ₂	0.0006			8,760	1.0	SO ₂	0.51	lb/MMBtu	Mass Balance	199.28	862	85.8	SO ₂	0.0006	0.23	7,898	0.9	86.8	86.8	
Part	Bollet #3	AD-350A	0-11		PM	0.0050	Vendor Data	1.95	8,760	8.5	PM	0.03	lb/MMBtu	Vendor Data	11.70	862	5.0	PM	0.0050	1.95	7,898	7.7	12.7	12.7	
Control Cont				MMBtu*	- 10	0.0050	Vendor Data	1.95	8,760	8.5	.0	0.02	lb/MMBtu	Vendor Data	8.15	862	3.5	.0	0.0050	1.95	7,898	7.7	11.2	11.2	
Part																									сарасну.
00.00					_					-	_	+		 	,				1	,			<u> </u>		
Marchan Marc				200					+	+		+				+	1						ł	ł	-
Mathematical Math				390										` '											
000 000 000 000 000 000 000 000 000 00							\ /			_				, ,											,
## 14 10 10 10 10 10 10 10	Boiler #4	AB-350B	U-12				` ′		+		-	+		1		+	1	_					ł		
Part				MMBtu*	7 777						_	+													
Part									+	+	.0	+		1		+	1		1				ł		capacity.
Marie Mar									· · ·			+	1	1		+	1		1				ł	207,688.2	
March Marc											NO _x	0.031	lb/hp-hr	AP-42 3.3 (10/96)	11.43	100	0.6						•	0.6	
Part				368.8							VOC	0.00251	lb/hp-hr	AP-42 3.3 (10/96)	0.93	100	0.05							0.05	
Add 10 10 10 10 10 10 10												0.00668	lb/hp-hr	AP-42 3.3 (10/96)	2.46	100								0.12	OZE KIM Concretor
Marchand	Emergency	AM-804	U-3									0.00205	lb/hp-hr	AP-42 3.3 (10/96)	0.76	100	0.04								
Martin	Generator #1	7 00 .												` '											
Mathematical Column				BHP							10		· ·	` '											
Compression of the compression													·	` '				4							
Part													•	· · · · · · · ·			-								
March Marc				/112									·	` '		+		4							-
Math				413								+		, ,		+	1	-							-
# N-402	Compressor												· ·					-							Hours limited by
Hamp	#1	AC-402	U-4									+	t			+									
Part				BHP									· ·	` '				1							Ĭ
Maching											PM _{2.5}	0.00220	lb/hp-hr	AP-42 3.3 (10/96)	0.91	100	0.05							0.05	
March Marc											CO ₂ e	1.1500	lb/hp-hr	AP-42 3.3 (10/96)	474.95	100	23.7							23.7	
Magnetian											NO _x	0.012	lb/hp-hr		3.37	100	0.2							0.2	
AG-228 A				285							VOC	0.001		\/d D-4-	0.15	100	0.01							0.01	
March Marc												+	·			+									
BHP	Emergency	AG-202B	U-5										·												-
PM2	FW Pump			DUD										March 2004			1	4							
Compression				BHP										-				-							·
AC-404 A												+	·	AD 42.2.2 (10/06)				-							-
AC-404 A												+		AF-42 3.3 (10/90)											
Compressor Race Rac				1200										-				1							
AC-404 AC-404 AC-404 BHP B												+	-	1		+		1							
#2	Compressor	10.404												Permit Limit											Hours limited by
PM25 0.0003 1b/hp-hr 0.05 500 0.1 0.1 0.1 0.002 0.1 0.1 0.1 0.002 0.003 0.1 0.003 0.003 0.1 0.003 0.003 0.1 0.003 0.003 0.1 0.003	#2	AC-404	U-6									0.0003		1	0.35	500	0.1							0.1	-
CC2e 1.16 lb/hp-hr AP-42.3.4 (10/96) 1,392.0 500 348.0 348.0 348.0 348.0				BHP							PM ₁₀	0.0003	lb/hp-hr		0.35	500	0.1							0.1	
NO _x 0.057 1b/h-hr VOC 0.0022 1b/h-hr VOC 0.00022 1b/h-hr VOC 0.00132 1											PM _{2.5}	0.0003	lb/hp-hr		0.35	500	0.1							0.1	
T-Head FW Pump BHP 224 VOC 0.00022 lb/hp-hr CO 0.00132 lb/h												+		AP-42 3.4 (10/96)	ŕ		-								
T-Head FW Pump]											
T-Head FW Pump				224										4			1								<u> </u>
Pump AG-229 U-7 BHP														Variety D. (-							l., "., ., .
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		AG-229	U-7											vendor Data			1	-							
PM _{2.5} 0.00018 lb/hp-hr 0.04 100 0.002 0.002	unip			RHD									-	1		+									WACT Tegulation
				DITE									-	1				1							1
													· ·	AP-42 3 3 (10/96)				1							1

Table B-28
Utility Controlled and Uncontrolled PTE Emissions

						NATURAL G	AS					(Engine	DIESEL es 0.05% Sulfur/Boilers at	0.5% Sulfur)			NATURAL GAS REST OF YEAR (Oil at 862 hr/yr [2,400,000 gal/yr each])					СОМВ		
EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	STACK ID NUMBER	MAXIMUM RATE	POLLUTANT	EF (lb/MMBtu)	EMISSION FACTOR REFERENCE	HOURLY EMISSION (lb/hr)	OPERATE (hrs/yr)	ANNUAL EMISSION (tpy)	POLLUTANT	OIL EMISSION FACTOR	UNITS	EMISSION FACTOR REFERENCE	HOURLY EMISSION (lb/hr)	OPERATION (hrs/yr)	ANNUAL EMISSION (tpy) -Oil	POLLUTAN' EMITTED	NG EMISSION	HOURLY EMISSIONS (lb/hr)	OPERATION (hrs/yr)	ANNUAL EMISSIONS (tpy) - NG	OIL AND NG ANNUAL EMISSIONS (tpy)	WORST-CASE ANNUAL EMISSION (tpy)	COMMENTS
										NO _x	0.107	lb/hp-hr		14.57	500	3.6							3.6	
			670.5							VOC	0.00044	lb/hp-hr	Vandan Data	0.06	500	0.02							0.02	
										CO	0.00402	lb/hp-hr	Vendor Data Submitted in	0.55	500	0.1							0.1	500 KW Generator
IT Emergency	/ AM-838	U-8								SO ₂	0.01171	lb/hp-hr	application	1.60	500	0.4							0.4	Hours limited by
Generator			DUD							PM	0.00498	lb/hp-hr	December 2001	0.68	500	0.2							0.2	permit
			BHP							PM ₁₀ PM _{2.5}	0.00498	lb/hp-hr	_	0.68	500	0.2							0.2	
										CO ₂ e	0.00498	lb/hp-hr	AD 42.2.4 (40/06)	0.68 158.7	500 500	0.2 39.7							0.2 39.7	
										NO _x	1.1613 0.022	lb/hp-hr	AP-42 3.4 (10/96)	158.7	250	1.8							1.8	
			669							VOC	0.022	lb/hp-hr lb/hp-hr	-	0.22	250	0.03							0.03	
			003							co	0.004	lb/hp-hr	Vendor Data	2.94	250	0.03							0.03	-
Emergency										SO ₂	0.007	lb/hp-hr	Submitted in	4.72	250	0.4							0.6	New pump installed in 2004.
FW Pump	AG-202C	U-9								PM	0.0004	lb/hp-hr	application June	0.27	250	0.03							0.03	Hours limited by
·			BHP							PM ₁₀	0.0004	lb/hp-hr	2003	0.27	250	0.03							0.03	permit.
										PM _{2.5}	0.0004	lb/hp-hr		0.27	250	0.03							0.03	
										CO ₂ e	1.16	lb/hp-hr	AP-42 3.4 (10/96)	776.0	250	97.0							97.0	
										NO _x	0.022	lb/hp-hr		14.65	250	1.8							1.8	
			669							VOC	0.000	lb/hp-hr		0.22	250	0.03							0.03	
										CO	0.004	lb/hp-hr	Vendor Data	2.94	250	0.4							0.4	New pump
Emergency	AG-202D	U-10								SO ₂	0.007	lb/hp-hr	Submitted in application June	4.72	250	0.6							0.6	installed in 2004.
FW Pump	AO-202D	0-10								PM	0.0004	lb/hp-hr	2003	0.27	250	0.03							0.03	Hours limited by
			BHP							PM ₁₀	0.0004	lb/hp-hr		0.27	250	0.03							0.03	permit.
										PM _{2.5}	0.0004	lb/hp-hr		0.27	250	0.03							0.03	
										CO ₂ e	1.16	lb/hp-hr	AP-42 3.4 (10/96)	776.0	250	97.0							97.0	
			2.99							NO _x		-		3.50	4,380	7.7							7.7	
			MMBtu/hr							VOC		-	4	0.53	4,380	1.16							1.2	Total combined
			4475							co		-	Downit Limit	0.75	4,380	1.64							1.6	capacity of
Compressor	L-1	U-13	1175 BHP							SO ₂		-	Permit Limit	3.00	4,380	6.57 3.94							6.6 3.9	compressors L-1 & 2 shall be less than
L-1			ВНР							PM ₁₀		-	4	1.80 1.80	4,380 4,380	3.94							3.9	2350 HP (5.98
										PM _{2.5}		-	-	1.80	4,380	3.94							3.9	Million Btu/hr)
										CO ₂ e	163.6	lb/MMBtu	USEPA Factor	489.16	4,380	1071.3							1071.3	
			2.99							NO _x	100.0	-	OOLI 7(1 deloi	3.50	4,380	7.7							7.7	
			MMBtu/hr							VOC		-	†	0.53	4.380	1.16							1.2	Takal as as bis
										CO		-	1	0.75	4,380	1.64							1.6	Total combined capacity of
Compressor		11.44	1175							SO ₂		-	Permit Limit	3.00	4,380	6.57							6.6	compressors L-1 &
L-2	L-2	U-14	BHP							PM		-]	1.80	4,380	3.94							3.9	2 shall be less than
										PM ₁₀		-]	1.80	4,380	3.94							3.9	2350 HP (5.98
										PM _{2.5}		-	<u>]</u>	1.80	4,380	3.94							3.9	Million Btu/hr)
										CO ₂ e	163.6	lb/MMBtu	USEPA Factor	489.16	4,380	1071.3							1071.3	

^{*} Maximum shown for the boilers is the nominal boiler fire rate.

TOTAL ANNUAL UTILITY EMISSIONS - CONTROLLED								
POLLUTANT	PROCESS SOURCES (lb/hr)	COMBUSTION SOURCES (lb/hr)	FUGITIVE SOURCES (lb/hr)	TOTALS				
NO _x	N/A	311.2	N/A	311.2				
VOC	N/A	21.2	N/A	21.2				
CO	N/A	286.1	N/A	286.1				
SO_2	N/A	188.9	N/A	188.9				
PM	N/A	33.8	N/A	33.8				
PM ₁₀	N/A	30.7	N/A	30.7				
PM _{2.5}	N/A	28.4	N/A	28.4				
CO ₂ e	N/A	418,174.8	N/A	418,174.8				

T	TOTAL ANNUAL UTILITY EMISSIONS - UNCONTROLLED									
POLLUTANT	PROCESS COM SOURCES SO (lb/hr) (FUGITIVE SOURCES (lb/hr)	TOTALS						
NO_x	N/A	311.2	N/A	311.2						
VOC	N/A	21.2	N/A	21.2						
CO	N/A	286.1	N/A	286.1						
SO ₂	N/A	188.9	N/A	188.9						
PM	N/A	33.8	N/A	33.8						
PM ₁₀	N/A	30.7	N/A	30.7						
PM _{2.5}	N/A	28.4	N/A	28.4						
CO ₂ e	N/A	418,174.8	N/A	418,174.8						

Table B-29 WWT Controlled and Uncontrolled PTE Emissions

WWT-Controlled

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	STACK ID NUMBER	MAXIMUM RATE	POLLUTANT(S) EMITTED	POLLUTANT EMISSION FACTOR	EMISION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hours/yr)	ANNUAL EMISSIONS (tpy)	COMMENTS
CO ₂ Stripper	AT-750	WT-10		VOC	-	BP Calcs	0.35	8,760	1.5	
Anaerobic Reactor / UASB	AM-775 / AR-751	WT-11**		VOC	-	BP Calcs	0.31	8,760	1.4	
WWTP Fugitives				VOC		USEPA Water 9.0	15	8,760	65.7	

^{**} Flow normally zero.

WWT-Uncontrolled

EMISSION EQUIPMENT DESCRIPTION	EQUIPMENT ID NUMBER	STACK ID NUMBER	MAXIMUM RATE	POLLUTANT(S) EMITTED	POLLUTANT EMISSION FACTOR	EMISION FACTOR REFERENCE	HOURLY EMISSIONS (lb/hr)	PERMITTED OPERATING (hours/yr)	ANNUAL EMISSIONS (tpy)	COMMENTS
CO ₂ Stripper	AT-750	WT-10		VOC	-	BP Calcs	0.35	8,760	1.5	
Anaerobic Reactor / UASB	AM-775 / AR-751	WT-11**		VOC	-	BP Calcs	0.31	8,760	1.4	
WWTP Fugitives				VOC		USEPA Water 9.0	15	8,760	65.7	

^{**} Flow normally zero.

TOTAL A	TOTAL ANNUAL WASTEWATER TREATMENT EMISSIONS - CONTROLLED									
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION FUGITIVE SOURCES (tpy) (tpy)		TOTALS						
NO _x	0	0	NA	0						
VOC	2.89	0.0	65.70	68.59						
CO	0	0	NA	0						
SO ₂	0	0	NA	0						
PM	0	0	NA	0						
PM ₁₀	0	0	NA	0						
PM _{2.5}	0	0	NA	0						
CO₂e	0	0	NA	0						

TOTAL AN	TOTAL ANNUAL WASTEWATER TREATMENT EMISSIONS - UNCONTROLLED									
POLLUTANT	PROCESS SOURCES (tpy)	COMBUSTION SOURCES (tpy)	FUGITIVE SOURCES (tpy)	TOTALS						
NO _x	0	0	NA	0						
VOC	2.89	0.0	65.70	68.59						
CO	0	0	NA	0						
SO ₂	0	0	NA	0						
PM	0	0	NA	0						
PM ₁₀	0	0	NA	0						
PM _{2.5}	0	0	NA	0						
CO ₂ e	0	0	NA	0						

Hazardous Air Pollutants Emissions

Table B-30 Hazardous Air Pollutants Emissions

#1 OX

EMISSION	EQUIP	STACK		HOURLY	ANNUAL
EQUIPMENT	ID	ID	POLLUTANT(S)	EMISSIONS	EMISSIONS
DESCRIPTION	NUMBER	NUMBER	EMITTED	(lb/hr)	(tpy)
			Acetaldehyde	0.004	0.02
			Benzene	1.21	5.3
		O-2/O-10/O-	Formaldehyde	0.003	0.013
HPVGTS	HPVGTS-1	15	Methanol	0.87	3.8
		13	Methyl Bromide	2.03	8.9
			Paraxylene	0.04	0.2
			Toluene	0.04	0.2
			Benzene	1.47	6.7
			Formaldehyde	0.01	0.03
Atmospheric Absorber	BT-603	O-3	Methanol	0.58	2.7
Attriosprieric Absorbei	D1-003	0-3	Methyl Bromide	1.75	8.0
			Paraxylene	0.88	4.0
			Toluene	0.18	0.8
Equipment Fugitives			Paraxylene	5.00	21.7

#1 OX

POLLUTANT	lb/hr	tpy
Acetaldehyde	0.004	0.015
Benzene	2.68	12.0
Formaldehyde	0.01	0.04
Methanol	1.45	6.5
Methyl Bromide	3.78	16.9
Paraxylene	5.92	25.9
Toluene	0.22	1.0
Total HAPS	14.08	62.4

#1 PTA

EMISSION	EQUIP	STACK		HOURLY	ANNUAL
EQUIPMENT	ID	ID	POLLUTANT(S)	EMISSIONS	EMISSIONS
DESCRIPTION	NUMBER	NUMBER	EMITTED	(lb/hr)	(tpy)
			Acetaldehyde	0.12	0.5
			Benzene	0.01	0.03
			Formaldehyde	0.10	0.5
Crystallizer Vent Scrubber	CM-301	P-2	Methanol	0.23	1.0
Crystallizer Verit Octubber	CIVI-30 I	F-Z	Methyl Bronide	0	0
			Paraxylene	0.28	1.2
			Toluene	0.08	0.4
			Total	0.82	3.6

Table B-30 Hazardous Air Pollutants Emissions

#2 OX

EMISSION	EQUIP	STACK		HOURLY	ANNUAL
EQUIPMENT	ID	ID	POLLUTANT(S)	EMISSIONS	EMISSIONS
DESCRIPTION	NUMBER	NUMBER	EMITTED	(lb/hr)	(tpy)
			Acetaldehyde	0.24	1.1
			Benzene	0.25	1.1
			Formaldehyde	0.46	2.0
HPVGTS	HPVGTS-2	O2-3/4	Methanol	0.97	4.2
			Methyl Bromide	0.22	0.9
			Paraxylene	0.75	3.3
			Toluene	0.18	0.8
			Benzene	1.42	6.2
			Formaldehyde	0.01	0.02
Atmospheric Absorber	DT-302	02-1	Methanol	0.56	2.5
Attriosprieric Absorbei	D1-302	02-1	Methyl Bromide	1.68	7.4
			Paraxylene	0.85	3.7
			Toluene	0.17	0.8
Equipment Fugitives			Paraxylene	5.06	22.2

#1 OX

POLLUTANT	lb/hr	tpy
Acetaldehyde	0.24	1.1
Benzene	1.67	7.3
Formaldehyde	0.47	2.1
Methanol	1.53	6.7
Methyl Bromide	1.90	8.3
Paraxylene	6.65	29.2
Toluene	0.35	1.5
Total HAPS	12.81	56.2

#2 PTA

EMISSION	EQUIP	STACK		HOURLY	ANNUAL
EQUIPMENT	ID	ID	POLLUTANT(S)	EMISSIONS	EMISSIONS
DESCRIPTION	NUMBER	NUMBER	EMITTED	(lb/hr)	(tpy)
			Acetaldehyde	0.21	0.9
			Benzene	0.01	0.05
			Formaldehyde	0.19	0.8
Crystallizer Vent Scrubber	DM-601	P2-2	Methanol	0.41	1.8
Crystallizer Verit Scrubber	DIVI-00 I	FZ-Z	Methyl Bronide	0	0
			Paraxylene	0.51	2.2
			Toluene	0.14	0.6
			Total	1.47	6.5

Facility-Wide

POLLUTANT	lb/hr	tpy
Acetaldehyde	0.6	2.5
Benzene	4.4	19.4
Formaldehyde	0.8	3.4
Methanol	3.6	16.0
Methyl Bromide	5.7	25.2
Paraxylene	13.4	58.5
Toluene	0.8	3.5
Total HAPS	29.2	128.6

Table B-31 Cooling Tower PM Fractions and Emissions

Input Data

TDS 1500 ppmw Annual Hours 8,760 hr/yr Density of Water 0.000001 μ g/ μ m³ Conversion 60 min/hr Density of particles 2.20E-06 μ g/ μ m³ Conversion 2,000 lb/ton

Recirculation Rate 97000 gpm
Drift % 0.0006 %
Density of Water 8.34 lb/gal

Table 1 Results⁽¹⁾

EPRI DROPLET DIAMETER (µm)	DROPLET VOLUME (µm³)	DROPLET MASS (µg)	PARTICLE MASS (Solids) (µg)	SOLID PARTICLE VOLUME (µm³)	SOLID PARTICLE DIAMETER (µm)	EPRI % MASS SMALLER
10	523.60	5.24E-04	7.85E-07	0.36	0.88	0.0000
20	4,188.79	4.19E-03	6.28E-06	2.86	1.76	0.196
30	14,137.17	1.41E-02	2.12E-05	9.64	2.64	0.226
40	33,510.32	3.35E-02	5.03E-05	22.85	3.52	0.514
50	65,449.85	6.54E-02	9.82E-05	44.62	4.40	1.816
60	113,097.34	1.13E-01	1.70E-04	77.11	5.28	5.702
70	179,594.38	1.80E-01	2.69E-04	122.45	6.16	21.348
90	381,703.51	3.82E-01	5.73E-04	260.25	7.92	49.812
110	696,909.97	6.97E-01	1.05E-03	475.17	9.68	70.509
130	1,150,346.51	1.15E+00	1.73E-03	784.33	11.44	82.023
150	1,767,145.87	1.77E+00	2.65E-03	1,204.87	13.20	88.012
180	3,053,628.06	3.05E+00	4.58E-03	2,082.02	15.84	91.032
210	4,849,048.26	4.85E+00	7.27E-03	3,306.17	18.48	92.468
240	7,238,229.47	7.24E+00	1.09E-02	4,935.16	21.12	94.091
270	10,305,994.70	1.03E+01	1.55E-02	7,026.81	23.76	94.689
300	14,137,166.94	1.41E+01	2.12E-02	9,638.98	26.40	96.288
350	22,449,297.50	2.24E+01	3.37E-02	15,306.34	30.81	97.011
400	33,510,321.64	3.35E+01	5.03E-02	22,847.95	35.21	98.340
450	47,712,938.43	4.77E+01	7.16E-02	32,531.55	39.61	99.071
500	65,449,846.95	6.54E+01	9.82E-02	44,624.90	44.01	99.071
600	113,097,335.53	1.13E+02	1.70E-01	77,111.82	52.81	100.000

Based on "Calculating Realistic PM10 Emissions from Cooling Towers" by Reisman & Frisbie at Greystone Environmental Consultants

		LINEAR INTERPOLATION VALUES				
PM MASS FI	RACTIONS	SOLID PARTIC	CLE DIAMETER	MASS FRA	CTION	
PM SIZE	MASS FRACTION	T1	T2	R1	R2	
10	72.591	9.682	11.442	70.509	82.023	
2.5	0.221	1.760	2.640	0.196	0.226	

Cooling Tower Emission Rates

EMISSIONS	lb/hr	tpy
Total PM	0.44	1.91
PM ₁₀	0.32	1.39
PM _{2.5}	0.001	0.004

Appendix C RBLC Search Results

RBLC Search Results
VOC Emissions (Process Types 64.000, 64.003 and 64.999)

VOC	RBLC ID	PROCESS	VOC EMISSIONS LIMIT	CONTROL METHOD
64.000	TX-0624	Olefins Cracking Unit	801 tpy	IFR tanks and LDAR program
	Main Fermenters	40 ppmvd	None	
64.003	.003 IA-0084	Seed Fermenters	40 ppmvd	None
04.003	IA-000 4	Broth Tanks	0.02 lb/hr	None
		Solvent Recovery System	3.784 lb/hr	Scrubber
		Stillage Evaporator	0.03 lb/hr	Wet Scrubber
64.003	NE-0037	Steephouse	1.18 lb/hr	95% Eff. Thermal Oxidizer
04.003	NL-0037	Fermentation	19.2 lb/hr	Wet scrubber
		Distillation Column	3.62 lb/hr	Wet scrubber
64.003	TX-0481	Process Steam Vent	0.01 lb/hr	None
04.003	17-0401	MSS Process Steam vent	0.01 lb/hr	None
		Phenol II Process	208.43 lb/d	Condenser/TO/RTO
		Primary Cumene Stripper	3.59 lb/d	Condenser
64.003	OH-0284	RTO for Cumene Oxid and Phenol II	6.17 lb/h	RTO
04.003	011-0204	Distillation of Alphamethylstyrene	75.16 lb/d	Condensers
		Cumene Oxidation Process	47.6 lb/d	Condenser/TO/RTO
		TO for Cumene Oxid and Phenol II	6.11 lb/hr	ТО
		Rotocel Operation Process Vents	10.8 lb/hr	Chilled Water Condenser/Scrubber
		Recovery Operation ARCON tank	8.76 lb/hr	Chilled Water Condenser
64.003	NC-0111	Recovery Operation Stripper/Receiver	4.89 lb/hr	None
04.003	NC-0111	Recovery Operation Stripper/Receiver	0.85 lb/hr	Chilled Water Condenser/Scrubber
		Botanical Extraction Process Vents	14.1 lb/hr	Chilled Water and liquid N2 Condensers
		Recovery Operation ARCON tank	0.80 lb/hr	Chilled Water Condenser/Scrubber
64.003	TX-0449	Analyzer Vents	0.22 lb/hr	None
64.003	WI-0207	Distillation P24-P29	127 lb/MM gal	Packed Scrubber Tower
04.003	VVI-0201	Distillation P46-P51	218 lb/MM gal	Packed Scrubber Tower
64.003	TX-0465	Glycol Vent	9.42 lb/hr	None
64.999	IN-0129	Rail TC Cleaning	98% Efficiency	Flare
64.999	NE-0042	Lactic Acid Production	5.53 lb/hr	98% Eff. RTO
04.999	INL-0042	Fermentation	15.4 TPY	RTO
		Incinerator Process Fugitives	0.01 lb/hr	LDAR Program
		Rundown Tank Fugitives	0.11 lb/hr	LDAR Program
64.999	TX-0354	Incinerator	1.69 lb/hr	None
		Product Recovery Twr Fugitives	0.02 lb/hr	LDAR Program
		Acrolein Unit Column/Filter Cleaning	0.01 lb/hr	None

RBLC Search Results VOC Emissions (Process Type: Equipment Leaks)

	VOO Emissions (1700035 1390. Equipment Leaks)				
PROCESS CODE	RBLC ID	PROCESS	VOC EMISSIONS LIMIT	CONTROL METHOD	
	FL-0322	Equipment Leaks	6.52 tpy	LDAR Vva program	
	TX-0575	Equipment Leaks	9.01 tpy	TX LAER LDAR program	
	IA-0084	Equipment Leaks	60.9 tpy	LDAR program	
		Recovery Equipment Leaks		LDAR program	
	NC-0111	Botanical Equipment Leaks		LDAR program	
		Rotocel Equipment Leaks		LDAR program	
	TX-0449	Cycle Compressor Oil Vent	0.11 lb/hr	None	
	17-0449	Area Fugitives	4.99 lb/hr		
	TX-0454	Fugitives	0.13 lb/hr	None	
	TX-0453	Fugitives	0.20 lb/hr	None	
	WI-0204	Fugitives	SOCMI	SOCMI LDAR	
64.002	TX-0457	Fugitives	0.07 lb/hr	None	
	TX-0465	Fugitives	9.33 lb/hr	None	
	17-0405	Fugitives 4	9.08 lb/hr	None	
		DD Area Fugitives	0.06 lb/hr	LDAR program	
		Train 2 Fugitives	0.08 lb/hr	LDAR program	
		MMP Area Fugitives	0.13 lb/hr	LDAR program	
	TX-0354	Acrolein Area Fugitives	0.07 lb/hr	LDAR program	
	17-0354	H2S Plant Fugitives	0.01 lb/hr	LDAR program	
		Train 1 Fugitives	0.05 lb/hr	LDAR program	
		Dimethyl Sulfide Fugitives	0.02 lb/hr	LDAR program	
		Train 1 ETSH Fugitives	0.30 lb/hr	LDAR program	
	TX-0422	Equipment Leaks		LDAR program	

RBLC Search Results
CO Emissions (Process Types 64.000, 64.003, and 64.999)

СО	RBLC ID	PROCESS	VOC EMISSIONS LIMIT	CONTROL METHOD
64.000	TX-0624	Olefins Cracking	2256 tpy	Good Engr and Combustion
	ID-0017	Selexol Vent	8.7 lb/hr	Catox
	TX-0481	Rectisol Vent	11.4 lb/hr	None
64.003		MSS Vent	21.6 lb/hr	None
04.003	OH-0284	RTO Emissions	7.56 lb/hr	None
		TO Emissions	8.24 lb/hr	None
	TX-0354	TO Emissions-Steady state	9.56 lb/hr	None
64.999	TX-0609	Olefins Unit	146.43 tpy	Proper excess air and steam flow
04.999	TX-0354	Incinerator	1.39 lb/hr	None

Appendix D BACT Analysis Cost Information

BP Cooper River COMMON COST VALUES FOR BACT ANALYSIS

COST DESCRIPTION	COST	BASIS FOR COST			
Operations and Maintenance Labor	45 \$/hr	BP CR With Benefits			
Natural Gas Cost	3.44 \$/1,000 cf	BP CR			
Electricity Cost	0.058 \$/kW-hr	BP CR			
Potable Water	2.67 \$/1,000 gal	BP CR			
Steam	5.80 \$/1000 lb	BP CR			
Nitrogen	1.625 \$/1000 SCF	BP CR			
Wastewater Treatment	3.30 \$/1,000 gal	BP CR			
Solid Waste Disposal	104.0 \$/ton	BP CR			
Liquid Waste Disposal	0.15 \$/lb	BP CR			
Caustic	0.31 \$/lb	BP CR			
Carbon	1.00 \$/lb	Vendor Quotes for BP facility			
Capital Recovery Factor (8% and 20 year life)	0.10185	USEPA Financial References			
Site Preparation	150,000				
Facilities and Buildings	25,000				

LPA VOC COST TABLES LPA THERMAL OXIDIZER

COST ITEM		COST	TOTALS
Direct Costs			
Purchased Equipment Costs: One 2,	500 acfm TO Unit		
	ndor Info and QAQPS USEPA Factor)	\$380,000	
Ancillary Equipment	,	\$57,000	N/A
Blower		\$30,000	
Ancillary Equipment		\$4,500	
1 1 1 1 1		Sum = "A" =	\$471,500
Instrumentation (0.10 * A)		\$47,150	, , , , , ,
Sales Taxes (0.03 * A)		\$14,145	
Freight (0.05 * A)		\$23,575	
1.0.g.n (0.00 7.)	Purchased Equipment Cost = "B" =		\$556,370
Direst Installation Costs			
Foundation and Supports (0.08 * B)		\$44,510	
Handling and Errection (0.14 * B)		\$77,892	
Electrical (0.04 * B)		\$22,255	
Piping, Ductwork, and Installation (0.	02 *B)	\$11,127	
Insulation for Ductwork (0.01 * B)	<i>32 2)</i>	\$5,564	
Painting (0.01 * B)		\$5,564	
Talliang (0.01 B)	Direct Installation Cost =	ψο,σσ ι	\$166,911
Site Preparation (User Inputs Actual		\$150,000	7
Facilities and Buildings (User Inputs		\$25,000	
j \ '	Total Direct Cost =		\$898,281
Indirect Cost (Installation)			
Engineering (0.10 * B)		\$55,637	
Construction and Field Expenses (0.	05 *B)	\$27,819	
Contractor Fees (0.10 *B)	,	\$55,637	
Start-Up (0.02 *B)		\$11,127	
Performance Test (0.01 *B)		\$5,564	
Contingencies (0.03 * B)		\$16,691	
	Total Indirect Cost =	, , , , , , ,	\$172,475
	TOTAL CAPITAL INVESTMENT =		\$1,070,756
Direct Annual Costs (DC)			
Operating Labor	(Basis of Calculations)		
Operator	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$32,850
Supervisor	= (15% of Operator Cost)		\$4,928
Operating Materials	(If Any)		\$0
Maintenance Labor	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$5,475
Maintenance Materials	= 100% of Maintenance Labor		\$5,475
Replacement Labor	N/A		\$0
Parts Cost	N/A		\$0
Utilities:			11
Fuel (natural gas)	(cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	129.3	\$233,783
Electricity	$= \frac{kWhr^*hp^*1}{kWhr/1.341} + \frac{kWhr}{1.341} + \frac{kWhr}$	40.5	\$15,345
, , ,		Total DC =	\$297,855
Indirect Annual Costs (IC)			
Overhead	= 60% of the Sum of Total Labor + Materials	\$48,728	\$29,237
Administrative	= 2% of Total Capital Investment		\$21,415
Property Tax	= 1% of Total Capital Investment		\$10,708
Insurance	= 1% of Total Capital Investment		\$10,708
Capital Recovery	(Based on 8% & 20 year life: Factor = 0.1	10185)	\$109,056
j .		Total IC =	\$181,123
	TOTAL ANNUAL OPERATING COSTS =		\$478,978

LPA CATALYTIC THERMAL OXIDIZER

COST ITEM		COST	TOTALS
Direct Costs			
Purchased Equipment Costs: One 2,			
Thermal Oxidizer (User Input Cos	t: Vendor Info and QAQPS USEPA Factor)	\$ 560,000	
Ancillary Equipment		\$84,000	N/A
Blower		\$30,000	
Ancillary Equipment		\$4,500	
		Sum = "A" =	\$ 678,500.00
Instrumentation (0.10 * A)		\$67,850	
Sales Taxes (0.03 * A)		\$20,355	
Freight (0.05 * A)		\$33,925	
,	Purchased Equipment Cost = "B" =		\$800,630
Direst Installation Costs	• •		
Foundation and Supports (0.08 * B)		\$64,050	
Handling and Errection (0.14 * B)		\$112,088	
Electrical (0.04 * B)		\$32,025	
Piping, Ductwork, and Installation (0.	02 *B)	\$16,013	
Insulation for Ductwork (0.01 * B)	02 B)	\$8,006	
Painting (0.01 * B)		II ·	
Painting (0.01 B)	Direct Installation Cost =	\$8,006	\$240,189
Site Preparation (User Inputs Actual		\$150,000	φ240, 109
Facilities and Buildings (User Inputs		\$25,000	
Facilities and Buildings (Oser Inputs	Total Direct Cost =	\$25,000	¢1 215 910
I will a second a second a second a second	Total Direct Cost =		\$1,215,819
Indirect Cost (Installation)		***	
Engineering (0.10 * B)		\$80,063	
Construction and Field Expenses (0.	05 *B)	\$40,032	
Contractor Fees (0.10 *B)		\$80,063	
Start-Up (0.02 *B)		\$16,013	
Performance Test (0.01 *B)		\$8,006	
Contingencies (0.03 * B)		\$24,019	
	Total Indirect Cost =		\$2 <i>4</i> 8,195
	TOTAL CAPITAL INVESTMENT =		\$1,464,014
Direct Annual Costs (DC)			
Operating Labor	(Basis of Calculations)		
Operator	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$14,600
Supervisor	= (15% of Operator Cost)		\$2,190
Operating Materials	(If Any)		\$0
Maintenance Labor	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$14,600
Maintenance Materials	= 100% of Maintenance Labor	-	\$14,600
Replacement Labor	N/A		\$0
Catalyst Cost	= CF cat* \$850/CF* 1@2 years	30	\$12,750
Utilities:		30	ψ·=,700
Fuel (natural gas)	(cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	47.0	\$84,979
Electricity	= \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr	40.5	\$15,345
Licotrioity	- ψ/Κττιι τι ρ τ Κττιι/ 1.0 τ ι τιρ 0/ 00 τιι//	Total DC =	\$159,064
Indirect Annual Costs (IC)		rolar DO =	Ψ109,004
Overhead	= 60% of the Sum of Total Labor + Materials	\$45,990	\$27,594
Administrative		ა4 ა,ყყს	
	= 2% of Total Capital Investment		\$29,280 \$14,640
Property Tax	= 1% of Total Capital Investment		\$14,640
Insurance	= 1% of Total Capital Investment	10405)	\$14,640
Capital Recovery	(Based on 8% & 20 year life: Factor = 0.1		\$149,110
	TOTAL ANNUAL OPERATING COORS	Total IC =	\$235,264
	TOTAL ANNUAL OPERATING COSTS =		\$394,328

LPA REGENERATIVE THERMAL OXIDIZER

COST ITEM		COST	TOTALS
<u>Direct Costs</u>			
Purchased Equipment Costs			
	t: Vendor Info and QAQPS USEPA Factor)	430,000	
Ancillary Equipment		\$64,500	N/A
Blower		\$30,000	
Ancillary Equipment		\$4,500	
		Sum = "A" =	529,000
Instrumentation (0.10 * A)		\$52,900	
Sales Taxes (0.03 * A)		\$15,870	
Freight (0.05 * A)		\$26,450	
	Purchased Equipment Cost = "B" =	=	\$624,220
Direst Installation Costs			
Foundation and Supports (0.08 * B)		\$49,938	
Handling and Errection (0.14 * B)		\$87,391	
Electrical (0.04 * B)		\$24,969	
Piping, Ductwork, and Installation (0.	02 *B)	\$12,484	
Insulation for Ductwork (0.01 * B)		\$6,242	
Painting (0.01 * B)		\$6,242	
	Direct Installation Cost =		\$187,266
Site Preparation (User Inputs Actual		\$150,000	
Facilities and Buildings (User Inputs	•	\$25,000	
	Total Direct Cost =		\$986,486
Indirect Cost (Installation)			
Engineering (0.10 * B)		\$62,422	
Construction and Field Expenses (0.	05 *B)	\$31,211	
Contractor Fees (0.10 *B)		\$62,422	
Start-Up (0.02 *B)		\$12,484	
Performance Test (0.01 *B)		\$6,242	
Contingencies (0.03 * B)		\$18,727	
	Total Indirect Cost =		\$193,508
	TOTAL CAPITAL INVESTMENT =		\$1,179,994
Direct Annual Costs (DC)			
Operating Labor	(Basis of Calculations)		
Operator	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$16,425
Supervisor	= (15% of Operator Cost)		\$2,464
Operating Materials	(If Any)		\$0
Maintenance Labor	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$16,425
Maintenance Materials	= 100% of Maintenance Labor		\$16,425
Replacement Labor	N/A		\$0
Parts Cost	N/A		\$0
Utilities:			
Fuel (natural gas)	(cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	45.0	\$81,363
Electricity	= \$/kWhr* <mark>kWhr</mark> *8760 hr/yr	48.0	\$24,388
Media Replacement	= CF media * \$50/CF / 2 years	400.0	\$10,000
		Total DC =	<i>\$167,4</i> 89
Indirect Annual Costs (IC)		.	*
Overhead	= 60% of the Sum of Total Labor + Materials	\$51,739	
Administrative	= 2% of Total Capital Investment		\$23,600
Property Tax	= 1% of Total Capital Investment		\$11,800
Insurance	= 1% of Total Capital Investment		\$11,800
Capital Recovery	(Based on 8% & 20 year life: Factor = 0.		\$120,182
	TOTAL ANNUAL OPERATING COSTS	Total IC =	\$198,425
	TOTAL ANNUAL OPERATING COSTS =		\$365,915

LPA RECUPERATIVE THERMAL OXIDIZER

COST ITEM		COST	TOTALS
Direct Costs			
Purchased Equipment Costs:			
Thermal Oxidizer (User Input Cos	t: Vendor Info and QAQPS USEPA Factor)	\$650,000	
Ancillary Equipment	·	\$97,500	N/A
Blower		\$30,000	
Ancillary Equipment		\$4,500	
, , ,		Sum = "A" =	\$782,000
Instrumentation (0.10 * A)		\$78,200	
Sales Taxes (0.03 * A)		\$23,460	
Freight (0.05 * A)		\$39,100	
,	Purchased Equipment Cost = "B" =		\$922,760
Direst Installation Costs	·		
Foundation and Supports (0.08 * B)		\$73,821	
Handling and Errection (0.14 * B)		\$129,186	
Electrical (0.04 * B)		\$36,910	
Piping, Ductwork, and Installation (0.	02 *B)	\$18,455	
Insulation for Ductwork (0.01 * B)	o= =,	\$9,228	
Painting (0.01 * B)		\$9,228	
	Direct Installation Cost =	II \$\psi_0,220	\$276,828
Site Preparation (User Inputs Actual		\$150,000	42.0,020
Facilities and Buildings (User Inputs		\$25,000	
Tradimined and Banarings (eder impare	Total Direct Cost =	μ Ψ20,000	\$1,374,588
Indirect Cost (Installation)			+ 1,51 1,555
Engineering (0.10 * B)		\$92,276	
Construction and Field Expenses (0.0	05 *B)	\$46,138	
Contractor Fees (0.10 *B)	00 2)	\$92,276	
Start-Up (0.02 *B)		\$18,455	
Performance Test (0.01 *B)		\$9,228	
Contingencies (0.03 * B)		\$27,683	
Contingencies (0.05 b)	Total Indirect Cost =	Ψ21,000	\$286,056
	TOTAL CAPITAL INVESTMENT =		\$1,660,644
Direct Annual Costs (DC)			\$ 1,000,011
Operating Labor	(Basis of Calculations)		
Operator	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$16,425
Supervisor	= (15% of Operator Cost)	0.5	\$2,464
Operating Materials	= (15% of Operator Cost) (If Any)		\$2,404 \$0
Maintenance Labor	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$16,425
Maintenance Labor Maintenance Materials	= (111/511111 Still(5/day days/y) \$/11/) = 100% of Maintenance Labor	0.5	\$16,425 \$16,425
Replacement Labor	N/A		\$0 \$0
Parts Cost Utilities:	N/A		\$0
	(atm/4000 * \$/4000 at * 00 min/br *0700 br/	E2.0	#05.007
Fuel (natural gas)	(cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	53.0	\$95,827
Electricity	= \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr	40.0	\$15,155 \$162,724
Indirect Annual Costs (IC)		Total DC =	\$162,721
Overhead	= 60% of the Sum of Total Labor + Materials	654 700	¢24.042
		\$51,739	
Administrative	= 2% of Total Capital Investment		\$33,213
Property Tax	= 1% of Total Capital Investment		\$16,606 \$16,606
Insurance	= 1% of Total Capital Investment	10405)	\$16,606
Capital Recovery	(Based on 8% & 20 year life: Factor = 0.	,	\$258,367
	TOTAL ANNUAL OPERATING COSTS =	Total IC =	\$355,836 \$518,557
	TOTAL ANNUAL OF ENATING COSTS =		φυ 10,001

LPA WET SCRUBBER

COST ITEM		COST	TOTALS
<u>Direct Costs</u>			
	Purchased Equipment Costs: Scrubber		
Scrubber (User Input Cost: Vend	or into)	\$120,000	NI/A
Ancillary Equipment Blower		\$18,000	N/A
Ancillary Equipment		\$30,000 \$4,500	
Andilary Equipment		Sum = "A" =	\$172,500
Instrumentation (0.10 * A)		\$15,525	φ172,300
Sales Taxes (0.03 * A)		\$8,625	
Freight (0.05 * A)		\$13,800	
1 . e.g (e.ee 7.1)	Purchased Equipment Cost = "B" =		\$210,450
Direst Installation Costs			
Foundation and Supports (0.12 * B)		\$25,254	
Handling and Errection (0.40 * B)		\$84,180	
Electrical (0.01 * B)		\$2,105	
Piping, Ductwork, and Installation (0	.30 *B)	\$63,135	
Insulation (0.01 * B)		\$2,105	
Painting (0.01 * B)		\$2,105	
	Direct Installation Cost =		\$178,883
Site Preparation (User Inputs Actua		\$150,000	
Facilities and Buildings (User Inputs	•	\$25,000	# FC4 222
	Total Direct Cost =	1	\$564,333
Indirect Cost (Installation)		CO4.045	
Engineering (0.10 * B)	4.0.*D)	\$21,045	
Construction and Field Expenses (0. Contractor Fees (0.10 *B)	10 °B)	\$21,045 \$21,045	
Start-Up (0.01 *B)		\$2,105	
Performance Test (0.01 *B)		\$2,105 \$2,105	
Contingencies (0.03 * B)		\$2,103 \$6,314	
Contingencies (0.03 B)	Total Indirect Cost =	ψ0,514	\$73,658
TOTAL CAPITAL INVESTMENT =			\$637,990
Direct Annual Costs (DC)			. ,
Operating Labor	(Basis of Calculations)		
	r/shift * shifts/day * days/yr * \$/hr)	0.50	\$16,425
Supervisor	= (15% of Operator Cost)		\$2,464
Operating Materials	(If Any)		\$0
Maintenance Labor = (h	r/shift * shifts/day * days/yr * \$/hr)	0.50	\$16,425
	= 100% of Maintenance Labor		\$16,425
Replacement Labor	(Actual Cost Per User)		\$0
Parts Cost	(5% of Purchased Cost)		\$0
Utilities:	ФЛАИ +1 + 4 IVVI /4 О.4.1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -		A
Electricity	= \$/kWhr * hp * 1 kWhr/1.341 hp * 8760 hr/yr	10	\$3,789
Water	= \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr	38	\$53,327
Wastewater	= \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr	38	\$65,910
Caustic	=lb/hr * \$/lb * 8760 hr/yr	46.3	\$125,597
••		Total DC =	\$300,362
Indirect Annual Costs (IC)			
Indirect Annual Costs (IC)	60% of the Sum of Total Labor	\$51 7 30	\$31 D//3
Overhead =	60% of the Sum of Total Labor	\$51,739	
Overhead = Administrative =	2% of Total Capital Investment	\$51,739	\$12,760
Overhead = Administrative = Property Tax =	2% of Total Capital Investment 1% of Total Capital Investment	\$51,739	\$12,760 \$6,380
Overhead = Administrative = Property Tax = Insurance =	2% of Total Capital Investment1% of Total Capital Investment1% of Total Capital Investment	\$51,739	\$12,760 \$6,380 \$6,380
Overhead = Administrative = Property Tax = Insurance =	2% of Total Capital Investment 1% of Total Capital Investment	\$51,739 Total IC =	\$31,043 \$12,760 \$6,380 \$6,380 \$64,979 \$121,542

LPA CARBON ADSORPTION/THERMAL OXIDIZER

COST ITEM	COST	TOTALS
<u>Direct Costs</u>		
Purchased Equipment Costs: Carbon Adsorber and Thermal Oxidizer	#240.000	
Adsorber (User Input Cost: QAQPS Info) Ancillary Equipment	\$219,000 \$54,750	N/A
Thermal Oxidizer (Input Cost: Vendor Info and QAQPS USEPA Factor)	\$220,000	IN/A
Ancillary Equipment	\$33,000	
Blower	\$30,000	
Ancillary Equipment	\$4,500	
	Sum = "A" =	\$561,250
Instrumentation (0.10 * A)	\$56,125	
Sales Taxes (0.03 * A)	\$16,838	
Freight (0.05 * A) Purchased Equipment Cost = "B" =	\$28,063	\$662,275
<u>Direst Installation Costs</u>		φ002,273
Foundation and Supports (0.08 * B)	\$52,982	
Handling and Errection (0.14 * B)	\$92,719	
Electrical (0.04 * B)	\$26,491	
Piping, Ductwork, and Installation (0.02 *B)	\$13,246	
Insulation for Ductwork (0.01 * B)	\$6,623	
Painting (0.02 * B)	\$13,246	
Direct Installation Cost =	II #450,000	\$205,305
Site Preparation (User Inputs Actual Cost) Facilities and Buildings (User Inputs Actual Cost)	\$150,000	
Facilities and Buildings (Oser Inputs Actual Cost) Total Direct Cost =	\$25,000	\$1,042,580
Indirect Cost (Installation)		\$1,042,360
Engineering (0.10 * B)	\$66,228	
Construction and Field Expenses (0.05 *B) \$33,11		
Contractor Fees (0.10 *B) \$66,		
Start-Up (0.02 *B)	\$13,246	
Performance Test (0.01 *B)	\$6,623	
Contingencies (0.03 * B)	\$19,868	4
Total Indirect Cost =		\$205,305 \$1,247,886
TOTAL CAPITAL INVESTMENT = Direct Annual Costs (DC)		
Operating Labor (Basis of Calculations)		
Operator = (hr/shift * shifts/day * days/yr * \$/hr)	0.50	\$16,425
Supervisor = (15% of Operator Cost)	0.00	\$2,464
Operating Materials (If Any)		\$0
Maintenance Labor = (hr/shift * shifts/day * days/yr * \$/hr)	0.50	\$16,425
Maintenance Materials = 100% of Maintenance Labor		\$16,425
Carbon Replacement Labor (Estimated hours x labor cost)	32	\$1,440
Parts Cost (5% of Purchased Cost)		\$0
Utilities: Replacement Carbon	220,752	\$220,752
Solid waste disposal = \$/ton * lbs/yr/2000	110	\$220,732 \$11,479
Steam =4.0 lbs steam/lb Organic adsorbed * \$/lb	331128	\$7,682
Fuel (natural gas) (cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	3.0	\$5,424
Electricity = \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr	4.5	\$1,705
	Total DC =	\$300,221
Indirect Annual Costs (IC)	A =0 :==	A
Overhead = 60% of the Sum of Total Labor	\$53,179	\$31,907
Administrative = 2% of Total Capital Investment		\$24,958 \$12,470
Property Tax = 1% of Total Capital Investment Insurance = 1% of Total Capital Investment		\$12,479 \$12,479
Insurance = 1% of Total Capital Investment Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185)		\$12,479 \$127,097
(20000 011 070 0 20 your me. 1 actor = 0.10100)	Total IC =	\$208,920
TOTAL ANNUAL OPERATING COSTS =		\$509,141

LPA REFRIGERATED CONDENSER

COST ITE	M	COST	TOTALS
Direct Costs			
Purchased Equipment Costs: Refrig	erated Condenser		
Condenser (User Input Cost: QA	AQPS Info)	\$219,000	
Ancillary Equipment		\$54,750	N/A
Blower		\$30,000	
Ancillary Equipment		\$4,500	
, , ,		Sum = "A" =	\$308,250
Instrumentation (0.10 * A)		\$30,825	
Sales Taxes (0.03 * A)		\$9,248	
Freight (0.05 * A)		\$15,413	
· · · · · · · · · · · · · · · · · · ·	Purchased Equipment Cost = "B" :		\$363,735
Direst Installation Costs			
Foundation & Supports (0.08 * B)		\$29,099	
Handling & Errection (0.14 * B)		\$50,923	
Electrical (0.04 * B)		\$14,549	
Piping, Ductwork & Installation (0.02	2 *R\	\$7,275	
Insulation for Ductwork (0.01 * B)		\$3,637	
Painting (0.02 * B)		\$7,275	
r aming (0.02 D)	Direct Installation Cost =	II \$1,275	\$112,758
Site Preparation (User Inputs Actua		\$150,000	Ψ112,700
Facilities & Buildings (User Inputs A		\$25,000	
Tacinites a Buildings (Oser inputs /	Total Direct Cost =	Ψ20,000	\$651,493
Indirect Cost (Installation)	Total Birott Cost =		φοσ1, 100
Engineering (0.10 * B)		\$36,374	
Construction & Field Expenses (0.09	5 *R)	\$18,187	
Contractor Fees (0.10 *B)	, ט	\$36,374	
Start-Up (0.02 *B)		\$7,275	
Performance Test (0.01 *B)		\$3,637	
Contingencies (0.03 * B)		\$3,637 \$10,912	
Contingencies (0.03 B)	Total Indirect Cost =	\$10,912	\$112,758
	TOTAL CAPITAL INVESTMENT =		\$764,251
Direct Annual Costs (DC)			4.0. , 20.
Operating Labor	(Basis of Calculations)		
	nr/shift * shifts/day * days/yr * \$/hr)	0.50	\$16,425
Supervisor	= (15% of Operator Cost)	0.00	\$2,464
Operating Materials	(If Any)		\$0
	r/shift * shifts/day * days/yr * \$/hr)	0.20	\$6,570
	= 100% of Maintenance Labor	0.20	\$6,570 \$6,570
			\$0,570 \$0
Replacement Labor	(Actual Cost Per User)		ΨΟ
Parts Cost Utilities:	(5% of Purchased Cost)		\$0
	- ¢/lb * lb/br * 9760 br//r	4.40	#400.000
Liquid Waste Disposal	= \$/lb * <mark>lb/hr</mark> * 8760 hr/yr	140	\$183,960
Electricity	= \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr	45	\$17,050
Wastewater	= \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr	1 Total DC	\$1,734
Indirect Appuel Costs (IC)		Total DC =	\$233,038
Indirect Annual Costs (IC) Overhead =	60% of the Sum of Total Labor	\$32,029	¢10.247
		Φ3∠,U2 9	\$19,217
	2% of Total Capital Investment		\$15,285
	1% of Total Capital Investment		\$7,643
	1% of Total Capital Investment		\$7,643
Capital Recovery (Based o	n 8% & 20 year life: Factor = 0.10185)	Total IC	\$77,839 \$127,636
	TOTAL ANNUAL OPERATING COSTS	Total IC =	\$127,626 \$260,665
	TOTAL ANNUAL OPERATING COSTS =		\$360,665

CAPITAL COST ESTIMATE LPA FLARE

BASIS: Vendor Quotations, OAQPS Cost Manual (Sixth Edition)

March-14

COST ITE	Marcn-14 M	COST	TOTALS
Direct Costs			
Purchased Equipment Costs:			
Flare		\$ 208,450.00	
Steam Vent		\$ 6,350.00	N/A
Knock Out Drum		\$ 1,500.00	
Fan		\$25,000	
Ancillary Equipment		\$3,750	
		Sum = "A" =	\$ 245,050.00
Instrumentation (0.10 * A)		\$24,505	
Sales Taxes (0.03 * A)		\$7,352	
Freight (0.05 * A)		\$12,253	
	Purchased Equipment Cost = "B" =	=	\$289,159
Direct Installation Costs			
Foundation & Supports (0.08 * B)		\$23,133	
Handling & Errection (0.14 * B)		\$40,482	
Electrical (0.04 * B)		\$11,566	
Piping, Ductwork & Installation (0.02	*B)	\$5,783	
Insulation for Ductwork (0.01 * B)		\$2,892	
Painting (0.02 * B)		\$5,783	
	Direct Installation Cost =		\$89,639
Site Preparation (User Inputs Actua	I Cost)	\$150,000	
Facilities & Buildings (User Inputs A	actual Cost)	\$25,000	
	Total Direct Cost =		\$553,798
Indirect Cost (Installation)			
Engineering (0.10 * B)		\$28,916	
Construction & Field Expenses (0.08	5 *B)	\$14,458	
Contractor Fees (0.10 *B)		\$28,916	
Start-Up (0.02 *B)		\$5,783	
Performance Test (0.01 *B)		\$2,892	
Contingencies (0.03 * B)		\$8,675	
	Total Indirect Cost =		\$89,639
	TOTAL CAPITAL INVESTMENT =		\$643,438
Direct Annual Costs (DC)			
Operating Labor	(Basis of Calculations)		
Operator	= 630 hr/yr	630.00	\$28,350
Supervisor	= (15% of Operator Cost)		\$4,253
Operating Materials	(If Any)		\$0
	r/shift * shifts/day * days/yr * \$/hr)	0.50	\$16,425
	= 100% of Maintenance Labor		\$16,425
Replacement Labor	(Actual Cost Per User)		\$0
Parts Cost	(5% of Purchased Cost)		\$0
Utilities:	6 /4 + 4 / + 0 7 00 : /		. .
Liquid Waste Disposal	= \$/lb * lb/hr * 8760 hr/yr	140	\$183,960
Electricity	= \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr	45	\$17,050
Wastewater	= \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr	1	\$1,734
Fuel	= \$/1000 cf * scf/min * 60 min * 8760 hr.yr	1137	\$2,055,769
		Total DC =	\$2,323,965
Indirect Annual Costs (IC)	000/ at the Own of Tatal Lat	DOE 450	#00.070
	60% of the Sum of Total Labor	\$65,453	\$39,272
	2% of Total Capital Investment		\$12,869
	1% of Total Capital Investment		\$6,434
	1% of Total Capital Investment		\$6,434
Capital Recovery (Based o	n 8% & 20 year life: Factor = 0.10185)	T	\$65,534
	TOTAL ANNUAL OPERATING COORS	Total IC =	\$130,543
	TOTAL ANNUAL OPERATING COSTS =		\$2,454,509

HPA VOC COST TABLES HPA THERMAL OXIDIZER

COST ITEM		COST	TOTALS
Direct Costs Purchased Equipment Costs: One 3	2 000 pates TO Unit		
• •	ndor Info and QAQPS USEPA Factor)	\$720,000	
Ancillary Equipment	ido inio dia qitai o occi itti dolorj	\$108,000	N/A
Bromine Scrubber		\$350,000	14/7
Ancillary Equipment		\$52,500	
, , ,		Sum = "A" =	\$1,230,500
Instrumentation (0.10 * A)		\$123,050	
Sales Taxes (0.03 * A)		\$36,915	
Freight (0.05 * A)	Durchased Equipment Cost IIDI	\$61,525	¢4 454 000
Bina ad In adalladia n Oa ada	Purchased Equipment Cost = "B" =	<u> </u>	\$1,451,990
<u>Direst Installation Costs</u> Foundation and Supports (0.08 * B)		\$116,159	
Handling and Errection (0.14 * B)		\$203,279	
Electrical (0.04 * B)		\$58,080	
Piping, Ductwork, and Installation (0	.02 *B)	\$29,040	
Insulation for Ductwork (0.01 * B)	,	\$14,520	
Painting (0.01 * B)		\$14,520	
	Direct Installation Cost =		\$435,597
	10 ()	#450.000	
Site Preparation (User Inputs Actua		\$150,000	
Facilities and Buildings (User Inputs	Total Direct Cost =	\$25,000	\$2,062,587
Indirect Cost (Installation)	Total Birdst Cost =		Ψ2,002,001
Engineering (0.10 * B)		\$145,199	
Construction and Field Expenses (0.	05 *B)	\$72,600	
Contractor Fees (0.10 *B)	,	\$145,199	
Start-Up (0.02 *B)		\$29,040	
Performance Test (0.01 *B)		\$14,520	
Contingencies (0.03 * B)	Total Indirect Cost	\$43,560	¢450 117
	Total Indirect Cost = TOTAL CAPITAL INVESTMENT =		\$450,117 \$2,512,704
Direct Annual Costs (DC)	TOTAL GALITAL INVESTIGATION -		Ψ2,512,764
Operating Labor	(Basis of Calculations)		
Operator	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$16,425
Supervisor	= (15% of Operator Cost)		\$2,464
Operating Materials	(If Any)		\$0
Maintenance Labor	= (hr/shift * shifts/day * days/yr * \$/hr)	0.2	\$6,570
Maintenance Materials	= 100% of Maintenance Labor		\$6,570
Replacement Labor Parts Cost	N/A		\$0 \$0
Utilities:	N/A		\$0
Fuel (natural gas)	(cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	6425.9	\$11,618,422
Electricity	= \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr	127.0	\$48,125
Nitrogen for carrier	\$/1000 scf * scfm carrier gas *60 min/hr*8760 hr/yr	20000.0	\$17,082,000
Water	= \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr	76	\$106,551
Wastewater	= \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr	76	\$131,692
Caustic	=lb/hr caustic * \$/lb*8760	55	\$149,358
		Total DC =	\$29,168,177
Indirect Annual Costs (IC) Overhead	600/ of the Cum of Total Labor . Materials	Ф 20,000	640.047
	= 60% of the Sum of Total Labor + Materials	\$32,029	
Administrative Property Tax	= 2% of Total Capital Investment = 1% of Total Capital Investment		\$50,254 \$25,127
Insurance	= 1% of Total Capital Investment		\$25,127 \$25,127
Capital Recovery	(Based on 8% & 20 year life: Factor = 0.	10185)	\$25,127 \$255,919
,	(1.111 1 111 11 11 1 1 1 1 1 1 1 1 1 1	Total IC =	\$375,644
	TOTAL ANNUAL OPERATING COSTS =		\$29,543,821

HPA CATALYTIC THERMAL OXIDIZER

COST ITEM		COST	TOTALS
Direct Costs			
Existing Unit No construction necessa	ary including bromine scrubber		
Thermal Oxidizer (User Input Cos	st: Vendor Info and QAQPS USEPA Factor)	\$ -	
Ancillary Equipment		\$0	N/A
·		Sum = "A" =	\$0
Instrumentation (0.10 * A)		\$0	
Sales Taxes (0.03 * A)		\$0	
Freight (0.05 * A)		\$0	
1 10.g.n. (0.00 7.1)	Purchased Equipment Cost = "B" =		\$0
Direst Installation Costs			7.0
Foundation and Supports (0.08 * B)		\$0	
Handling and Errection (0.14 * B)		\$0	
Electrical (0.04 * B)	00 +D)	\$0	
Piping, Ductwork, and Installation (0	.02 ⁻ B)	\$0	
Insulation for Ductwork (0.01 * B)		\$0	
Painting (0.01 * B)		\$0	
	Direct Installation Cost =		\$0
Site Preparation (User Inputs Actua		\$0	
Facilities and Buildings (User Inputs		\$0	
	Total Direct Cost =		\$0
Indirect Cost (Installation)			
Engineering (0.10 * B)		\$0	
Construction and Field Expenses (0	.05 *B)	\$0	
Contractor Fees (0.10 *B)	,	\$0	
Start-Up (0.02 *B)		\$0	
Performance Test (0.01 *B)		\$0	
Contingencies (0.03 * B)		\$0	
Contingencies (0.05 b)	Total Indirect Cost =	ΨΟ	\$0
	TOTAL CAPITAL INVESTMENT =		\$0
Direct Annual Costs (DC)	TOTAL CALITAL INVESTIGATION		ΨΟ
Operating Labor	(Pagis of Coloulations)		
	(Basis of Calculations)	0.5	\$16,425
Operator	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	
Supervisor	= (15% of Operator Cost)		\$2,464
Operating Materials	(If Any)		\$0
Maintenance Labor	= (hr/shift * shifts/day * days/yr * \$/hr)	0.2	\$6,570
Maintenance Materials	= 100% of Maintenance Labor		\$6,570
Replacement Labor	N/A		\$0
Catalyst Cost	= CF cat* \$850/CF* 1@2 years	20	\$8,500
Utilities:			
Fuel (natural gas)	(cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	196.1	\$354,522
Electricity	$= \frac{\text{kWhr*}^{\text{hp*}1 \text{kWhr/1.341 hp*8760 hr/yr}}}{\text{kWhr*}^{\text{hp*}1 \text{kWhr/1.341 hp*8760 hr/yr}}}$	15.0	\$5,683
Wastewater	= \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr	15	\$26,017
Sodium Formate	=lb/hr * \$/lb * 8760 hr/yr	15.0	\$40,734
	4 0. 00 1111 11	Total DC =	\$467,486
Indirect Annual Costs (IC)		. 3.0. 2 3	\$ 757, 100
Overhead	= 60% of the Sum of Total Labor + Materials	\$32,029	\$19,217
Administrative	= 2% of Total Capital Investment	Ψ02,023	\$0
Property Tax	= 1% of Total Capital Investment		\$0 \$0
1	= 1% of Total Capital Investment		ΦΟ
Insurance		10405)	\$0 \$0
Capital Recovery	(Based on 8% & 20 year life: Factor = 0.1		
	TOTAL ANNUAL OPERATING COCTO	Total IC =	\$19,217
	TOTAL ANNUAL OPERATING COSTS =		\$486,703

HPA REGENERATIVE THERMAL OXIDIZER/BROMINE SCRUBBER BASIS: Vendor Quotations, OAQPS Cost Manual (Sixth Edition)

COST ITEM		COST	TOTALS
<u>Direct Costs</u>			
Purchased Equipment Costs			
	t: Vendor Info and QAQPS USEPA Factor)	2,101,175	
Ancillary Equipment		\$315,176	N/A
Bromine Scrubber		\$350,000	
Ancillary Equipment		\$52,500	
		Sum = "A" =	2,818,852
Instrumentation (0.10 * A)		\$281,885	
Sales Taxes (0.03 * A)		\$84,566	
Freight (0.05 * A)	Purchased Equipment Cost = "B" =	\$140,943	\$2.226.24E
Direct Installation Coats	Furchased Equipment Cost = B =		\$3,326,245
<u>Direst Installation Costs</u> Foundation and Supports (0.08 * B)		\$266,100	
Handling and Errection (0.14 * B)		II .	
Electrical (0.04 * B)		\$465,674 \$133,050	
Piping, Ductwork, and Installation (0.	02 *P)	\$133,030 \$66,525	
Insulation for Ductwork (0.01 * B)	02 B)	\$33,262	
Painting (0.01 * B)		\$33,262	
Fairting (0.01 B)	Direct Installation Cost =	¶ \$33,202	\$997,874
Site Preparation (User Inputs Actua		\$150,000	φοστ,σττ
Facilities and Buildings (User Inputs		\$25,000	
	Total Direct Cost =	W +===,===	\$4,499,119
Indirect Cost (Installation)			
Engineering (0.10 * B)		\$332,625	
Construction and Field Expenses (0.	05 *B)	\$166,312	
Contractor Fees (0.10 *B)	,	\$332,625	
Start-Up (0.02 *B)		\$66,525	
Performance Test (0.01 *B)		\$33,262	
Contingencies (0.03 * B)		\$99,787	
	Total Indirect Cost =		\$1,031,136
	TOTAL CAPITAL INVESTMENT =		\$5,530,255
Direct Annual Costs (DC)			
Operating Labor	(Basis of Calculations)		•
Operator	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$16,425
Supervisor	= (15% of Operator Cost)		\$2,464
Operating Materials	(If Any)		\$0
Maintenance Labor	= (hr/shift * shifts/day * days/yr * \$/hr)	0.2	\$6,570
Maintenance Materials	= 100% of Maintenance Labor		\$6,570
Replacement Labor	N/A		\$0
Parts Cost Utilities:	N/A		\$0
	(ofm/1000 * \$/1000 of * 60 min/h- *0700 h-/>	640.0	Ø4 404 040
Fuel (natural gas) Electricity	(cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr) = \$/kWhr* kWhr *8760 hr/yr	642.6 395.0	\$1,161,842
Nitrogen for carrier	= \$/kwnr	20000.0	\$200,692 \$17,082,000
Water	= \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr	20000.0 76	\$17,082,000 \$106,551
Wastewater	= \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr	76 76	\$106,551 \$131,692
Caustic	=\(\frac{1}{3}\)/1,000 gai \(\frac{1}{3}\)/1111/11100 \(\frac{1}{3}\)/1111/111 \(\frac{1}{3}\)/100 \(\frac{1}{3}\)/111/111 \(\frac{1}{3}\)/100 \(\frac{1}{3}\)/111/111 \(\frac{1}{3}\)/100 \(\frac{1}{3}\)/11/111/111 \(\frac{1}{3}\)/100 \(\frac{1}{3}\)/11/111 \(\frac{1}{3}\)/100 \(\frac{1}{3}\)/11/11/11 \(\frac{1}{3}\)/11/11/11 \(\frac{1}{3}\)/11/11/11 \(\frac{1}{3}\)/11/11/11 \(\frac{1}{3}\)/11/11/11 \(\frac{1}{3}\)/11/11/11/11 \(\frac{1}{3}\)/11/11/11 \(\frac{1}{3}\)/11/11/11/11 \(\frac{1}{3}\)/11/11/11/11 \(\frac{1}{3}\)/11/11/11/11 \(\frac{1}{3}\)/11/11/11/11 \(\frac{1}{3}\)/11/11/11/11 \(\frac{1}{3}\)/11/11/11/11 \(\frac{1}{3}\)/11/11/11/11 \(\frac{1}{3}\)/11/11/11/11 \(\frac{1}{3}\)/11/11/11/11/11/11/11/11/11/11/11/11/11	76 55	\$131,692 \$149,358
Media Replacement	= CF media * \$50/CF / 3 years	10000.0	\$149,356 \$166,667
iviedia Nepiacement	- Of Media \$50/OF / 3 years	Total DC =	\$19,030,830
Indirect Annual Costs (IC)		. 5141 20 -	φ10,000,000
Overhead	= 60% of the Sum of Total Labor + Materials	\$32,029	\$19,217
Administrative	= 2% of Total Capital Investment	Ψ02,020	\$110,605
Property Tax	= 1% of Total Capital Investment		\$55,303
Insurance	= 1% of Total Capital Investment		\$55,303
Capital Recovery	(Based on 8% & 20 year life: Factor = 0.7	10185)	\$418,691
	(=3.55.5 5.7 5.7 5.7 5.7 5.7 5.7 5.7 5.7 5.	Total IC =	\$659,119
	TOTAL ANNUAL OPERATING COSTS =		\$19,689,949

HPA RECUPERATIVE THERMAL OXIDIZER

COST ITEM		COST	TOTALS
Direct Costs			
Purchased Equipment Costs:			
	t: Vendor Info and QAQPS UEPA Factor)	\$1,095,000	
Ancillary Equipment		\$164,250	N/A
Bromine Scrubber		\$350,000	
Ancillary Equipment		\$52,500 Sum = "A" =	¢1 661 750
Instrumentation (0.10 * A)		\$166,175	\$1,661,750
Sales Taxes (0.03 * A)		\$49,853	
Freight (0.05 * A)		\$83,088	
Troight (0.00 7t)	Purchased Equipment Cost = "B" =		\$1,960,865
Direst Installation Costs			, , ,
Foundation and Supports (0.08 * B)		\$156,869	
Handling and Errection (0.14 * B)		\$274,521	
Electrical (0.04 * B)		\$78,435	
Piping, Ductwork, and Installation (0.	02 *B)	\$39,217	
Insulation for Ductwork (0.01 * B)		\$19,609	
Painting (0.01 * B)		\$19,609	
	Direct Installation Cost =	11 * -	\$588,260
Site Preparation (User Inputs Actua		\$150,000	
Facilities and Buildings (User Inputs		\$25,000	Ø0 70 4 40 F
	Total Direct Cost =		\$2,724,125
Indirect Cost (Installation)		# 400.007	
Engineering (0.10 * B)	OC *D)	\$196,087	
Construction and Field Expenses (0.	05 °B)	\$98,043 \$196,087	
Contractor Fees (0.10 *B) Start-Up (0.02 *B)		\$196,087	
Performance Test (0.01 *B)		\$19,609	
Contingencies (0.03 * B)		\$58,826	
Contingential (c.co b)	Total Indirect Cost =	ψ00,020	\$607,868
	TOTAL CAPITAL INVESTMENT =	"	\$3,331,993
Direct Annual Costs (DC)			
Operating Labor	(Basis of Calculations)		
Operator	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$16,425
Supervisor	= (15% of Operator Cost)		\$2,464
Operating Materials	(If Any)		\$0
Maintenance Labor	= (hr/shift * shifts/day * days/yr * \$/hr)	0.2	\$6,570
Maintenance Materials	= 100% of Maintenance Labor		\$6,570
Replacement Labor	N/A		\$0
Parts Cost	N/A		\$0
Utilities:	/ 1 /4000 + 0/4000	0040.0	Ø5 000 044
Fuel (natural gas)	(cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	3212.9	\$5,809,211
Electricity	= \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr	301.7	\$114,297
Nitrogen for carrier Water	\$/1000 scf * scfm carrier gas *60 min/hr*8760 hr/yr = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr	20000.0 76	\$17,082,000 \$106,551
Wastewater	= \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr	76 76	\$106,551 \$131,692
Caustic	=\(\beta/1,000\) gai \(\text{gai/\text{fill}}\) 1000 \(\text{00}\) \(\text{fill}\) 1000 \(\text{00}\) 1100 \(\text{fill}\) 1000 \(\text{fill}\) 10000 \(\text{fill}\) 1000 \(\text{fill}\) 10000 \(\text{fill}\) 10000 \(\text{fill}\) 10000 \(\text{fill}\) 10000 \(\text{fill}\) 1	76 55	\$131,092 \$149,358
Cadolio		Total DC =	\$23,425,138
Indirect Annual Costs (IC)			φ=0, :=0, :00
Overhead	= 60% of the Sum of Total Labor + Materials	\$32,029	\$19,217
Administrative	= 2% of Total Capital Investment	, - ,	\$66,640
Property Tax	= 1% of Total Capital Investment		\$33,320
Insurance	= 1% of Total Capital Investment		\$33,320
Capital Recovery	(Based on 8% & 20 year life: Factor = 0.7		\$258,367
••		Total IC =	¢110 061
	TOTAL ANNUAL OPERATING COSTS =	10tal 10 =	\$410,864 \$23,836,001

HPA WET SCRUBBER

	1	COST	TOTALS
<u>Direct Costs</u>			
Purchased Equipment Costs: Scrub			
Scrubber (User Input Cost: Vendo	dor Info)	\$870,000	
Ancillary Equipment		\$130,500	N/A
		Sum = "A" =	\$1,000,500
Instrumentation (0.10 * A)		\$90,045	
Sales Taxes (0.03 * A)		\$50,025	
Freight (0.05 * A)		\$80,040	
	Purchased Equipment Cost = "B" =	_	\$1,220,610
Direst Installation Costs			
Foundation and Supports (0.12 * B)		\$146,473	
Handling and Errection (0.40 * B)		\$488,244	
Electrical (0.01 * B)		\$12,206	
Piping, Ductwork, and Installation (0	0.30 *B)	\$366,183	
Insulation (0.01 * B)		\$12,206	
Painting (0.01 * B)		\$12,206	4.
	Direct Installation Cost =	II #4=0.000	\$1,037,519
Site Preparation (User Inputs Actua		\$150,000	
Facilities and Buildings (User Input		\$25,000	(0. 400 400
	Total Direct Cost =	1	\$2,433,129
Indirect Cost (Installation)		* • • • • • • • • • • • • • • • • • • •	
Engineering (0.10 * B)	40.45	\$122,061	
Construction and Field Expenses (0	.10 *B)	\$122,061	
Contractor Fees (0.10 *B)		\$122,061	
Start-Up (0.01 *B)		\$12,206	
Performance Test (0.01 *B)		\$12,206	
Contingencies (0.03 * B)	T (\$36,618	0.407.04.4
	Total Indirect Cost =		\$427,214
Direct Assessed Contra (DO)	TOTAL CAPITAL INVESTMENT =		\$2,860,342
Direct Annual Costs (DC)	(Paris of Calculations)		
Operating Labor	(Basis of Calculations)	0.50	040 405
	nr/shift * shifts/day * days/yr * \$/hr)	0.50	\$16,425
Supervisor	= (15% of Operator Cost)		\$2,464
Operating Materials	(If Any)	0.50	\$0 \$16.435
	r/shift * shifts/day * days/yr * \$/hr) = 100% of Maintenance Labor	0.50	\$16,425
			\$16,425
Replacement Labor	(Actual Cost Per User)		\$0 \$0
Parts Cost Utilities:	(5% of Purchased Cost)		\$0
Electricity	- \$/k\\\\ hr * hn * 1 k\\\\ hr/1 2/1 hn * 9760 hr/m	130	\$49,114
Water	= \$/kWhr * hp * 1 kWhr/1.341 hp * 8760 hr/yr = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr		\$49,114 \$129,940
Wastewater	= \$/1,000 gal * gal/min/1000 * 60 min/m * 8760 m/yr = \$/1,000 gal * gal/min/1000 * 60 min/m * 8760 m/yr	93 93	\$129,940 \$160,600
Caustic	=\(\frac{1}{1}\),000 gai \(\frac{\text{gai/fillif}}{\text{100}}\) 1000 \(\text{80 fillif}\) 1000	433	\$1,175,695
Causiic	-ιν/τιι causiic ψ/ιν σ/ σσ	Total DC =	\$1,175,095 \$1,567,088
Indirect Annual Costs (IC)		i olai DO =	φ1,007,000
	60% of the Sum of Total Labor	\$51,739	\$31,043
	2% of Total Capital Investment	ψο 1,7 ο σ	\$57,043 \$57,207
	: 1% of Total Capital Investment		\$28,603
	: 1% of Total Capital Investment		\$28,603 \$28,603
	n 8% & 20 year life: Factor = 0.10185)		\$28,003 \$291,326
	11 0 70 & 20 your mo. 1 abiot - 0.10100)		
(Basea s		Total IC -	\$436 783
Capital Moderaty (Bassa s	TOTAL ANNUAL OPERATING COSTS =	Total IC =	\$436,783 \$2,003,871

HPA CARBON ADSORPTION/THERMAL OXIDIZER/SCRUBBER BASIS: Vendor Quotations, OAQPS Cost Manual (Sixth Edition)

Direct Coots	М	COST	TOTALS
Direct Costs Purchased Equipment Costs: Carbo Adsorber (User Input Cost: QAC Ancillary Equipment Thermal oxidizer Ancillary Equipment		\$215,000 \$53,750 \$435,000 \$108,750	N/A
Bromine Scrubber Ancillary Equipment		\$270,000 \$40,500 Sum = "A" =	\$1,123,000
Instrumentation (0.10 * A) Sales Taxes (0.03 * A) Freight (0.05 * A)		\$112,300 \$33,690 \$56,150	ψ1,123,000
,	Purchased Equipment Cost = "B" =	=	\$1,325,140
Direst Installation Costs Foundation and Supports (0.08 * B) Handling and Errection (0.14 * B) Electrical (0.04 * B) Piping, Ductwork, and Installation (0.01 * B) Painting (0.02 * B)		\$106,011 \$185,520 \$53,006 \$26,503 \$13,251 \$26,503	
	Direct Installation Cost =		\$410,793
Site Preparation (User Inputs Actual Facilities and Buildings (User Input	s Actual Cost)	\$150,000 \$25,000	# 4.040.000
Indirect Cost (Installation)	Total Direct Cost =	1	\$1,910,933
Engineering (0.10 * B) Construction and Field Expenses (0 Contractor Fees (0.10 *B) Start-Up (0.02 *B) Performance Test (0.01 *B) Contingencies (0.03 * B)	.05 *B)	\$132,514 \$66,257 \$132,514 \$26,503 \$13,251 \$39,754	
	Total Indirect Cost =		\$410,793
	TOTAL CAPITAL INVESTMENT =		\$2,321,727
Direct Annual Costs (DC)			\$2,321,727
Operating Labor Operator = (h Supervisor	(Basis of Calculations) nr/shift * shifts/day * days/yr * \$/hr) = (15% of Operator Cost)	0.50	\$16,425 \$2,464
Operating Labor Operator = (h Supervisor Operating Materials Maintenance Labor = (h Maintenance Materials Replacement Labor Parts Cost	(Basis of Calculations) nr/shift * shifts/day * days/yr * \$/hr)	0.50 0.50	\$2,321,727 \$16,425 \$2,464 \$0 \$16,425 \$16,425 \$0 \$0
Operating Labor Operator = (h Supervisor Operating Materials Maintenance Labor = (h Maintenance Materials Replacement Labor	(Basis of Calculations) nr/shift * shifts/day * days/yr * \$/hr) = (15% of Operator Cost)	0.50 3,416,400 1708 5,124,600 580.0 45 40 40 40.0	\$16,425 \$2,464 \$0 \$16,425 \$16,425 \$0 \$0 \$3,416,400 \$177,653 \$118,891 \$94,503 \$293,960 \$56,134 \$69,379 \$108,624
Operating Labor Operator = (h Supervisor Operating Materials Maintenance Labor = (h Maintenance Materials Replacement Labor Parts Cost Utilities: Replacement Carbon Solid waste disposal Steam Fuel (natural gas) Electricity Water Wastewater Sodium Formate	(Basis of Calculations) nr/shift * shifts/day * days/yr * \$/hr) = (15% of Operator Cost) (If Any) nr/shift * shifts/day * days/yr * \$/hr) = 100% of Maintenance Labor (Actual Cost Per User) (5% of Purchased Cost) = \$/ton * lbs/yr/2000 =4.0 lbs steam/lb Organic adsorbed * \$/lb (cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	0.50 3,416,400 1708 5,124,600 580.0 45 40 40	\$16,425 \$2,464 \$0 \$16,425 \$16,425 \$0 \$0 \$3,416,400 \$177,653 \$118,891 \$94,503 \$293,960 \$56,134 \$69,379
Operating Labor Operator = (h Supervisor Operating Materials Maintenance Labor = (h Maintenance Materials Replacement Labor Parts Cost Utilities: Replacement Carbon Solid waste disposal Steam Fuel (natural gas) Electricity Water Wastewater Sodium Formate Indirect Annual Costs (IC) Overhead = Administrative Property Tax Insurance = (h	(Basis of Calculations) nr/shift * shifts/day * days/yr * \$/hr) = (15% of Operator Cost) (If Any) nr/shift * shifts/day * days/yr * \$/hr) = 100% of Maintenance Labor (Actual Cost Per User) (5% of Purchased Cost) = \$/ton * lbs/yr/2000 =4.0 lbs steam/lb Organic adsorbed * \$/lb (cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	0.50 3,416,400 1708 5,124,600 580.0 45 40 40 40.0	\$16,425 \$2,464 \$0 \$16,425 \$16,425 \$0 \$3,416,400 \$177,653 \$118,891 \$94,503 \$293,960 \$56,134 \$69,379 \$108,624

${\sf HPA}\ {\sf REFRIGERATED}\ {\sf CONDENSER}\ {\sf SYSTEM/BROMINE}\ {\sf SCRUBBER}$

BASIS: Vendor Quotations, OAQPS Cost Manual (Sixth Edition)

Instrumentation (0.10 ° A) Sales Taxes (0.03 ° A) Freight (0.05 ° A) Purchased Equipment Cost = "B" = \$147,300 \$144,190 \$73,650 \$147,300 \$144,190 \$73,650 \$139,051 \$139,051 \$2243,340 \$140,001 \$140,001 \$140,001 \$140,001 \$150,000 \$140,001 \$150,000	COST	TITEM	COST	TOTALS
Condenser (User Input Cost: QAQPS Info) S850,000 Ancillary Equipment \$212,500 \$100,000 \$20,0000 \$40,500 \$270,0000 \$40,500 \$270,0000 \$40,500 \$270,0000 \$40,500 \$270,0000 \$40,500 \$270,0000 \$40,500 \$270,0000 \$40,500 \$270,0000 \$40,500 \$270,0000 \$40,500 \$270,0000 \$40,500 \$270,0000 \$40,500 \$270,0000 \$40,500 \$270,0000 \$40,500 \$270,0000 \$40,500 \$270,0000 \$40,500 \$270,0000 \$40,500 \$41,7300 \$				
Ancillary Equipment VOC Storage Bromine Scrubber Ancillary Equipment Vox Ancillary Equipment Cost = VAT				
VOC Storage Bromine Scrubber S40,000 S270,000 S270,000 S40,000 S270,000 S40,000 S44,190		: QAQPS Info)		
Bromine Scrubber Ancillary Equipment \$270,000 \$40,500 \$4				N/A
Ancillary Equipment				
Instrumentation (0.10 * A) Sales Taxes (0.03 * A) Freight (0.05 * A) S417,300				
Instrumentation (0.10 * A) Sales Taxes (0.03 * A) Freight (0.05 *	Ancillary Equipment			
Sales Taxes (0.03 * A) Freight (0.05 * A) S73,650				\$1,473,000
Purchased Equipment Cost = "B" = \$73,650 Purchased Equipment Cost = "B" = \$1,738,146 Direct Installation Costs \$139,051 Foundation and Supports (0.08 * B) Handling and Errection (0.14 * B) \$243,340 Electrical (0.04 * B) \$543,763 Insulation for Ductwork (0.01 * B) \$34,763 Insulation for Ductwork (0.01 * B) \$17,381 Painting (0.02 * B) \$173,814 Painting (0.10 * B) \$173,814 Engineering (0.10 * B) \$173,814 Construction and Field Expenses (0.05 * B) \$86,907 Contractor Fees (0.10 * B) \$173,814 Construction and Field Expenses (0.05 * B) \$86,907 Contractor Fees (0.10 * B) \$173,814 Contingencies (0.03 * B) \$173,814 Solution \$173,	Instrumentation (0.10 * A)		\$147,300	
Purchased Equipment Cost = "B" = \$1,738,146			\$44,190	
Direct Installation Costs Stock	Freight (0.05 * A)		\$73,650	
Foundation and Supports (0.08 * B)		Purchased Equipment Cost = "B" :	=	\$1,738,140
Handling and Errection (0.14 * B) \$243,340 \$89,526 \$10,004 * B) \$34,763 \$17,361 \$34,763 \$17,361 \$34,763 \$3				
Electrical (0.04 * B)				
Piping, Ductwork, and Installation (0.02 *B)	Handling and Errection (0.14 *	В)	\$243,340	
Insulation for Ductwork (0.01 * B)				
Painting (0.02 * B)				
Site Preparation (User Inputs Actual Cost) \$150,000 \$25,000		3)	\$17,381	
Site Preparation (User Inputs Actual Cost)	Painting (0.02 * B)		\$34,763	
Facilities and Buildings (User Inputs Actual Cost) Total Direct Cost \$25,000 \$2,451,963 \$173,814 \$173,81 \$173,814 \$173,814 \$173,814 \$173,814 \$173,814 \$173,814 \$173,814 \$173,814 \$173,814 \$173,814 \$173,814 \$173,814 \$173,814 \$173,814 \$173,814 \$173,814 \$173,814 \$1				\$538,823
Total Direct Cost S2,451,963				
Indirect Cost (Installation) Engineering (0.10 ° B) \$173,814 \$173,814 \$86,907 \$173,814	Facilities and Buildings (User I	•	\$25,000	
Engineering (0.10 * B) Construction and Field Expenses (0.05 *B) Construction and Field Expenses (0.05 *B) Contractor Fees (0.10 *B) Start-Up (0.02 *B) Performance Test (0.01 *B) Contingencies (0.03 * B) Total Indirect Cost = \$538,823 TOTAL CAPITAL INVESTMENT = \$2,990,78 Direct Annual Costs (DC) Operating Labor Operating Labor Operating Materials Giff Any) Maintenance Labor = (hr/shift * shifts/day * days/yr * \$/hr)		Total Direct Cost =		\$2,451,963
Construction and Field Expenses (0.05 *B) \$86,907 \$173,814 \$173,814 \$247-Up (0.02 *B) \$347,763 \$173,814 \$247-Up (0.02 *B) \$173,814 \$247-Up (0.02 *B) \$173,814 \$247-Up (0.02 *B) \$173,814 \$252,144 \$252,144 \$252,910,783 \$252,144 \$253,823 \$252,144 \$253,823 \$252,144 \$253,823 \$252,910,783 \$253,823 \$252,910,783 \$252,910,783 \$253,823 \$252,910,783 \$253,823 \$252,910,783 \$253,823 \$252,910,783 \$253,823 \$252,910,783 \$253,823 \$252,910,783 \$253,823 \$252,910,783 \$253,823 \$252,910,783 \$253,823 \$252,910,783 \$253,823 \$252,910,783 \$253,823 \$253,				
Contractor Fees (0.10 *B) Start-Up (0.02 *B) Start-Up (0.02 *B) Start-Up (0.02 *B) Start-Up (0.02 *B) Start-Up (0.03 *B)				
Start-Up (0.02 *B)		es (0.05 *B)		
Performance Test (0.01 *B) Contingencies (0.03 * B) Total Indirect Cost = \$538,825			\$173,814	
S52,144 \$538,823				
Total Indirect Cost = \$538,823				
Direct Annual Costs (DC)	Contingencies (0.03 * B)		\$52,144	
Direct Annual Costs (DC) Operating Labor				
Operator (Basis of Calculations) Operator = (hr/shift * shifts/day * days/yr * \$/hr) 0.50 \$16,42 Supervisor = (15% of Operator Cost) \$2,46 Operating Materials (If Any) \$2,46 Maintenance Labor = (hr/shift * shifts/day * days/yr * \$/hr) 0.20 \$6,57 Maintenance Materials = 100% of Maintenance Labor \$6,57 Replacement Labor (Actual Cost Per User) \$6,57 Parts Cost (5% of Purchased Cost) \$300 Utilities: Liquid Waste Disposal = \$/lb * lb/hr * 8760 hr/yr 300 \$394,20 Electricity = \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr 45 \$17,00 Water = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 45 \$78,05 Caustic = b/hr caustic * \$/lb*8760 40 \$108,62 Caustic = b/hr caustic * \$/lb*8760 70tal DC = \$686,08 Indirect Annual Costs (IC) Overhead = 60% of the Sum of Total Labor \$32,029 \$19,21 Administrative		TOTAL CAPITAL INVESTMENT =		\$2,990,787
Operator = (hr/shift * shifts/day * days/yr * \$/hr) 0.50 \$16,42 Supervisor = (15% of Operator Cost) \$2,46 Operating Materials (lf Any) \$3 Maintenance Labor = (hr/shift * shifts/day * days/yr * \$/hr) 0.20 \$6,57 Maintenance Materials = 100% of Maintenance Labor \$6,57 Replacement Labor (Actual Cost Per User) \$6,57 Parts Cost (5% of Purchased Cost) \$300 Utilities: \$1,000 gal * bl/hr * 8760 hr/yr 45 \$17,05 Utilities: \$1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 40 \$56,13 Water \$1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 45 \$78,05 Caustic \$1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 45 \$78,05 Caustic \$1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 45 \$78,05 Caustic \$1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 45 \$78,05 Caustic \$1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 45 \$78,05 Overhead = 60% of the Sum of Total Labor		(Pagin of Calculations)		
Supervisor			0.50	₾4.C. 4.O.E
Operating Materials (If Any) \$ Maintenance Labor = (hr/shift * shifts/day * days/yr * \$/hr) 0.20 \$6,57 Maintenance Materials = 100% of Maintenance Labor \$6,57 Replacement Labor (Actual Cost Per User) \$ Parts Cost (5% of Purchased Cost) \$ Utilities: Liquid Waste Disposal = \$/lb * lb/hr * 8760 hr/yr 300 \$394,20 Electricity = \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr 45 \$17,05 Waster = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 40 \$56,13 Wastewater = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 45 \$78,05 Caustic = lb/hr caustic * \$/lb*8760 40 \$108,62 Mainistrative = \$0% of the Sum of Total Labor \$32,029 \$19,21 Administrative = 2% of Total Capital Investment \$59,81 Property Tax = 1% of Total Capital Investment \$29,90 Insurance = 1% of Total Capital Investment \$29,90 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185)			0.50	
Maintenance Labor = (hr/shift * shifts/day * days/yr * \$/hr) 0.20 \$6,57 Maintenance Materials = 100% of Maintenance Labor \$6,57 Replacement Labor (Actual Cost Per User) \$ Parts Cost (5% of Purchased Cost) \$ Utilities: Liquid Waste Disposal = \$/lb * lb/hr * 8760 hr/yr 300 \$394,20 Electricity = \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr 45 \$17,05 Water = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 40 \$56,13 Wastewater = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 45 \$78,05 Caustic = lb/hr caustic * \$/lb*8760 40 \$108,62 Indirect Annual Costs (IC) Total DC = \$686,08 Verhead = 60% of the Sum of Total Labor \$32,029 \$19,21 Administrative = 2% of Total Capital Investment \$29,90 Property Tax = 1% of Total Capital Investment \$29,90 Insurance = 1% of Total Capital Investment \$29,90 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) Total IC = \$443,46 TO	11 .			
Maintenance Materials = 100% of Maintenance Labor \$6,57 Replacement Labor (Actual Cost Per User) \$ Parts Cost (5% of Purchased Cost) \$ Utilities: Liquid Waste Disposal = \$/lb * lb/hr * 8760 hr/yr 300 \$394,20 Electricity = \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr 45 \$17,05 Water = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 40 \$56,13 Wastewater = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 45 \$78,05 Caustic = lb/hr caustic * \$/lb*8760 40 \$108,62 Indirect Annual Costs (IC) Total DC = \$686,08 Overhead = 60% of the Sum of Total Labor \$32,029 \$19,21 Administrative = 2% of Total Capital Investment \$59,81 Property Tax = 1% of Total Capital Investment \$29,90 Insurance = 1% of Total Capital Investment \$29,90 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$304,61 Total IC = \$443,46 Total IC = \$1,129,548			0.00	\$0 \$6.570
Replacement Labor (Actual Cost Per User) (5% of Purchased Cost) Utilities: Liquid Waste Disposal = \$/lb * lb/hr * 8760 hr/yr 300 \$394,20 \$17,05 \$17,			0.20	
Parts Cost (5% of Purchased Cost) Utilities: Liquid Waste Disposal = \$/lb * lb/hr * 8760 hr/yr 300 \$394,20 Electricity = \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr 45 \$17,05 Water = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 40 \$56,13 Wastewater = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 45 \$78,05 Caustic = lb/hr caustic * \$/lb*8760 40 \$108,62 Indirect Annual Costs (IC) Overhead = 60% of the Sum of Total Labor \$32,029 \$19,21 Administrative = 2% of Total Capital Investment \$59,81 Property Tax = 1% of Total Capital Investment \$29,90 Insurance = 1% of Total Capital Investment \$29,90 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$304,61 Total IC = TOTAL ANNUAL OPERATING COSTS = \$1,129,548				. ,
Utilities: Liquid Waste Disposal = \$/lb * lb/hr * 8760 hr/yr 300 \$394,20 Electricity = \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr 45 \$17,05 Water = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 40 \$56,13 Wastewater = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 45 \$78,05 Caustic = lb/hr caustic * \$/lb*8760 40 \$108,62 Indirect Annual Costs (IC) Total DC = \$686,08 Overhead = 60% of the Sum of Total Labor \$32,029 \$19,21 Administrative = 2% of Total Capital Investment \$59,81 Property Tax = 1% of Total Capital Investment \$29,90 Insurance = 1% of Total Capital Investment \$29,90 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$304,61 Total IC = TOTAL ANNUAL OPERATING COSTS = \$1,129,548				\$0 \$0
Liquid Waste Disposal = \$/lb * lb/hr * 8760 hr/yr 300 \$394,20		(5% OF PUTCHASED COST)		\$0
Electricity		- ¢/lb * lb/br * 9760 br//r	200	#204.000
Water = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 40 \$56,13 Wastewater = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 45 \$78,05 Caustic \$10,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 45 \$78,05 Caustic \$10,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 45 \$78,05 Total DC = \$686,08 Total DC = \$686,08 Total DC = \$686,08 Total Capital Labor \$32,029 \$19,21 Administrative = 2% of Total Capital Investment \$59,81 Property Tax = 1% of Total Capital Investment \$29,90 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$304,61 Total IC = \$443,46 TOTAL ANNUAL OPERATING COSTS = \$1,129,548	II			
Wastewater = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 45 \$78,05 Caustic * \$/1b*8760 40 \$108,62 Indirect Annual Costs (IC) Overhead = 60% of the Sum of Total Labor \$32,029 \$19,21 Administrative = 2% of Total Capital Investment \$59,81 Property Tax = 1% of Total Capital Investment \$29,90 Insurance = 1% of Total Capital Investment \$29,90 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) Total IC = \$443,46 TOTAL ANNUAL OPERATING COSTS = \$1,129,548	11			
Caustic = b/hr caustic * \$/ b*8760 40 \$108,62 Indirect Annual Costs (IC) Overhead = 60% of the Sum of Total Labor \$32,029 \$19,21 Administrative = 2% of Total Capital Investment \$59,81 Property Tax = 1% of Total Capital Investment \$29,90 Insurance = 1% of Total Capital Investment \$29,90 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) Total IC = \$443,46 TOTAL ANNUAL OPERATING COSTS = \$1,129,548				
Indirect Annual Costs (IC) Overhead				
Indirect Annual Costs (IC) Overhead	Caustic	=ID/Nr caustic " \$/ID^8/6U		
Overhead = 60% of the Sum of Total Labor \$32,029 \$19,21 Administrative = 2% of Total Capital Investment \$59,81 Property Tax = 1% of Total Capital Investment \$29,90 Insurance = 1% of Total Capital Investment \$29,90 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$304,61 Total IC = \$443,46 TOTAL ANNUAL OPERATING COSTS = \$1,129,548	Indirect Appual Costs (IC)		rolar DC =	\$086,088
Administrative = 2% of Total Capital Investment \$59,81 Property Tax = 1% of Total Capital Investment \$29,90 Insurance = 1% of Total Capital Investment \$29,90 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$304,61 Total IC = \$443,46 TOTAL ANNUAL OPERATING COSTS = \$1,129,548		- 60% of the Sum of Total Labor	¢32 U20	¢10 247
Property Tax = 1% of Total Capital Investment \$29,90 Insurance = 1% of Total Capital Investment \$29,90 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$304,61 Total IC = \$443,46 TOTAL ANNUAL OPERATING COSTS = \$1,129,548			φ3 ∠ ,0 ∠ 9	
Insurance = 1% of Total Capital Investment \$29,90 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$304,61 Total IC = \$443,46 TOTAL ANNUAL OPERATING COSTS = \$1,129,548				
Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$304,61 Total IC = \$443,46 TOTAL ANNUAL OPERATING COSTS = \$1,129,548	 	·		
Total IC = \$443,46 TOTAL ANNUAL OPERATING COSTS = \$1,129,548				
TOTAL ANNUAL OPERATING COSTS = \$1,129,548	Capital Recovery (Bas	ed on 8% & 20 year life: Factor = 0.10185)	Total IC	
		TOTAL ANNUAL OPERATING COSTS -	i olai i o =	
Carrier Cas Addition Nitrogen		Carrier Gas Addition - Nitrogen		ψ1,123,340

Carrier Gas Addition - Nitrogen

Nitrogen for carrier \$/1000 scf * scfm carrier gas *60 min/hr*8760 hr/yr 20,000 \$17,082,000

VENT SCRUBBER VOC COST TABLES VENT SCRUBBER THERMAL OXIDIZER

COST ITEM	is. Vehdor Quotations, OAQES Cost Mandai (Sixtif Editi	COST	TOTALS
Direct Costs			
Purchased Equipment Costs: One 25	5,000 acfm TO Unit		
Thermal Oxidizer (Input Cost: Ver	dor Info and QAQPS USEPA Factor)	\$500,000	
Ancillary Equipment	·	\$75,000	N/A
Fan		\$25,000	
Ancillary Equipment		\$3,750	
, , ,		Sum = "A" =	\$603,750
Instrumentation (0.10 * A)		\$60,375	,
Sales Taxes (0.03 * A)		\$18,113	
Freight (0.05 * A)		\$30,188	
,	Purchased Equipment Cost = "B" =		\$712,425
Direst Installation Costs	· ·		
Foundation and Supports (0.08 * B)		\$56,994	
Handling and Errection (0.14 * B)		\$99,740	
Electrical (0.04 * B)		\$28,497	
Piping, Ductwork, and Installation (0.	02 *B)	\$14,249	
Insulation for Ductwork (0.01 * B)	<i>3</i> = <i>3</i> ,	\$7,124	
Painting (0.01 * B)		\$7,124	
r aming (0.01 b)	Direct Installation Cost =	Ψ,121	\$213,728
Site Preparation (User Inputs Actual		\$150,000	φ2 10,120
Facilities and Buildings (User Inputs		\$25,000	
r dominee and Bananige (eeer inpute	Total Direct Cost =	μ Ψ20,000	\$1,101,153
Indirect Cost (Installation)			+ 1,101,100
Engineering (0.10 * B)		\$71,243	
Construction and Field Expenses (0.0)5 *R)	\$35,621	
Contractor Fees (0.10 *B)	,e 5,	\$71,243	
Start-Up (0.02 *B)		\$14,249	
Performance Test (0.01 *B)		\$7,124	
Contingencies (0.03 * B)		\$21,373	
Contingencies (0.05 b)	Total Indirect Cost =	Ψ21,373	\$220,852
	TOTAL CAPITAL INVESTMENT =		\$1,322,004
Direct Annual Costs (DC)			\$1,022,00 1
Operating Labor	(Basis of Calculations)		
Operator	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$32,850
Supervisor	= (15% of Operator Cost)	0.0	\$4,928
Operating Materials	(If Any)		\$0
Maintenance Labor	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$5,475
Maintenance Materials	= 100% of Maintenance Labor	0.0	\$5,475
Replacement Labor	N/A		\$0
Parts Cost	N/A		\$0
Utilities:	14/1		Ψ
Fuel (natural gas)	(cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	536.9	\$970,693
Electricity	= \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr	31.5	\$11,935
	with the father than the proof in yi	Total DC =	\$1,031,355
Indirect Annual Costs (IC)		. 3.0. 20 =	ψ1,001,000
Overhead	= 60% of the Sum of Total Labor + Materials	\$48,728	\$29,237
Administrative	= 2% of Total Capital Investment	ψ.o,. 20	\$26,440
Property Tax	= 1% of Total Capital Investment		\$13,220
Insurance	= 1% of Total Capital Investment		\$13,220
Capital Recovery	(Based on 8% & 20 year life: Factor = 0.1	0185)	\$134,646
	(2000 011 070 0 20 your mo. 1 dotor = 0.1	Total IC =	\$216,763
	TOTAL ANNUAL OPERATING COSTS =	. 3.0 0	\$1,248,118
	. STATE ANTONIA OF ENAMENTS OF E		Ψ·,= /0,110

VENT SCRUBBER CATALYTIC THERMAL OXIDIZER

COST ITEM		COST	TOTALS
Direct Costs			
Purchased Equipment Costs: One 2	5,000 acfm CTO Unit		
Thermal Oxidizer (User Input Cos	t: Vendor Info and QAQPS USEPA Factor)	\$ 1,000,000	
Ancillary Equipment		\$150,000	N/A
Fan		\$25,000	
Ancillary Equipment		\$3,750	
1 1 1 1 1		Sum = "A" =	\$ 1,178,750.00
Instrumentation (0.10 * A)		\$117,875	, , , ,
Sales Taxes (0.03 * A)		\$35,363	
Freight (0.05 * A)		\$58,938	
1 10ight (0.00 7t)	Purchased Equipment Cost = "B" =		\$1,390,925
Direst Installation Costs	- aronacca =qarpment coct =		ψ1,000,020
Foundation and Supports (0.08 * B)		\$111,274	
Handling and Errection (0.14 * B)		\$111,274 \$194,730	
Electrical (0.04 * B)	20 *D)	\$55,637	
Piping, Ductwork and Installation (0.0	JZ "B)	\$27,819	
Insulation for Ductwork (0.01 * B)		\$13,909	
Painting (0.01 * B)		\$13,909	
	Direct Installation Cost =		\$417,278
Site Preparation (User Inputs Actual		\$150,000	
Facilities and Buildings (User Inputs		\$25,000	
	Total Direct Cost =		\$1,983,203
Indirect Cost (Installation)			
Engineering (0.10 * B)		\$139,093	
Construction and Field Expenses (0.	05 *B)	\$69,546	
Contractor Fees (0.10 *B)	,	\$139,093	
Start-Up (0.02 *B)		\$27,819	
Performance Test (0.01 *B)		\$13,909	
Contingencies (0.03 * B)		\$41,728	
g(Total Indirect Cost =	4 ,. = 5	\$431,187
	TOTAL CAPITAL INVESTMENT =		\$2,414,389
Direct Annual Costs (DC)			
Operating Labor	(Basis of Calculations)		
Operator	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$14,600
Supervisor	= (15% of Operator Cost)	0.5	\$2,190
			\$0
Operating Materials	(If Any) = (hr/shift * shifts/day * days/yr * \$/hr)	0.5	•
Maintenance Labor		0.5	\$14,600 \$14,600
Maintenance Materials	= 100% of Maintenance Labor		\$14,600
Replacement Labor	N/A	22	\$0
Catalyst Cost	= CF cat* \$850/CF* 1@2 years	20	\$8,500
Utilities:	/	4====	
Fuel (natural gas)	(cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	179.0	\$615,609
Electricity	= \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr	31.5	\$11,935
		Total DC =	\$682,034
Indirect Annual Costs (IC)		_	
Overhead	= 60% of the Sum of Total Labor + Materials	\$45,990	\$27,594
Administrative	= 2% of Total Capital Investment		\$48,288
Property Tax	= 1% of Total Capital Investment		\$24,144
Insurance	= 1% of Total Capital Investment		\$24,144
Capital Recovery	(Based on 8% & 20 year life: Factor = 0.1	0185)	\$245,906
		Total IC =	\$370,075
	TOTAL ANNUAL OPERATING COSTS =		\$1,052,109

VENT SCRUBBER REGENERATIVE THERMAL OXIDIZER

COST ITEM	is. Vendor Quotations, OAQI 5 Cost Mandai (Sixtii Editi	COST	TOTALS
Direct Costs			
Purchased Equipment Costs			
	t: Vendor Info and QAQPS USEPA Factor)	560,000	
Ancillary Equipment	,	\$84,000	N/A
Fan		\$25,000	
Ancillary Equipment		\$3,750	
· · · · · · · · · · · · · · · · · · ·		Sum = "A" =	672,750
Instrumentation (0.10 * A)		\$67,275	5,. 55
Sales Taxes (0.03 * A)		\$20,183	
Freight (0.05 * A)		\$33,638	
Treight (0.00 7t)	Purchased Equipment Cost = "B" =		\$793,845
Direst Installation Costs			7.00,010
Foundation and Supports (0.08 * B)		\$63,508	
Handling and Errection (0.14 * B)		\$111,138	
Electrical (0.04 * B)		\$111,136 \$31,754	
	00 *D)		
Piping, Ductwork, and Installation (0.	U2 B)	\$15,877	
Insulation for Ductwork (0.01 * B)		\$7,938	
Painting (0.01 * B)	D: (1 (1 1 0)	\$7,938	0000454
G: 5	Direct Installation Cost =	II #450.000	\$238,154
Site Preparation (User Inputs Actual		\$150,000	
Facilities and Buildings (User Inputs		\$25,000	
	Total Direct Cost =	1.	\$1,206,999
Indirect Cost (Installation)			
Engineering (0.10 * B)		\$79,385	
Construction and Field Expenses (0.	05 *B)	\$39,692	
Contractor Fees (0.10 *B)		\$79,385	
Start-Up (0.02 *B)		\$15,877	
Performance Test (0.01 *B)		\$7,938	
Contingencies (0.03 * B)		\$23,815	
	Total Indirect Cost =		\$246,092
	TOTAL CAPITAL INVESTMENT =		\$1,453,090
Direct Annual Costs (DC)			
Operating Labor	(Basis of Calculations)		
Operator	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$16,425
Supervisor	= (15% of Operator Cost)		\$2,464
Operating Materials	(If Any)		\$0
Maintenance Labor	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$16,425
Maintenance Materials	= 100% of Maintenance Labor		\$16,425
Replacement Labor	N/A		\$0
Parts Cost	N/A		\$0
Utilities:	I V/C		ΨΟ
Fuel (natural gas)	(cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	107.4	\$369,366
Electricity	= \$/kWhr* kWhr *8760 hr/yr	80.0	\$309,300 \$40,646
Media Replacement	= 5/kvviii kvviii 6/60/ii/yi = CF media * \$50/CF / 3 years	750.0	\$40,646 \$12,500
iviedia Nepiacement	= Or media \$30/OF / 3 years	Total DC =	\$12,500 \$474,251
Indirect Annual Costs (IC)		Total DC =	φ414,231
Overhead	= 60% of the Sum of Total Labor + Materials	\$51,739	¢24.042
		Ф Э1,739	
Administrative	= 2% of Total Capital Investment		\$29,062
Property Tax	= 1% of Total Capital Investment		\$14,531
Insurance	= 1% of Total Capital Investment	0.4.0.5\	\$14,531
Capital Recovery	(Based on 8% & 20 year life: Factor = 0.1		\$147,997
		Total IC =	\$237,164
	TOTAL ANNUAL OPERATING COSTS =		\$711,415

VENT SCRUBBER RECUPERATIVE THERMAL OXIDIZER

COST ITE	Л	COST	TOTALS
Direct Costs			
Purchased Equipment Costs:			
Thermal Oxidizer (User Input Cos	t: Vendor Info and QAQPS USEPA Factor)	\$960,000	
Ancillary Equipment		\$144,000	N/A
Fan		\$25,000	
Ancillary Equipment		\$3,750	
		Sum = "A" =	\$1,132,750
Instrumentation (0.10 * A)		\$113,275	
Sales Taxes (0.03 * A)		\$33,983	
Freight (0.05 * A)		\$56,638	
,	Purchased Equipment Cost = "B" =		\$1,336,645
Direst Installation Costs			
Foundation and Supports (0.08 * B)		\$106,932	
Handling and Errection (0.14 * B)		\$187,130	
Electrical (0.04 * B)		\$53,466	
Piping, Ductwork, and Installation (0.	02 *B)	\$26,733	
Insulation for Ductwork (0.01 * B)	02 0)	\$13,366	
Painting (0.01 * B)		\$13,366	
Fairting (0.01 B)	Direct Installation Cost =	\$13,300	\$400,994
Site Preparation (User Inputs Actual		\$150,000	<i>ф400,994</i>
		\$150,000	
Facilities and Buildings (User Inputs	Total Direct Cost =	\$25,000	¢4 042 620
	Total Direct Cost =	Ti .	\$1,912,639
Indirect Cost (Installation)			
Engineering (0.10 * B)		\$133,665	
Construction and Field Expenses (0.	05 *B)	\$66,832	
Contractor Fees (0.10 *B)		\$133,665	
Start-Up (0.02 *B)		\$26,733	
Performance Test (0.01 *B)		\$13,366	
Contingencies (0.03 * B)		\$40,099	
	Total Indirect Cost =		\$414,360
	TOTAL CAPITAL INVESTMENT =		\$2,326,998
Direct Annual Costs (DC)			
Operating Labor	(Basis of Calculations)		
Operator	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$16,425
Supervisor	= (15% of Operator Cost)		\$2,464
Operating Materials	(If Any)		\$0
Maintenance Labor	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$16,425
Maintenance Materials	= 100% of Maintenance Labor		\$16,425
Replacement Labor	N/A		\$0
Parts Cost	N/A		\$0
Utilities:			ΨΟ
Fuel (natural gas)	(cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	268.4	\$923,414
Electricity	= \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr	26.0	\$9,851
Licotricity	- ψ/ΚΥΥΠΙ ΤΙΡ Τ ΚΥΥΠΙ/ 1.0+1 ΤΙΡ 0/ 00 ΠΙ/ΥΙ	Total DC =	\$985,003
Indirect Annual Costs (IC)		, star 20 =	ψ300,003
Overhead	= 60% of the Sum of Total Labor + Materials	\$51,739	\$31,043
Administrative		φυ1,739	· ·
	= 2% of Total Capital Investment		\$46,540 \$22,270
Property Tax	= 1% of Total Capital Investment		\$23,270
Insurance	= 1% of Total Capital Investment	0405)	\$23,270
Capital Recovery	(Based on 8% & 20 year life: Factor = 0.1		\$258,367
	TOTAL ANNUAL OPERATING COOLS	Total IC =	\$382,490
	TOTAL ANNUAL OPERATING COSTS =		\$1,367,493

VENT SCRUBBER WET SCRUBBER

COST ITEM	COST	TOTALS
Direct Costs		
Purchased Equipment Costs: Scrubber	* 4 7 0 000	
Scrubber (User Input Cost: Vendor Info)	\$470,000	NI/A
Ancillary Equipment Fan	\$70,500 \$35,000	N/A
Ancillary Equipment	\$25,000 \$3,750	
Andmary Equipment	Sum = "A" =	\$569,250
Instrumentation (0.10 * A)	\$51,233	φ503,250
Sales Taxes (0.03 * A)	\$28,463	
Freight (0.05 * A)	\$45,540	
Purchased Equipment Cost = "B" =		\$694,485
Direst Installation Costs		
Foundation and Supports (0.12 * B)	\$83,338	
Handling and Errection (0.40 * B)	\$277,794	
Electrical (0.01 * B)	\$6,945	
Piping, Ductwork, and Installation (0.30 *B)	\$208,346	
Insulation (0.01 * B)	\$6,945	
Painting (0.01 * B)	\$6,945	4
Direct Installation Cost =	II #450.000	\$590,312
Site Preparation (User Inputs Actual Cost)	\$150,000	
Facilities and Buildings (User Inputs Actual Cost) Total Direct Cost =	\$25,000	\$1,459,797
	1	\$1, 4 59,797
Indirect Cost (Installation) Engineering (0.10 * B)	\$69,449	
Construction and Field Expenses (0.10 *B)	\$69,449 \$69,449	
Contractor Fees (0.10 *B)	\$69,449	
Start-Up (0.01 *B)	\$6,945	
Performance Test (0.01 *B)	\$6,945	
Contingencies (0.03 * B)	\$20,835	
Total Indirect Cost =		\$243,070
TOTAL CAPITAL INVESTMENT =	-1	\$1,702,867
Direct Annual Costs (DC)		
Operating Labor (Basis of Calculations)		
Operator = (hr/shift * shifts/day * days/yr * \$/hr)	0.50	\$16,425
Supervisor = (15% of Operator Cost)		\$2,464
Operating Materials (If Any)		\$0
Maintenance Labor = (hr/shift * shifts/day * days/yr * \$/hr)	0.50	\$16,425
Maintenance Materials = 100% of Maintenance Labor		\$16,425
Replacement Labor (Actual Cost Per User)		\$0
Parts Cost (5% of Purchased Cost)		\$0
Utilities:	40	40.700
Electricity = \$/kWhr * hp * 1 kWhr/1.341 hp * 8760 hr/yr	10	\$3,789
Water = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr	38	\$53,327
Wastewater = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr	38	\$65,910
Caustic = b/hr * \$/lb * 8760 hr/yr	46.3 Total DC =	\$125,597 \$200,262
Indirect Annual Costs (IC)	i Ulai DC =	\$300,362
Overhead = 60% of the Sum of Total Labor	\$51,739	\$31,043
Administrative = 2% of Total Capital Investment	ψο 1,7 ο σ	\$31,043 \$34,057
Property Tax = 1% of Total Capital Investment		\$17,029
Insurance = 1% of Total Capital Investment		\$17,029
Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185)		\$173,437
(2.5.5.3.5.7.5.5.7.5.6.5.7.5.7.7.6.6.7.7.6.6.7.7.6.6.7.7.6.6.7.7.6.6.7.7.6.6.7.7.6.6.7.7.6.6.7.7.6.6.7.7.6.6.7.7.6.6.7.7.6.6.7.7.6.6.7.7.6.6.7.7.6.6.7.7.6.7.7.6.7.7.6.7.7.6.7.7.6.7.7.6.7	Total IC =	\$272,595
TOTAL ANNUAL OPERATING COSTS =		\$572,957

VENT SCRUBBER REFRIGERATED CONDENSER

COST ITEM	COST	TOTALS
Direct Costs		
Purchased Equipment Costs: Refrigerated Condenser		
Condenser (User Input Cost: QAQPS Info)	\$219,000	
Ancillary Equipment	\$54,750	N/A
Fan	\$25,000	
Ancillary Equipment	\$3,750	
	Sum = "A" =	\$302,500
Instrumentation (0.10 * A)	\$30,250	
Sales Taxes (0.03 * A)	\$9,075	
Freight (0.05 * A)	\$15,125	
Purchased Equipment Cost = "B" =	=	\$356,950
Direst Installation Costs		
Foundation & Supports (0.08 * B)	\$28,556	
Handling & Errection (0.14 * B)	\$49,973	
Electrical (0.04 * B)	\$14,278	
Piping, Ductwork & Installation (0.02 *B)	\$7,139	
Insulation for Ductwork (0.01 * B)	\$3,570	
Painting (0.02 * B)	\$7,139	
Direct Installation Cost =	"	\$110,655
Site Preparation (User Inputs Actual Cost)	\$150,000	4110,000
Facilities & Buildings (User Inputs Actual Cost)	\$25,000	
Total Direct Cost =	Ψ20,000	\$642,605
Indirect Cost (Installation)		φο 12,000
Engineering (0.10 * B)	\$35,695	
Construction & Field Expenses (0.05 *B)		
	\$17,848	
Contractor Fees (0.10 *B)	\$35,695	
Start-Up (0.02 *B)	\$7,139	
Performance Test (0.01 *B)	\$3,570	
Contingencies (0.03 * B)	\$10,709	¢440.055
Total Indirect Cost =		\$110,655
TOTAL CAPITAL INVESTMENT =		\$753,259
Direct Annual Costs (DC)		
Operating Labor (Basis of Calculations)		A
Operator = (hr/shift * shifts/day * days/yr * \$/hr)	0.50	\$16,425
Supervisor = (15% of Operator Cost)		\$2,464
Operating Materials (If Any)		\$0
Maintenance Labor = (hr/shift * shifts/day * days/yr * \$/hr)	0.20	\$6,570
Maintenance Materials = 100% of Maintenance Labor		\$6,570
Replacement Labor (Actual Cost Per User)		\$0
Parts Cost (5% of Purchased Cost)		\$0
Utilities:		
Liquid Waste Disposal = \$/lb * lb/hr * 8760 hr/yr	140	\$183,960
Electricity = \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr	45	\$17,050
Wastewater = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr	1	\$1,734
	Total DC =	\$233,038
Indirect Annual Costs (IC)		
Overhead = 60% of the Sum of Total Labor	\$32,029	\$19,217
Administrative = 2% of Total Capital Investment		\$15,065
Property Tax = 1% of Total Capital Investment		\$7,533
Insurance = 1% of Total Capital Investment		\$7,533
Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185)		\$76,719
	Total IC =	\$126,067
TOTAL ANNUAL OPERATING COSTS =		\$359,105

FUGITIVES VOC COST TABLES Existing LDAR Program

COST ITEM	1	COST	TOTALS
Direct Annual Costs (DC) Operating Labor LDAR Technician Supervisor Repairs Labor	(Basis of Calculations) = (hrs/month* 12 * \$/hr) = (hrs/month* 12 * \$/hr) = (hrs/month* 12 * \$/hr)	120 10 3	\$64,800 \$7,800 \$1,620
Repairs Materials	= 100% of Maintenance Labor	Total DC =	\$1,620 \$1,620 <i>\$75,840</i>
	TOTAL ANNUAL OPERATING COSTS =		\$75,840

Upgrade NSPS VV Portion to NSPS Vva

COST ITEM		COST	TOTALS
Direct Annual Costs (DC) Operating Labor LDAR Technician Supervisor Repairs Labor	(Basis of Calculations) = (hrs/month* 12 * \$/hr) = (hrs/month* 12 * \$/hr) = (hrs/month* 12 * \$/hr)	135 10 8	\$72,900 \$7,800 \$4,320
Repairs Materials	= 100% of Maintenance Labor	Total DC =	\$4,320 \$89.340
	TOTAL ANNUAL OPERATING COSTS =	Total DC =	\$89,340

Upgrade NSPS VV Portion to HON

COST ITEM		COST	TOTALS
Direct Annual Costs (DC) Operating Labor	(Basis of Calculations)		
LDAR Technician	= (hrs/month* 12 * \$/hr)	145	\$78,300
Supervisor	= (hrs/month* 12 * \$/hr)	10	\$7,800
Repairs Labor	= (hrs/month* 12 * \$/hr)	20	\$10,800
Repairs Materials	= 100% of Maintenance Labor		\$10,800
		Total DC =	\$107,700
	TOTAL ANNUAL OPERATING COSTS =		\$107,700

LPA CO COST TABLES LPA THERMAL OXIDIZER

COST ITEM	15. Vehidor Quotations, OAQES Cost Mandai (Sixtif Editi	COST	TOTALS
Direct Costs			
Purchased Equipment Costs: One 2,	500 acfm TO Unit		
Thermal Oxidizer (Input Cost: Ver	ndor Info and QAQPS USEPA Factor)	\$380,000	
Ancillary Equipment		\$57,000	N/A
Blower		\$30,000	
Ancillary Equipment		\$4,500	
		Sum = "A" =	\$471,500
Instrumentation (0.10 * A)		\$47,150	
Sales Taxes (0.03 * A)		\$14,145	
Freight (0.05 * A)		\$23,575	
	Purchased Equipment Cost = "B" =	<u> </u>	\$556,370
Direst Installation Costs		* • • • • • • • • • • • • • • • • • • •	
Foundation and Supports (0.08 * B)		\$44,510	
Handling and Errection (0.14 * B)		\$77,892	
Electrical (0.04 * B)		\$22,255	
Piping, Ductwork, and Installation (0.	02 *B)	\$11,127	
Insulation for Ductwork (0.01 * B)		\$5,564	
Painting (0.01 * B)		\$5,564	
	Direct Installation Cost =	II	\$166,911
Site Preparation (User Inputs Actual		\$150,000	
Facilities and Buildings (User Inputs		\$25,000	# 200 004
	Total Direct Cost =		\$898,281
Indirect Cost (Installation)			
Engineering (0.10 * B)		\$55,637	
Construction and Field Expenses (0.	05 *B)	\$27,819	
Contractor Fees (0.10 *B)		\$55,637	
Start-Up (0.02 *B)		\$11,127	
Performance Test (0.01 *B)		\$5,564	
Contingencies (0.03 * B)		\$16,691	
	Total Indirect Cost =		\$172,475
	TOTAL CAPITAL INVESTMENT =		\$1,070,756
Direct Annual Costs (DC)			
Operating Labor	(Basis of Calculations)		• • • • • •
Operator	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$32,850
Supervisor	= (15% of Operator Cost)		\$4,928
Operating Materials	(If Any)		\$0
Maintenance Labor	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$5,475
Maintenance Materials	= 100% of Maintenance Labor		\$5,475
Replacement Labor	N/A		\$0
Parts Cost	N/A		\$0
Utilities:	/	405.5	A
Fuel (natural gas)	(cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	129.3	\$233,783
Electricity	= \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr	40.5	\$15,345
Indirect Applied Coats (IC)		Total DC =	\$297,855
Indirect Annual Costs (IC)	COOK of the Course of Total I alice a Martinia	Ф40 700	#00.00 7
Overhead	= 60% of the Sum of Total Labor + Materials	\$48,728	\$29,237
Administrative	= 2% of Total Capital Investment		\$21,415
Property Tax	= 1% of Total Capital Investment		\$10,708
Insurance	= 1% of Total Capital Investment	0405)	\$10,708
Capital Recovery	(Based on 8% & 20 year life: Factor = 0.1		\$109,056
	TOTAL ANNUAL OPERATING COSTS	Total IC =	\$181,123
	TOTAL ANNUAL OPERATING COSTS =		\$478,978

LPA CATALYTIC THERMAL OXIDIZER

COST ITEM	Л	COST		TOTALS
Direct Costs				
Purchased Equipment Costs: One 2,	500 acfm CTO Unit			
	t: Vendor Info and QAQPS USEPA Factor)	\$ 560,000		
Ancillary Equipment		\$84,000		N/A
Blower		\$30,000		
Ancillary Equipment		\$4,500		
		Sum = "A" =	\$	678,500.00
Instrumentation (0.10 * A)		\$67,850		
Sales Taxes (0.03 * A)		\$20,355		
Freight (0.05 * A)		\$33,925		
	Purchased Equipment Cost = "B" =			\$800,630
Direst Installation Costs				
Foundation and Supports (0.08 * B)		\$64,050		
Handling and Errection (0.14 * B)		\$112,088		
Electrical (0.04 * B)		\$32,025		
Piping, Ductwork, and Installation (0.	02 *B)	\$16,013		
Insulation for Ductwork (0.01 * B)		\$8,006		
Painting (0.01 * B)		\$8,006		
,	Direct Installation Cost =			\$240,189
Site Preparation (User Inputs Actual	Cost)	\$150,000		
Facilities and Buildings (User Inputs	Actual Cost)	\$25,000		
	Total Direct Cost =			\$1,215,819
Indirect Cost (Installation)				
Engineering (0.10 * B)		\$80,063		
Construction and Field Expenses (0.	05 *B)	\$40,032		
Contractor Fees (0.10 *B)		\$80,063		
Start-Up (0.02 *B)		\$16,013		
Performance Test (0.01 *B)		\$8,006		
Contingencies (0.03 * B)		\$24,019		
	Total Indirect Cost =	V = 1,010		\$248,195
	TOTAL CAPITAL INVESTMENT =	*		\$1,464,014
Direct Annual Costs (DC)				• • • • • • • • • • • • • • • • • • •
Operating Labor	(Basis of Calculations)			
Operator	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5		\$14,600
Supervisor	= (15% of Operator Cost)	0.0		\$2,190
Operating Materials	(If Any)			\$0
Maintenance Labor	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5		\$14,600
Maintenance Materials	= 100% of Maintenance Labor	0.0		\$14,600
Replacement Labor	N/A			\$14,000 \$0
Catalyst Cost	= CF cat* \$850/CF* 1@2 years	30		\$12,750
Utilities:	- OI Cal 4000/OF 1@2 years	30		ψ12,730
Fuel (natural gas)	(cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	47.0		\$84,979
	= \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr	47.0 40.5	I	\$04,979 \$15,345
Electricity	- φ/κνντιι τι ρ τ κνντιί/1.341 τιρ ο/ου π/γΓ	Total DC =		\$15,345 \$159,064
Indirect Annual Costs (IC)		Total DC =		φ109,004
Overhead	= 60% of the Sum of Total Labor + Materials	\$45,990		\$27,594
		φ 4 5,990	I	
Administrative	= 2% of Total Capital Investment			\$29,280
Property Tax	= 1% of Total Capital Investment			\$14,640
Insurance	= 1% of Total Capital Investment	0405)		\$14,640
Capital Recovery	(Based on 8% & 20 year life: Factor = 0.1			\$149,110
	TOTAL ANNUAL OPERATING COSTS	Total IC =		\$235,264
	TOTAL ANNUAL OPERATING COSTS =			\$394,328

LPA REGENERATIVE THERMAL OXIDIZER

COST ITEI	M	COST	TOTALS
Direct Costs			
Purchased Equipment Costs			
	t: Vendor Info and QAQPS USEPA Factor)	430,000	
Ancillary Equipment		\$64,500	N/A
Blower		\$30,000	
Ancillary Equipment		\$4,500	
, , ,		Sum = "A" =	529,000
Instrumentation (0.10 * A)		\$52,900	
Sales Taxes (0.03 * A)		\$15,870	
Freight (0.05 * A)		\$26,450	
,	Purchased Equipment Cost = "B" =		\$624,220
Direst Installation Costs			
Foundation and Supports (0.08 * B)		\$49,938	
Handling and Errection (0.14 * B)		\$87,391	
Electrical (0.04 * B)		\$24,969	
Piping, Ductwork, and Installation (0.	02 *B)	\$12,484	
Insulation for Ductwork (0.01 * B)	,	\$6,242	
Painting (0.01 * B)		\$6,242	
,	Direct Installation Cost =		\$187,266
Site Preparation (User Inputs Actual	Cost)	\$150,000	
Facilities and Buildings (User Inputs		\$25,000	
	Total Direct Cost =		\$986,486
Indirect Cost (Installation)			
Engineering (0.10 * B)		\$62,422	
Construction and Field Expenses (0.	05 *B)	\$31,211	
Contractor Fees (0.10 *B)	,	\$62,422	
Start-Up (0.02 *B)		\$12,484	
Performance Test (0.01 *B)		\$6,242	
Contingencies (0.03 * B)		\$18,727	
	Total Indirect Cost =		\$193,508
	TOTAL CAPITAL INVESTMENT =		\$1,179,994
Direct Annual Costs (DC)			
Operating Labor	(Basis of Calculations)		
Operator	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$16,425
Supervisor	= (15% of Operator Cost)		\$2,464
Operating Materials	(If Any)		\$0
Maintenance Labor	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$16,425
Maintenance Materials	= 100% of Maintenance Labor		\$16,425
Replacement Labor	N/A		\$0
Parts Cost	N/A		\$0
Utilities:			
Fuel (natural gas)	(cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	45.0	\$81,363
Electricity	= \$/kWhr* <mark>kWhr</mark> *8760 hr/yr	48.0	\$24,388
Media Replacement	= CF media * \$50/CF / 2 years	400.0	\$10,000
		Total DC =	<i>\$167,489</i>
Indirect Annual Costs (IC)			
Overhead	= 60% of the Sum of Total Labor + Materials	\$51,739	
Administrative	= 2% of Total Capital Investment		\$23,600
Property Tax	= 1% of Total Capital Investment		\$11,800
Insurance	= 1% of Total Capital Investment	 	\$11,800
Capital Recovery	(Based on 8% & 20 year life: Factor = 0.1		\$120,182
		Total IC =	\$198,425
	TOTAL ANNUAL OPERATING COSTS =		\$365,915

LPA RECUPERATIVE THERMAL OXIDIZER

COST ITEM	Л	COST	TOTALS
Direct Costs			
Purchased Equipment Costs:			
	t: Vendor Info and QAQPS USEPA Factor)	\$650,000	
Ancillary Equipment		\$97,500	N/A
Blower		\$30,000	
Ancillary Equipment		\$4,500	4
		Sum = "A" =	\$782,000
Instrumentation (0.10 * A)		\$78,200	
Sales Taxes (0.03 * A)		\$23,460	
Freight (0.05 * A)	D	\$39,100	¢000 700
	Purchased Equipment Cost = "B" =	<u> </u>	\$922,760
Direst Installation Costs		Ф 7 0 004	
Foundation and Supports (0.08 * B)		\$73,821	
Handling and Errection (0.14 * B)		\$129,186	
Electrical (0.04 * B)	00 # D \	\$36,910	
Piping, Ductwork, and Installation (0.	02 *B)	\$18,455	
Insulation for Ductwork (0.01 * B)		\$9,228	
Painting (0.01 * B)		\$9,228	4
0: 5	Direct Installation Cost =	II #450.000	\$276,828
Site Preparation (User Inputs Actual		\$150,000	
Facilities and Buildings (User Inputs	Actual Cost) Total Direct Cost =	\$25,000	¢4 274 500
	Total Direct Cost =	11	\$1,374,588
Indirect Cost (Installation)		#00.070	
Engineering (0.10 * B)		\$92,276	
Construction and Field Expenses (0.0	J5 ^B)	\$46,138	
Contractor Fees (0.10 *B)		\$92,276	
Start-Up (0.02 *B)		\$18,455	
Performance Test (0.01 *B)		\$9,228	
Contingencies (0.03 * B)	Total Indianat Cont	\$27,683	\$200.0EC
	Total Indirect Cost = TOTAL CAPITAL INVESTMENT =		\$286,056
	TOTAL CAPITAL INVESTMENT =		\$1,660,644
Direct Annual Costs (DC) Operating Labor	(Basis of Calculations)		
Operating Labor Operator	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$16,425
Supervisor	= (11/Silitt Silits/day days/yr \$/fir) = (15% of Operator Cost)	0.5	
			\$2,464
Operating Materials Maintenance Labor	(If Any) = (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$0 \$16,425
	= (m/smit smits/day days/yr \$/m) = 100% of Maintenance Labor	0.5	
Maintenance Materials			\$16,425
Replacement Labor	N/A		\$0 \$0
Parts Cost Utilities:	N/A		\$0
	(ofm/1000 * \$/1000 of * 60 min/hr *0760 h-/)	53.0	₽ 0€ 007
Fuel (natural gas)	(cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	53.0	\$95,827
Electricity	= \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr	40.0 Total DC =	\$15,155 \$162,721
Indirect Annual Costs (IC)		TOTAL DO =	\$162,721
Overhead	= 60% of the Sum of Total Labor + Materials	\$51,739	\$31,043
Administrative		φυ1, <i>1</i> 39	
	= 2% of Total Capital Investment = 1% of Total Capital Investment		\$33,213 \$16,606
Property Tax Insurance	= 1% of Total Capital Investment = 1% of Total Capital Investment		
Capital Recovery	= 1% of Total Capital Investment (Based on 8% & 20 year life: Factor = 0.1	0185)	\$16,606 \$258,367
Capital Necovery	(Dased Oil 0 /0 & 20 year life. Factor = 0.1	Total IC =	\$355,836
	TOTAL ANNUAL OPERATING COSTS =	10tai 10 =	\$518,557
	TOTAL ANNUAL OF ENATING COSTS =		φυ10,001

HPA CO COST TABLES HPA THERMAL OXIDIZER

Site Preparation (User Inputs Actual Cost)	COST ITEM		COST	TOTALS
Thermal Oxidizer (Input Cost: Vendor Info and QAQPS USEPA Factor)				
Ancillary Equipment Sromines Scrubber Side, 2000 S350,000 Ancillary Equipment Side Scrubber Side				
Bromine Scrubber S350,000 \$52,500 S52,500 S52,		ndor Info and QAQPS USEPA Factor)		
Ancillary Equipment				N/A
Instrumentation (0.10 ° A) Sales Taxes (0.03 ° A) Freight (0.05 ° A) \$36,915 \$1,230,500 \$36,915 \$1,230,500 \$36,915 \$1,230,500 \$36,915 \$1,230,500 \$36,915 \$1,451,990 \$1,451,990 \$1,451,990 \$1,451,990 \$1,451,990 \$1,451,990 \$1,451,990 \$1,451,990 \$1,451,990 \$1,4520 \$1,451,990 \$1,4520			II ' '	
Instrumentation (0.10 ° A) Sales Taxes (0.03 ° A) Freight (0.05 ° A) Purchased Equipment Cost = "B" \$113,050 \$36,915 \$116,159 \$116,159 \$116,159 \$20,32.79 \$116,159 \$20,32.79 \$116,159 \$20,32.79 \$116,159 \$20,32.79 \$116,159 \$20,32.79 \$116,159 \$20,32.79 \$116,159 \$20,32.79 \$116,159 \$20,32.79 \$116,159 \$20,32.79 \$116,159 \$20,32.79 \$116,159 \$20,32.79 \$116,159 \$20,940 \$116,150 \$20,940 \$116,150 \$20,940 \$14,520 \$14,520 \$14,520 \$14,520 \$14,520 \$14,520 \$14,520 \$14,520 \$14,520 \$14,520 \$14,520 \$14,520 \$14,520 \$1,45,	Ancillary Equipment			Ø4 000 500
Sales Taxes (0.03 *A)	Instrumentation (0.10 * A)			\$1,230,500
Freight (0.05 * A) Purchased Equipment Cost = "B" = \$1,451,996				
Purchased Equipment Cost = "B" =				
Direct Installation Costs Foundation and Supports (0.08 * B)	Freight (0.05 A)	Purchased Equipment Cost = "B" =		\$1 451 990
Foundation and Supports (0.08 * B)	Direct Installation Costs	Taronacea Equipment ecot = B		ψ1,101,000
Handling and Errection (0.14 * B) \$203,279 \$58,080 \$29,040 \$19ping, Ductwork, and Installation (0.02 * B) \$14,520 \$14,54,199 \$14,			\$116.159	
Electrical (0.04 * B)				
Piping, Ductwork, and Installation (0.02 *B)				
Insulation for Ductwork (0.01 * B)		02 *B)	II .	
Direct Installation Cost = \$435,593		,		
Site Preparation (User Inputs Actual Cost)				
Facilities and Buildings (User Inputs Actual Cost)				\$435,597
Total Direct Cost St. (1,000 St. (1,00			II .	
Indirect Cost (Installation) Engineering (0.10 * B) \$145,199 \$172,600 \$145,199	Facilities and Buildings (User Inputs	·	\$25,000	4
Engineering (0.10 * B)		Total Direct Cost =	<u></u>	\$2,062,587
Construction and Field Expenses (0.05 *B)			* 4.5 4.00	
Contractor Fees (0.10 *B) Start-Up (0.02 *B) S29,040 S29,040 S29,040 S43,560 S45,017; S4		05 45)		
Start-Up (0.02 *B)		05 [*] B)		
Performance Test (0.01 *B)			II .	
Contingencies (0.03 * B) Total Indirect Cost = \$43,560 \$4450,117	Start-Up (0.02 °B)			
Total Indirect Cost = \$450,117				
Direct Annual Costs (DC) Operating Labor	Contingencies (0.03 B)	Total Indirect Cost -	\$43,560	\$450 117
Direct Annual Costs (DC) Operating Labor				
Operator (Basis of Calculations) Operator = (hr/shift * shifts/day * days/yr * \$/hr) 0.5 \$16,42 Supervisor = (15% of Operator Cost) \$2,44 Operating Materials (If Any) \$3,44 Maintenance Labor = (hr/shift * shifts/day * days/yr * \$/hr) 0.2 \$6,57 Maintenance Materials = 100% of Maintenance Labor \$6,57 Replacement Labor N/A \$3,67 Parts Cost N/A \$4,67 Utilities: Fuel (natural gas) (cfm/1000 * \$/1000 cf * 60 min/hr * 8760 hr/yr) 6425.9 \$11,618,42 Electricity = \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr 127.0 \$48,12 Nitrogen for carrier \$/1000 scf * scfm carrier gas *60 min/hr*8760 hr/yr 20000.0 \$17,082,00 Waster = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 76 \$106,55 Wastewater = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 76 \$131,68 Caustic = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 76 \$134,93 Depart Tax = 60% of the Sum of Total Labor + Materials	Direct Annual Costs (DC)	TOTAL OATTIAL INVESTIGENT =		Ψ <u>2,</u> 012,704
Operator		(Basis of Calculations)		
Supervisor		= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$16,425
Operating Materials				\$2,464
Maintenance Labor = (hr/shift * shifts/day * days/yr * \$/hr) 0.2 \$6,57 Maintenance Materials = 100% of Maintenance Labor \$6,57 Replacement Labor N/A \$6,57 Parts Cost N/A \$1 Utilities: Vilities: \$1 Fuel (natural gas) (cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr) 6425.9 \$11,618,42 Electricity = \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr 127.0 \$48,12 Nitrogen for carrier \$/1000 scf * scfm carrier gas *60 min/hr *8760 hr/yr 20000.0 \$17,082,00 Water = \$/1,000 gal * gal/min/1000 * 60 min/hr *8760 hr/yr 76 \$106,55 Wastewater = \$/1,000 gal * gal/min/1000 * 60 min/hr *8760 hr/yr 76 \$131,65 Caustic = \$/1,000 gal * gal/min/1000 * 60 min/hr *8760 hr/yr 76 \$131,65 Doverhead = \$/1,000 gal * gal/min/1000 * 60 min/hr *8760 hr/yr 76 \$131,65 Capital Capital Capital Investment \$29,168,17 Property Tax = 60% of the Sum of Total Labor + Materials \$32,029 \$19,21 Administrative = 2% of Total Capital Investment \$25,12 Property Tax = 1%				\$0
Replacement Labor N/A N/A Parts Cost N/A N/A Utilities: Fuel (natural gas) (cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr) 6425.9 \$11,618,42 Electricity = \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr 127.0 \$48,12 Nitrogen for carrier \$/1000 scf * scfm carrier gas *60 min/hr*8760 hr/yr 20000.0 \$17,082,00 Water = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 76 \$106,55 Wastewater = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 76 \$131,69 Caustic = b/hr caustic * \$/ b*8760 55 \$149,35 Indirect Annual Costs (IC) Total DC = \$29,168,17 Overhead = 60% of the Sum of Total Labor + Materials \$32,029 \$19,21 Administrative = 2% of Total Capital Investment \$50,25 Property Tax = 1% of Total Capital Investment \$25,12 Insurance = 1% of Total Capital Investment \$25,12 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$255,91			0.2	\$6,570
Parts Cost N/A S Utilities: Fuel (natural gas) (cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr) 6425.9 \$11,618,42 Electricity = \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr 127.0 \$48,12 Nitrogen for carrier \$/1000 scf * scfm carrier gas *60 min/hr*8760 hr/yr 20000.0 \$17,082,00 Water = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 76 \$106,55 Wastewater = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 76 \$131,69 Caustic = b/hr caustic * \$/lb*8760 55 \$149,35 Indirect Annual Costs (IC) Total DC = \$29,168,17 Overhead = 60% of the Sum of Total Labor + Materials \$32,029 \$19,21 Administrative = 2% of Total Capital Investment \$50,25 Property Tax = 1% of Total Capital Investment \$25,12 Insurance = 1% of Total Capital Investment \$25,12 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$255,91	Maintenance Materials	= 100% of Maintenance Labor		\$6,570
Utilities: Fuel (natural gas) (cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr) 6425.9 \$11,618,42 Electricity = \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr 127.0 \$48,12 Nitrogen for carrier \$/1000 scf * scfm carrier gas *60 min/hr*8760 hr/yr 20000.0 \$17,082,00 Water = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 76 \$106,55 Wastewater = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 76 \$131,69 Caustic = b/hr caustic * \$/ b*8760 55 \$149,35 Indirect Annual Costs (IC) = 60% of the Sum of Total Labor + Materials \$32,029 \$19,21 Administrative = 2% of Total Capital Investment \$50,25 Property Tax = 1% of Total Capital Investment \$25,12 Insurance = 1% of Total Capital Investment \$25,12 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$255,91	Replacement Labor	N/A		\$0
Fuel (natural gas)	Parts Cost	N/A		\$0
Electricity				
Nitrogen for carrier				\$11,618,422
Water = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 76 \$106,55 Wastewater = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 76 \$131,69 Caustic = b/hr caustic * \$/ b*8760 55 \$149,35 Total DC = \$29,168,17 Indirect Annual Costs (IC) Overhead = 60% of the Sum of Total Labor + Materials \$32,029 \$19,21 Administrative = 2% of Total Capital Investment \$50,25 Property Tax = 1% of Total Capital Investment \$25,12 Insurance = 1% of Total Capital Investment \$25,12 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$255,91			-	\$48,125
Wastewater = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr 76 \$131,69 Caustic = b/hr caustic * \$/ b*8760 55 \$149,35 Total DC = \$29,168,17 Indirect Annual Costs (IC) Overhead = 60% of the Sum of Total Labor + Materials \$32,029 \$19,21 Administrative = 2% of Total Capital Investment \$50,25 Property Tax = 1% of Total Capital Investment \$25,12 Insurance = 1% of Total Capital Investment \$25,12 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$255,91				\$17,082,000
Caustic * \$/lb*8760 55 \$149,35 Indirect Annual Costs (IC) Overhead = 60% of the Sum of Total Labor + Materials \$32,029 \$19,21 Administrative = 2% of Total Capital Investment \$50,25 Property Tax = 1% of Total Capital Investment \$25,12 Insurance = 1% of Total Capital Investment \$25,12 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$255,91				\$106,551
Total DC = \$29,168,17 Indirect Annual Costs (IC)				\$131,692
Indirect Annual Costs (IC) Overhead = 60% of the Sum of Total Labor + Materials \$32,029 \$19,21 Administrative = 2% of Total Capital Investment \$50,25 Property Tax = 1% of Total Capital Investment \$25,12 Insurance = 1% of Total Capital Investment \$25,12 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$255,91	Caustic	=ID/nr caustic * \$/Ib*8760		\$149,358 \$20,469,477
Overhead = 60% of the Sum of Total Labor + Materials \$32,029 \$19,21 Administrative = 2% of Total Capital Investment \$50,25 Property Tax = 1% of Total Capital Investment \$25,12 Insurance = 1% of Total Capital Investment \$25,12 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$255,91	Indirect Appuel Costs (IC)		Total DC =	\$29,168,177
Administrative = 2% of Total Capital Investment \$50,25 Property Tax = 1% of Total Capital Investment \$25,12 Insurance = 1% of Total Capital Investment \$25,12 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$255,91		- 60% of the Sum of Total Labor + Materials	¢32 U20	¢10 217
Property Tax= 1% of Total Capital Investment\$25,12Insurance= 1% of Total Capital Investment\$25,12Capital Recovery(Based on 8% & 20 year life: Factor = 0.10185)\$255,91			ψ32,029	· ·
Insurance = 1% of Total Capital Investment \$25,12 Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$255,91				
Capital Recovery (Based on 8% & 20 year life: Factor = 0.10185) \$255,91				
			0185)	
$I \text{ otal } IC = II \qquad \$3/5.64$		(2000 0 0.0 d 20) odi iiio. 1 doloi = 0.1	Total IC =	\$375,644
TOTAL ANNUAL OPERATING COSTS = \$29,543,821		TOTAL ANNUAL OPERATING COSTS =		· · · · · · · · · · · · · · · · · · ·

HPA EXISTING CATALYTIC THERMAL OXIDIZER

Direct Costs		
Existing Unit - No construction necessary including bromine scrubber		
Thermal Oxidizer (User Input Cost: Vendor Info and QAQPS USEPA Factor)	\$ -	
Ancillary Equipment	\$0	N/A
	Sum = "A" =	\$0
Instrumentation (0.10 * A)	\$0	
Sales Taxes (0.03 * A)	\$0	
Freight (0.05 * A)	\$0	
Purchased Equipment Cost = "B" =		\$0
Direst Installation Costs		
Foundation and Supports (0.08 * B)	\$0	
Handling and Errection (0.14 * B)	\$0 \$0	
Electrical (0.04 * B)	\$0 \$0	
Piping, Ductwork, and Installation (0.02 *B)	\$0 \$0	
Insulation for Ductwork (0.01 * B)		
	\$0 \$0	
Painting (0.01 * B)	\$0	C O
Direct Installation Cost =	II 00	\$0
Site Preparation (User Inputs Actual Cost)	\$0	
Facilities and Buildings (User Inputs Actual Cost)	\$0	40
Total Direct Cost =	1.	\$0
Indirect Cost (Installation)		
Engineering (0.10 * B)	\$0	
Construction and Field Expenses (0.05 *B)	\$0	
Contractor Fees (0.10 *B)	\$0	
Start-Up (0.02 *B)	\$0	
Performance Test (0.01 *B)	\$0	
Contingencies (0.03 * B)	\$0	
Total Indirect Cost =		\$0
TOTAL CAPITAL INVESTMENT =	41-	\$0
Direct Annual Costs (DC)		
Operating Labor (Basis of Calculations)		
Operator = (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$16,425
Supervisor = (15% of Operator Cost)	0.0	\$2,464
Operating Materials (If Any)		\$0
Maintenance Labor = (hr/shift * shifts/day * days/yr * \$/hr)	0.2	\$6,570
Maintenance Materials = 100% of Maintenance Labor	0.2	\$6,570
Replacement Labor N/A		\$6,570 \$0
	20	
ll ,	20	\$8,500
Utilities:	400.4	COE 4 COO
Fuel (natural gas) (cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	196.1	\$354,522
Electricity = $\frac{\text{kWhr}^{\text{h}} \text{p}^{\text{*}} 1 \text{ kWhr}}{1.341 \text{ hp}^{\text{*}} 8760 \text{ hr}}$	15.0	\$5,683
Wastewater = \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr	15	\$26,017
Sodium Formate =lb/hr * \$/lb * 8760 hr/yr	15.0	\$40,734
	Total DC =	\$467,486
Indirect Annual Costs (IC)		
Overhead = 60% of the Sum of Total Labor + Materials	\$32,029	
Administrative = 2% of Total Capital Investment		\$0
Property Tax = 1% of Total Capital Investment		\$0
Insurance = 1% of Total Capital Investment		\$0
Capital Recovery (Based on 8% & 20 year life: Factor = 0.1	0185)	\$0
	Total IC =	\$19,217
TOTAL ANNUAL OPERATING COSTS =		\$486,703

HPA REGENERATIVE THERMAL OXIDIZER/BROMINE SCRUBBER BASIS: Vendor Quotations, OAQPS Cost Manual (Sixth Edition)

COST ITEM		COST	TOTALS
Direct Costs			
Purchased Equipment Costs			
	st: Vendor Info and QAQPS USEPA Factor)	2,101,175	
Ancillary Equipment		\$315,176	N/A
Bromine Scrubber		\$350,000	
Ancillary Equipment		\$52,500	
		Sum = "A" =	2,818,852
Instrumentation (0.10 * A)		\$281,885	
Sales Taxes (0.03 * A)		\$84,566	
Freight (0.05 * A)		\$140,943	
	Purchased Equipment Cost = "B" =	=	\$3,326,245
Direst Installation Costs			
Foundation and Supports (0.08 * B)		\$266,100	
Handling and Errection (0.14 * B)		\$465,674	
Electrical (0.04 * B)		\$133,050	
Piping, Ductwork, and Installation (0	.02 *B)	\$66,525	
Insulation for Ductwork (0.01 * B)		\$33,262	
Painting (0.01 * B)		\$33,262	
	Direct Installation Cost =		\$997,874
Site Preparation (User Inputs Actua		\$150,000	
Facilities and Buildings (User Inputs		\$25,000	
	Total Direct Cost =		\$4,499,119
Indirect Cost (Installation)			
Engineering (0.10 * B)		\$332,625	
Construction and Field Expenses (0.	05 *B)	\$166,312	
Contractor Fees (0.10 *B)		\$332,625	
Start-Up (0.02 *B)		\$66,525	
Performance Test (0.01 *B)		\$33,262	
Contingencies (0.03 * B)		\$99,787	
	Total Indirect Cost =		\$1,031,136
	TOTAL CAPITAL INVESTMENT =		\$5,530,255
Direct Annual Costs (DC)			
Operating Labor	(Basis of Calculations)		
Operator	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$16,425
Supervisor	= (15% of Operator Cost)		\$2,464
Operating Materials	(If Any)		\$0
Maintenance Labor	= (hr/shift * shifts/day * days/yr * \$/hr)	0.2	\$6,570
Maintenance Materials	= 100% of Maintenance Labor		\$6,570
Replacement Labor	N/A		\$0
Parts Cost	N/A		\$0
Utilities:			
Fuel (natural gas)	(cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr)	642.6	\$1,161,842
Electricity	= \$/kWhr* <mark>kWhr</mark> *8760 hr/yr	395.0	\$200,692
Nitrogen for carrier	\$/1000 scf * scfm carrier gas *60 min/hr*8760 hr/yr	20000.0	\$17,082,000
Water	= \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr	76	\$106,551
Wastewater	= \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr	76 	\$131,692
Caustic	=lb/hr caustic * \$/lb*8760	55	\$149,358
Media Replacement	= CF media * \$50/CF / 3 years	10000.0	\$166,667
		Total DC =	\$19,030,830
Indirect Annual Costs (IC)	000/ (4) 0 (7)	*	A
Overhead	= 60% of the Sum of Total Labor + Materials	\$32,029	\$19,217
Administrative	= 2% of Total Capital Investment		\$110,605
Property Tax	= 1% of Total Capital Investment		\$55,303
Insurance	= 1% of Total Capital Investment		\$55,303
Capital Recovery	(Based on 8% & 20 year life: Factor = 0.1		\$418,691
	TOTAL ANNUAL OPERATOR OF THE	Total IC =	\$659,119
	TOTAL ANNUAL OPERATING COSTS =		\$19,689,949

HPA RECUPERATIVE THERMAL OXIDIZER

BASIS: Vendor Quotations, OAQPS Cost Manual (Sixth Edition)

COST ITEM		COST	TOTALS
Direct Costs			
Purchased Equipment Costs:	tt. \/	#4.005.000	
	st: Vendor Info and QAQPS USEPA Factor)	\$1,095,000	NI/A
Ancillary Equipment Bromine Scrubber		\$164,250 \$350,000	N/A
Ancillary Equipment		\$50,000 \$52,500	
Anciliary Equipment		Sum = "A" =	\$1,661,750
Instrumentation (0.10 * A)		\$166,175	φ1,001,730
Sales Taxes (0.03 * A)		\$49,853	
Freight (0.05 * A)		\$83,088	
,	Purchased Equipment Cost = "B" =		\$1,960,865
Direst Installation Costs			
Foundation and Supports (0.08 * B)		\$156,869	
Handling and Errection (0.14 * B)		\$274,521	
Electrical (0.04 * B)		\$78,435	
Piping, Ductwork, and Installation (0	.02 *B)	\$39,217	
Insulation for Ductwork (0.01 * B)		\$19,609	
Painting (0.01 * B)		\$19,609	4
8: 5 : 41 1	Direct Installation Cost =		\$588,260
Site Preparation (User Inputs Actua		\$150,000	
Facilities and Buildings (User Inputs	Total Direct Cost =	\$25,000	¢2 724 125
Indiana Cont (Inotallation)	Total Direct Cost =		\$2,724,125
Indirect Cost (Installation) Engineering (0.10 * B)		\$406.007	
Construction and Field Expenses (0.	05 *B\	\$196,087 \$98,043	
Contractor Fees (0.10 *B)	03-Б)	\$196,087	
Start-Up (0.02 *B)		\$39,217	
Performance Test (0.01 *B)		\$19,609	
Contingencies (0.03 * B)		\$58,826	
3 ,	Total Indirect Cost =	, , , , ,	\$607,868
	TOTAL CAPITAL INVESTMENT =		\$3,331,993
Direct Annual Costs (DC)			
Operating Labor	(Basis of Calculations)		
Operator	= (hr/shift * shifts/day * days/yr * \$/hr)	0.5	\$16,425
Supervisor	= (15% of Operator Cost)		\$2,464
Operating Materials	(If Any)		\$0
Maintenance Labor	= (hr/shift * shifts/day * days/yr * \$/hr)	0.2	\$6,570
Maintenance Materials	= 100% of Maintenance Labor		\$6,570
Replacement Labor	N/A		\$0
Parts Cost	N/A		\$0
Utilities:	(cfm/1000 * \$/1000 cf * 50 min/hr *9750 hr//m)	3212.9	¢5 000 244
Fuel (natural gas) Electricity	(cfm/1000 * \$/1000 cf * 60 min/hr *8760 hr/yr) = \$/kWhr*hp*1 kWhr/1.341 hp*8760 hr/yr	3212.9	\$5,809,211 \$114,297
Nitrogen for carrier	= \$/kvviii fip 1 kvviii/1.341 fip 6/60 fil/yi \$/1000 scf * scfm carrier gas *60 min/hr*8760 hr/yr	20000.0	\$17,082,000
Water	= \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr	76	\$106,551
Wastewater	= \$/1,000 gal * gal/min/1000 * 60 min/hr * 8760 hr/yr	76 76	\$131,692
Caustic	=lb/hr caustic * \$/lb*8760	55	\$149,358
		Total DC =	\$23,425,138
Indirect Annual Costs (IC)			
Overhead	= 60% of the Sum of Total Labor + Materials	\$32,029	
Administrative	= 2% of Total Capital Investment	\$32,029	\$66,640
Administrative Property Tax	= 2% of Total Capital Investment= 1% of Total Capital Investment	\$32,029	\$66,640 \$33,320
Administrative Property Tax Insurance	= 2% of Total Capital Investment= 1% of Total Capital Investment= 1% of Total Capital Investment		\$66,640 \$33,320 \$33,320
Administrative Property Tax	= 2% of Total Capital Investment= 1% of Total Capital Investment	0185)	\$66,640 \$33,320 \$33,320 \$258,367
Administrative Property Tax Insurance	= 2% of Total Capital Investment = 1% of Total Capital Investment = 1% of Total Capital Investment (Based on 8% & 20 year life: Factor = 0.1		\$19,217 \$66,640 \$33,320 \$33,320 \$258,367 \$410,864
Administrative Property Tax Insurance	= 2% of Total Capital Investment= 1% of Total Capital Investment= 1% of Total Capital Investment	0185)	\$66,640 \$33,320 \$33,320 \$258,367

\$/1000 scf * scfm carrier gas *60 min/hr*8760 hr/yr

Non-confidential April 2013, Revised March 2014

\$17,082,000

20,000

Nitrogen for carrier

Appendix E Title V Permit Mark-up

The Title V permit mark-up that follows has the requested changes for this PSD application highlighted in yellow. Any changes not highlighted in yellow were included in the Title V renewal application previously submitted but do not have to be implemented for this application.



Part 70 Air Quality Permit

BP Amoco Chemical Company-Cooper River Plant 1306 Amoco Drive Wando, South Carolina 29492-7879

(Permit Updated 12/17/09)

In accordance with the provisions of the Pollution Control Act, Sections 48-1-50(5) and 48-1-110(a), and the 1976 Code of Laws of South Carolina, as amended, Regulation 61-62, the above named permittee is hereby granted permission to discharge air contaminants into the ambient air. The Bureau of Air Quality authorizes the operation of this facility and its applicable equipment specified herein in accordance with the plans, specifications and other information submitted in the Title V permit application dated December 17, 2003.

This permit is subject to and conditioned upon the terms, limitations, standards, and schedules contained in or specified on the 69 pages, with the accompanying attachments, of this permit.

Permit Number: TV-0420-0029 Effective Date: October 1, 2007 Issue Date: June 26, 2007 Expiration Date: September 30, 2012

> Director, Engineering Services Division Bureau of Air Quality

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PART 1.0 GENERAL INFORMATION

A. APPLICABLE PERMIT DATES

ISSUE DATE : June 26, 2007 EFFECTIVE DATE : October 1, 2007 EXPIRATION DATE : September 30, 2012

RENEWAL APPLICATION DUE : March 31, 2012

B. FACILITY INFORMATION

FEDERAL TAX IDENTIFICATION NO. : 36-2347240

ENVIRONMENTAL CONTACT : Brent A. Pace

CONTACT TELEPHONE NUMBER : (843) 881-5182

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FACILITY LOCATION : Highway 98 & Clements Ferry Road

 COUNTY
 : Berkeley

 SIC CODE(S)
 : 2869

 NAICS CODE(S)
 : 325199

 AFS CODE
 : 4501500029

C. FACILITY ADDRESS

FACILITY NAME : BP Amoco Chemical Company-Cooper River Site

ADDRESS : 1306 Amoco Drive

CITY, STATE, ZIP : Wando, South Carolina 29492-7879

D. FACILITY BILLING ADDRESS

FACILITY BILLING NAME : BP Amoco Chemical Company-Cooper River Site

ADDRESS : 1306 Amoco Drive

CITY, STATE, ZIP : Wando, South Carolina 29492-7879

PART 5.0 EMISSION UNIT REQUIREMENTS

A. EMISSION UNIT DESCRIPTION

Table 5.1 is a description of emission units located at this facility.

TABLE 5.1 EMISSION UNITS				
Unit ID	Unit Description	Control Device Description		
01	Boiler #1 (242 Million Btu/hr) – VOID-	Dust Collection Hopper (Voluntary Control Device) - VOID		
02	Boiler #2 (242 Million Btu/hr) – VOID-	Dust Collection Hopper (Voluntary Control Device) - VOID		
03	Cooper River #1: Oxidation Unit	Scrubbers, Catalytic Oxidizer, Condenser		
04	Cooper River # 1: PTA Unit	Baghouse, Scubbers, Spray Nozzle		
05	Cooper River #2: Oxidation Unit	Scrubbers, Catalytic Oxidizer, Condenser		
06	Cooper River #2: PTA Unit	Baghouses, Scrubbers, Condenser		
07	Shipping/Loading	Baghouses		
08	Cooper River #1: Ox Four Compressors –VOID-	Low sulfur fuels –VOID-		
09	Cooper River#2: Ox Emergency Generator (see Unit ID 11 below)	See Unit ID 11 below		
10	CR#2 Utility Compressor #2 (see Unit ID 11 below)	See Unit ID 11 below		
11	Utilities Generators, Compressors, and Pumps	N/A		
12	Tank Farm	Internal Floating Roofs		
13	Wastewater Treatment	Boilers (for biogas)		
14	Waste Treatment Compressors	See Unit ID 11 above		
15	Boiler #3 (Boiler AB-350A (390 Million Btu/hr))	Low Nox NOx Burners		
16	Boiler #4 (Boiler AB-350B (390 Million Btu/hr))	Low Nox NOx Burners		

N/A = Not Applicable

B. CONTROL DEVICE DESCRIPTION

Table 5.2 is a description of control devices located at this facility.

	TABLE 5.2 CONTROL DEVICES				
Control Device ID	<u>Unit</u> <u>ID</u>	Control Device Description	Installation Date	Pollutant(s) Controlled	
301A (DC)	(Unit ID-01)	Dust Collection Hopper, Boiler #1(Voluntary Control Device) – VOID-	1977	Particulates	
301B (DC)	(Unit ID-02)	Dust Collection Hopper, Boiler #2 (Voluntary Control Device) -VOID-	1977	Particulates	
CR#1- HPVGT	(Unit ID-03)	High Pressure Vent Gas Treatment System (#1 Oxidation) (Consists of catalytic oxidizer and a scrubber)	1999	VOC, CO	

TABLE 5.2 CONTROL DEVICES				
Control Device ID	<u>Unit</u> <u>ID</u>	Control Device Description	Installation Date	Pollutant(s) Controlled
BT-603	(Unit ID-03)	Atmospheric Absorber	1977 2004 (Revision)	VOC
BM-504A	(Unit ID-03)	Bag Filters; Intermediate Storage –VOID-	1977	Particulates
BM-504B	(Unit ID-03)	Bag Filters; Intermediate Storage –VOID-	1977	Particulates
BT-501	(Unit ID-03)	Scrubber: Intermediate Storage	2002	Particulates
BH-522	(Unit ID-03)	Dry Cyclone Scrubber; Rotary Lock – VOID -	1983	Particulates
BE-645	(Unit ID-03)	Condenser (Recovery Device)	1977	VOC
CM-301	(Unit ID-04)	Venturi Scrubber; Crystallizer Vent Scrubber	1977	Particulates
CM-603A	(Unit ID-04)	Bag Filter; Day Silo	1977	Particulates
CM-603B	(Unit ID-04)	Bag Filter; Day Silo	1977	Particulates
CM-607A	(Unit ID-04)	Dust Collectors /Rotary Lock –VOID-	1991	Particulates
CM-607B	(Unit ID- 04)	Dust Collectors/Rotary Lock-VOID-	1991	Particulates
CM-608A	(Unit ID- 04)	Dust Collectors /Screener	1991	Particulates
CM-608B	(Unit ID- 04)	Dust Collectors; Screener	1991	Particulates
CR#2- HPVGT	(Unit ID-05)	High Pressure Vent Gas Treatment System DR- 1814/DT-1821 (Consists of catalytic oxidizer and a scrubber)	1996	HAP's, VOC, CO
DT-302	(Unit ID-05)	Atmospheric Absorber	1996	VOC
DT-500	(Unit ID-04)	Venturi Scrubber and Spray Tower; Ox Feed Silos	1996	Particulates
DE-416	(Unit ID-05)	Evaporator Overhead Condenser	1996	VOC
DM- 601/DE-601	(Unit ID-06)	Venturi Scrubber and Spray Tower Crystallizer Vent Scrubber	1996	Particulates
DE-317	(Unit ID-06)	Mother Liquor Cooler Ejector Condenser	1996	VOC
DM-797A	(Unit ID-06)	Day Silo Dust Collector	1996	Particulates
DM-797B	(Unit ID-06)	Day Silo Dust Collector	1996	Particulates
CM-701A	(Unit ID-07)	Storage Silo Bag Filter	1977	Particulates
CM-701B	(Unit ID-07)	Storage Silo Bag Filter	1977	Particulates

TABLE 5.2 CONTROL DEVICES				
Control Device ID	Control Device Description		Installation Date	Pollutant(s) Controlled
CM-701C	(Unit ID-07)	Storage Silo Bag Filter	1977	Particulates
CM-701D	(Unit ID- 07)	Storage Silo Bag Filter	1977	Particulates
CM-701E	(Unit ID- 07)	Storage Silo Bag Filter	1977	Particulates
CM-720A (F Silo)	(Unit ID- 07)	Storage Silo Bag Filter	1996	Particulates
CM-720B (F Silo)	(Unit ID- 07)	Storage Silo Bag Filter	1996	Particulates
CM-722	(Unit ID- 07)	Bulk Truck Loading Bag Filter	1996	Particulates
CM-705A	(Unit ID- 07)	Loading Spout Dust Collector	1977	Particulates
CM-705B	(Unit ID- 07)	Loading Spout Dust Collector	1977	Particulates
CM-705C	(Unit ID- 07)	Loading Spout Dust Collector	1977	Particulates

C. EQUIPMENT DESCRIPTION

A description of the equipment located at this facility is provided in the following tables:

TABLE 5.3 UNIT ID 03 – Cooper River #1 Oxidation Unit					
Equip ID	Equipment Description	Installation Date	Control Device ID	Stack ID	
BR 301 A-D BR-301	Reactors	5/3/77 2014	High Pressure Absorber (Recovery Device; BT 401) then to CR#1-HPVGT	O-2/10/15	
BD- 401 /402	Crystallizers	5/3/77	High Pressure Absorber (Recovery Device; BT 401) then to CR#1-HPVGT	O-2/10/15	
BD- 402/403	<u>Crystallizer</u>	5/3/77	BT 601(Dryer Scrubber) then to BT-603 (Low Ppressure aAbsorber)	<mark>O-3</mark>	
BD-202	Solvent Charge	Modified 5/3/95	BT-603	O-3	
BD-204	Feed Mix Drum	Modified 5/3/95	BT-603	O-3	
BD-503	Filter Vacuum Pump Separator	Modified 5/3/95	BT-603	O-3	
BD-602	Mother Liquor Drum	Modified 5/3/95	BT-603	O-3	
BD-705	Dehydrated Solvent Drum (Bottom Receiver)	Modified 5/3/95	BT-603	O-3	
BD-501	Filter	Modified 5/3/95	BT-603	O-3	
BF-1401	Acetic Acid Tank	1977	BT-603	O-3	

TABLE 5.3 UNIT ID 03 – Cooper River #1 Oxidation Unit					
Equip ID	Equipment Description	Installation Date	Control Device ID	Stack ID	
BM-502	Ox Product Dryer	5/3/77	BT-603	O-3	
BT- 701/ BE- 7 06	Dehydration Tower	Modified 5/3/95 and 2004 <u>& 2011</u> <u>&2014</u>	DHT Scrubber (HON Recovery Device & Control) Control Device ID (BT 702) BT-603 (HON Recovery Device)	0-23 <u>0-3</u>	
BT - 701/BE- 706	Dehydration Tower	Modified 5/3/95 and 2004	CR#1 HPVGTS	O-2/10/15	
BF-501A	Intermediate Storage Silo -VOID-	5/23/77	BM-504A-VOID	O-7	
BF-501B	Intermediate Storage Silo -VOID-	5/23/77	BM-504B <u>-VOID</u>	O-8	
BF-501A	Intermediate Storage Silo	2002	BT-501	O-22	
BF-501B	Intermediate Storage Silo	2002	BT-501	O-22	
BM <u>-</u> 1101 A/B	Off Gas Dryer (Emission Point for BT-401)	Modified 5/3/95	None	O-10	
BD-625	CRU Extraction Drum	<mark>8/7/80</mark>	None	O-11	
BD-631	CRU Mother Liquor Drum	8/7/80	None	O-12	
BD-632	CRU Waste Solids Reslurry Drum	<mark>1983</mark>	None	O-13	
BH-523	Dryer Rotary Lock Venting System (Fluidizer) -VOID-	1983	BH-522(VOID)	O-14	
BM- 1101C/D	Off Gas Dryer (Emission Point for B-401)	2/1/85	None	O-15	
BD 640	CRU Evaporator	8/7/80	BE 645	O-16	
BM-1201	Emergency Generator #2	5/23/77	None	O-17	

The CR#1 Dehydration Tower is a HON Group 2 stream, with a TRE between 1 and 4, after the <u>DHT ScrubberLow Pressure Absorber</u> (HON Recovery Device). The DHT Scrubber outlet will normally go via the LPVGT system to the CR#1 HPVGTS. However, the DHT Scrubber can vent to the atmosphere (Vent O 23) per the emission limitations from construction permit 0420-0029-CR.

TABLE 5.4 UNIT ID 04 – Cooper River #1:PTA Unit					
Equip ID	Equipment Description	Installation Date	Control Device ID	Stack ID	
CD-101/ CH-108	Feed Slurry Drum and Eductor	5/23/77	None	P-1	
CD-413	Reslurry Solvent Drum	Modified 5/3/95	BT-603	O-3	
CD-411	Mother Liquor Solids Reslurry Drum	Modified 5/3/95	BT-603	O-3	
CD-301-303, CD-305	Crystallizers	5/23/77	CM-301	P-2	
<u>CM-402A/B</u>	<u>Filters</u>	<u>2011</u>	<u>N/A</u>	<u>N/A</u>	
CM-403A	Product Dryer and Vacuum System	5/23/77	None	P-3A	
CM-403B	Product Dryer and Vacuum System	5/23/77	None	P-3B	
CD-404A	Atmospheric Mother Liquor Flash Drum	5/23/77 Modified in 2005	CM-301	P-2	
CR-202	Reactor	5/23/77	CM-301	P-2	
CF-601A	Day Silo	5/23/77	CM-603A	P-4A	
CF-601B	Day Silo	5/23/77	CM-603B	P-5BP-4B	
CD-405	Filter Feed Drum and CH-418 Maintenance Spray	5/23/77	None	P-14	

TABLE 5.4 UNIT ID 04 - Cooper River #1:PTA Unit						
Equip ID	Equipment Description	Installation Date	Control Device ID	Stack ID		
CM-609A	Product Screener A	1991	CM-608A	P-17		
CM-609B	Product Screener B	1991	CM-608B	P-18		
CH-430	Vacuum Ejector	8/7/80	None	P-19		
CH-431	Hogger Vacuum Ejector	8/7/80	None	P-19		
CD-412	Filtrate	8/7/80	None	P-19		

	TABLE 5.5 UNIT ID 05 – Cooper River #2 Oxidation Unit					
Equip ID	Equipment Description	Installation Date	Control Device ID	Stack ID		
O2 1 DM-302	Product Dryer	6/22/95	DT-302	O2-1		
DD-303	TA Filter Feed Drum-Vacuum Pump KO Drum	6/22/95	DT-302	O2-1		
DD-306	Mother Liquor Drum	6/22/95	DT-302	O2-1		
DD-405	Dehydrated Solvent Drum	6/22/95	DT-302	O2-1		
DD- <u>202/</u> 203	Crystallizer <u>s</u> Condenser	6/22/95	DT-302	O2-1		
DD-307	Slurry Surge Drum	6/22/95	DT-302	O2-1		
DD-103	Catalyst Charge Drum	6/22/95	DT-302	O2-1		
DE-110	Feed Mix Drum Vent Condenser	6/22/95	DT-302	O2-1		
DE-204	Crystallizer Overhead Ejector Condenser	6/22/95	DT-302	O2-1		
DD-305	Filter Cake Reslurry Drum	6/22/95	DT-302	O2-1		
DT-111	High Pressure Absorber**	6/22/95	CR#2-HPVGT	O2-3/4		
DB-1813	HPVGT Fired Heater	6/22/95	None	O2-2		
DT-403	Dehydration Tower	6/22/95 2014	CR#2 HPVGT DT- 302 (HON Recovery Device)	O2-3/4 <u>O2-1</u>		
DR-106 A/B	Reactors	6/22/95	CR#2-HPVGT	O2-3/4		
DD <u>-</u> 201	1 st Crystallizer	6/22/95	CR#2-HPVGT	O2-3/4		
DF- 500A/B	OX Feed Silos to PTA	6/22/95	DT-500	O2-5		
DD-412	CRU Extraction Drum	<mark>6/22/95</mark>	None	O2-6		
DD-413	CRU Waste Slurry Drum	<mark>6/22/95</mark>	None	O2-7		
DD-414	CRU Mother Liquor Drum	6/22/95	None None	O2-8		
DE-390	CRU Evaporation Drum	6/22/95	DE-416	O2-9		

**The CR#2 Dehydration tower is subject to the requirements of Sub part G of part 40 CFR 63. BP has elected to comply with Subpart G by first routing the dehydration Tower emissions through the HPA (recovery device) to the CR#2-HPVGTS, which is a HON Group 1 control device.

TABLE 5.6 UNIT ID 06 – Cooper River #2 PTA Unit						
Equip ID	Control Device ID	Stack ID				
DD-500/ DH-518	Feed Slurry Drum and Eductor	6/22/95	None	P2-1		
DD-601-605	Crystallizers	6/22/95	DM-601/DE-601	P2-2		
DD-705	Filter Feed Drum	6/22/95	DM-601/DE-601	P2-2		
DD-704	PRU Mother Liquor Flash Drum	6/22/95	DM-601/DE-601	P2-2		
DM-702A/B	<u>Filters</u>	<u>2011</u>	<u>N/A</u>	<u>N/A</u>		

TABLE 5.6 UNIT ID 06 – Cooper River #2 PTA Unit						
Equip ID	Equipment Description	Installation Date	Control Device ID	Stack ID		
DM-703/ DM-704	Product Dryers and Vacuum System	6/22/95	None	P2-3		
DF-703A	Day Silo	6/22/95	DM-797A	P2-4A		
DF-703B	Day Silo	6/22/95	DM-797B	P2-4B		
DM-798A	Product Screener	6/22/95	DD 799/ DM-797A	P2-4A		
DM-798B	Product Screener	6/22/95	DD 799 /DM-797B	P2-4B		
DD-304	PRU Mother Liquor Cooler	6/22/95	DE-317	P2-9		
DD-308	PRU Mother Liquor Drum	6/22/95	None	P2-10		
DR-500	Reactor	6/22/95	DM-601/DE-601	P2-2		

	TABLE 5.7 UNIT ID 07 – Shipping/Loading						
Equip ID	Equipment Description	Installation Date	Control Device ID	Stack ID			
CP-701A-E	Product Loading Spout	5/03/77	CM-705A	SL-7			
CP-701A-E	Product Loading Spout	5/03/77	CM-705B	SL-8			
CP-701A-E	Product Loading Spout	5/03/77	CM-705C	SL-9			
CF-701A	Shipping Storage Silo A	5/23/77	CM-701A	SL-1			
CF-701B	Shipping Storage Silo B	5/23/77	CM-701B	SL-2			
CF-701C	Shipping Storage Silo C	5/23/77	CM-701C	SL-3			
CF-701D	Shipping Storage Silo D	5/23/77	CM-701D	SL-4			
CF-701E	Shipping Storage Silo E	5/23/77	CM-701E	SL-5			
CF-677 Intermediate Transfer Tank – VOID-		6/22/95	CM-677	SL-11			
CF-701F	Shipping Storage Silo F	6/22/95	CM-720A	SL-6A			
CF-701F	Shipping Storage Silo F	6/22/95	CM-720B	SL-6B			
CP-701F/ 709F	Bulk Truck Loading	6/22/95	CM-722	SL-10			

	TABLE 5.8 UNIT ID 11 – Utilities Generator, Compressor and Pumps					
Equip ID	Equipment Description	Installation Date	Control Device ID	Stack ID		
AM-804	Emergency Generator #1 (275 kW/0.136 Million Btu/hr)			5/03/77 1/1/79 None		U-3
AC-402	Emergency Compressor #1 (0.1361.53 Million Btu/hr)	5/03/77	None	U-4		
AG-202 <u>B</u>	Emergency Fire Water Pump (200.76) Million Btu/hr)	5/03/77 <u>.</u> replaced 3/04	None	U-5		
AC-404	Compressor #2 (8.2 Million Btu/hr)	1997	None	U-6		
AG-229	T-Head FW Pump (4 .0 Million Btu/hr 224 BHP)	5/03/77	None	U-7		
AM-838	IT Emergency Generator (5.5 Million Btu/hr)	2002	None	U-8		
AG-202C	Emergency Fire Water Pump	200 <u>5</u> 3	None	U-9		
AG-202D	Emergency Fire Water Pump	200 <u>5</u> 3	None	U-10		
BM-1201	Emergency Generator #2	5/03/77 <u>1/1/79</u>	None	U-11 <u>O-17</u>		
DM-135	Emergency Generator #3 (max 800 kW)	1997 <u>12/11/95</u>	None	U 12<u>O2-</u> <u>10</u>		
L-1	(Leased) Compressor #1*	1998<u>N/A</u>	None	U-13		
L-2	(Leased) Compressor #2*	1998<u>N/A</u>	None	U-14		

* Total combined capacity of compressors shall be less than 2350 HP (5.98 Million Btu/hr)

TABLE 5.9 UNIT ID 12 – Tank Farm						
Equip ID	Control Device ID	Stack ID				
AF-101	Px Storage Tank (internal floating roof)	1977 (modified 10/92)	None	TK-1		
AF-102	Px Storage Tank (internal floating roof)	1977 (modified 10/92)	None	TK-2		
AF-103	Px Storage Tank (internal floating roof)	1977 (modified 10/92)	None	TK-6		
	Px Unloading station	1977	None	N/A		

	TABLE 5.10 UNIT ID 13 – Wastewater Treatment					
Equip ID	Equipment Description	Installation Date	Control Device ID	Stack ID		
AT-750	4 Million Gallon per day CO ₂ Stripper	6/22/95	None	WT-10		
AM-775	4 Million Gallon per day Anaerobic Reactor	6/22/95	None	WT-11		
AM-704A	Aerobic Reactor	5/3/77	None	None		
AM-705A	Aerobic Reactor	5/3/77	None	None		
AM-705B	Aerobic Reactor	5/3/77	None	None		
AF-760	Surge Tank	6/22/95	None	None		
AF-206A	88,128 gallon Waste Neutralizing Tank	5/3/77	N/A	None		
AF-206B	88,128 gallon Waste Neutralizing Tank	5/3/77	N/A	None		
AF-206C	88,128 gallon Waste Neutralizing Tank	5/3/77	N/A	None		
AR-751	500, 000 gallon UASB Reactor	2002	None	WT-11		
AR 754	4,000 gallon UASB Seed Storage Tank	2002	None	None		

TABLE 5.11 UNIT ID 15 – 390 Million Btu/hr Boiler #13					
Equip ID Equipment Description Installation Date Control Device ID State					
AB-350A	390 Million Btu/hr Boiler #3	2005	Low Nox <u>NOx</u> Burners	U-11	

	TABLE 5.12 UNIT ID 16 – 390 Million Btu/hr Boiler #2-4					
Equip ID	Equipment Description	Installation Date	Control Device ID	Stack ID		
AB-350B	390 Million Btu/hr Boiler #4	2005	Low Nox <u>NOx</u> Burners	U-12		

TABLE 5.13 UNIT ID Insignificant Activity Generators (IAG)					
Equip ID	Control Device ID	Stack ID			
<u>AM-819</u>	Administration Building Emergency Generator	04/01/05	<u>None</u>	IAG-1	
<u>AM-840</u>	PX Pump Emergency Generator	07/31/06	<u>None</u>	IAG-2	
<u>AM-846</u>	Main Gate Emergency Generator	05/01/05	<u>None</u>	IAG-3	

	TABLE 5.13 UNIT ID Insignificant Activity Generators (IAG)					
Equip ID	Equipment Description	Order Date	Control Device ID	Stack ID		
<u>AM-847</u>	Contractor Gate Emergency Generator	<u>05/01/05</u>	<u>None</u>	IAG-4		
<u>AM-848</u>	T-Head Emergency Generator	<u>05/01/05</u>	<u>None</u>	IAG-5		
<u>AM-849</u>	WWT Control Room Emergency Generator	12/01/07	<u>None</u>	IAG-6		

D. EMISSION LIMITS AND STANDARDS

Table 5.13 contains summaries of emission unit emission limits and standards.

	TABLE 5.13 EMISSION LIMITS AND STANDARDS							
Unit ID	Pollutant/ Standard	Limit	Reference Method	Regulation	State Only	Condition Number		
All	VOCs	See Permit Condition	18	SC Reg. 61-62.5, Std.5 <u>.1</u>	Yes	5.E. 17		
03	CO	1452 lb/hr and 375 TPY	10B	SC Reg. 61-62.5, Section II (H)	No.	5.E.4		
03	VOCs	85 lb/hr and 80 TPY	18	SC Reg. 61-62.5, Section II (H)	No.	<mark>5.E.4</mark>		
03	PM_{10}	2.16 lb/hr	201, 201A	SC Reg. 61-62.5, Section II (H)	No	5.E.4		
03	VOCs	40 lb/hr & 80 TPY	18	SC Reg. 61-62.5, Section II (H)	No.	<mark>5.E.4</mark>		
03	CO	40 TPY	10B	SC Reg. 61-62.5, Section II (H)	No.	<mark>5.E.4</mark>		
03	VOCs	60 lb/hr & 165 TPY	18	SC Reg. 61-62.5, Section II (H)	No.	<mark>5.E.4</mark>		
03	CO	380 TPY	10B	SC Reg. 61-62.5, Section II (H)	No.	<mark>5.E.4</mark>		
03-06	VOCs	1825 TPY	Method 18 or 25A	Letter dated November 2, 1998, Construction Permit 0420-0029-CP & SC Reg. 61-62.1, Section II(H)	No	<u>5.E.5</u>		
03-06	PM (HPVGTS)	0.5 lb/10 ⁶ Btu	<u>5</u>	SC Reg. 61-62.1, Standard No. 3, Section HI(1)	Yes	5.E.6		
03-06	Opacity	20%	<mark>9</mark>	SC Reg. 61-62.1, Standard No. 3, Section HI(1)	Yes	5.E.6		
05	DRE	Less than 20 ppmv HAPs (HON regulation)	18 or 25A	SC Reg. 61-62.1, Sec. H(H)	No	5.E.6		
03- 06, 12-13	HAPs	See Condition	N/A	40 CFR 63, Subparts A, F, G and H	No	5.E.7, 5.E.10, 5.E.12, 5.E.13		
03-04	TRE value	See Condition	Per 40 CFR 63	40 CFR 63.113 (d)	No	5.E.7		

TABLE 5.13 EMISSION LIMITS AND STANDARDS							
Unit ID	Pollutant/ Standard	Limit	Reference Method	Regulation	State Only	Condition Number	
03-04	PM	56.0 lbs/hr	5	SC Regulation 61-62.5, Standard No. 4, Sec. VIII	No	5.E.8	
03-04	Opacity (all)	20%	9	SC Regulation 61-62.5, Standard No. 4, Section IX	No	5.E.8	
05-06	VOC	215.9 tpy and 49.3 lbs/hr	N/A	SC Regulation 61-62.5, Section II (H)	No.	5.E.31	
05-06	PM	53.67 lbs/hr	5	SC Regulation 61-62.5, Standard No. 4, Sec. VIII	No	5.E.9	
05-06	Opacity (all)	20%	9	SC Regulation 61-62.5, Standard No. 4, Section IX	No	5.E.9	
05	TOCs (VOCs)	See Condition	N/A	40 CFR 60 Subparts A and III	No	5.E.10	
05	TOCs (VOCs)	See Condition	N/A	40 CFR 60 Subparts A and NNN	No	5.E.10	
05	HAPs	See Condition	18	40 CFR 63 Subpart G	No	5.E.10	
05	Halogens	See Condition	26	40 CFR 63 Subpart G	No.	5.E.10	
05-06	VOCs	See Condition	N/A	40 CFR 60 Subparts A and VV	No.	5.E.10	
07	PM	56.25 lbs/hr	5	SC Reg 61-62.5, Standard No. 4, Section VIII	No	5.E.11	
07	Opacity	20%	9	SC Reg 61-62.5, Standard No. 4, Section IX	No	5.E.11	
07	PM_{10}	1.08 lb/hr (each for Silos CF-701-A-E)	As approved by BAQ	SC Reg. 61-62.1, Sec. II(H)	No	5.E.11	
07	PM_{10}	0.48 lb/hr (for Silo CF-701F)	As approved by BAQ	SC Reg. 61-62.1, Sec. II(H)	No	5.E.11	
11	Opacity (all)	See Condition	9	SC Reg. 61-62.1, Sec. II(H)	No	5.E.14	
11	PM/PM ₁₀	See Condition	5	SC Reg. 61-62.1, Sec. II(H)	No	5.E.14	
11	SO ₂	See Condition	6	SC Reg. 61-62.1, Sec II(H)	No	5.E.14	
11	NO_x	See Condition	7	SC Reg. 61-62.1, Sec. II(H)	No	5.E.14	
11	СО	See Condition	10	SC Reg. 61-62.1, Sec II(H)	No	5.E.14	
11	VOCs	See Condition	25	SC Reg. 61-62.1, Sec. II(H)	No	5.E.14	
11	Fuel sulfur content	See Condition	N/A	SC Reg. 61-62.1, Sec II(H)	No	5.E.14	
11	Hours of operation	See Condition	N/A	SC Reg. 61-62.1, Sec. II(H) or 40 CFR 63 Subpart ZZZZ	No	5.E.14	

	T	ABLE 5.13 EMIS	SION LIMIT	S AND STANDARDS	<u> </u>	
Unit ID	Pollutant/ Standard	Limit	Reference Method	Regulation	State Only	Condition Number
11	See Condition	See Condition	See Condition	40 CFR 63 Subpart ZZZZ	No	5.E.28
12	Opacity (all)	20%	9	SC Reg. 61-62.5, Std. 4, See IX	No	5.E.15
13	Opacity (all)	20%	9	SC Reg. 61-62.5, Std. 4, Section IX	No	5.E.16
15-16	Opacity	20%	9	40 CFR 60 Subpart Db	No	5.E.20-22
15-16	Opacity	20%	9	SC Reg. 61-62.5, Std.1, Section I	No	5.E.18
15-16	PM	0.6 lbs/10 ⁶ Btu (3 hour average)	5, 5B or 17	SC Reg. 61-62.5, Std.1, Section II	No	5.E.18
15-16	PM/PM ₁₀	50.9 TPY, total for both boilers combined (12- month rolling sum)	5, 5B or 17	SC Regulation 61-62.1, Section II.H	No	5.E.19
05 <u>.</u> 15-16	PMSee Condition	0.03 lb/10 ⁶ Btu of heat input, each (30 day average)See Condition	<u> 5NA</u>	40 CFR 63 Subpart DDDDD	No	5.E.24 -26
15-16	SO_2	3.5 lbs/10 ⁶ Btu	6 or 6C	SC Reg. 61-62.5, Std.1, Section III	No	5.E.18
15-16	SO_2	733.4 TPY, total for both boilers combined (12- month rolling sum)	6 or 6C	SC Regulation 61-62.1, Section II.H	No	5.E.19
15-16	NO _x	0.10 lb/10 ⁶ Btu, each (30-day rolling average)	NOx monitoring system under 40 CFR 60.48b	40 CFR 60.44.b	No	5.E.20, 5.E.23
15-16	NO _x	317.0 TPY, total for both boilers combined (12-month rolling sum)	7 or 7E	SC Regulation 61-62.1, Section II.H	No	5.E.19
15-16	СО	299.6 TPY, total for both boilers combined (12- month rolling sum)	10	SC Regulation 61-62.1, Section II.H	No	5.E.19
15-16	CO	400 ppm by volume on a dry basis corrected to a 3 percent oxygen, each (30 day average)	CO monitoring system under 40 CFR 63 Subpart DDDDD	40 CFR 63 Subpart DDDDD	No	5.E.24-25
15-16	Hydrogen Chloride	0.0005 lb/10 ⁶ Btu of heat input, each	2 6	40 CFR 63 Subpart DDDDD	No.	5.E.24-26
15-16	Used oil	See Condition	N/A	SC Regulation 61 62.1	Yes	<mark>5.E.29</mark>
15-16	NO _x Budget	N/A	N/A	SC Regulation 61- 62.96	No	5.E.27

	TABLE 5.13 EMISSION LIMITS AND STANDARDS							
Unit ID	Pollutant/ Standard	Limit	Reference Method	Regulation	State Only	Condition Number		
03	VOCs	<mark>Voluntary LDAR</mark> Program	N/A	SC Regulation 61-62.1, Section H.H	No.	5.E.30		
<u>IAG</u>	<u>See</u> Condition	See Condition	<u>See</u> <u>Condition</u>	40 CFR 63 Subpart ZZZZ	<u>No</u>	<u>5.E.32</u>		
<u>IAG</u>	<u>See</u> Condition	See Condition	See Condition	40 CFR 60 Subpart IIII	<u>No</u>	<u>5.E.33</u>		

The maximum allowable emission limits above are derived from the various Federal and State regulations that govern the operation of this type of source. All applicable facility wide emission limits and corresponding regulations are listed above. Additional operating requirements which may be more stringent than those above are contained in Part 4.0, Part 6.0, and Part 7.0 of this permit.

E. EMISSION UNIT CONDITIONS

Condition Number	Conditions
	Conditions 5.E.1-5.E.3 Voided
5.E.4	For Cooper River #1, emission limitations were established to avoid a PSD review for the project to debottleneck Cooper River #1 and #2 that was approved in Construction Permit Nos. 0420-0029-CJ, CK and CL. Also for Cooper River #1, emission limitations were updated and added_ to avoid a PSD review for the project to complete an emission reduction project that was approved in Construction Permit No. 0420-0029-CP. The maximum allowable CO emission rate from the #1 HPVGTS is 1452 lb/hr and 375 TPY. The maximum allowable VOC emission rate from the #1 HPVGTS is 85 lb/hr and 80 TPY. The maximum allowable VOC emission rate from the #1 Silo Scrubber is 2.16 lb/hr. The maximum allowable CO emission rate from the BT 603 LPA is 80 TPY and 40 lb/hr. The maximum allowable CO emission rate from the BT 702 DHT Scrubber is 165 TPY and 60 lb/hr.
5.E.5	For Cooper River #1 and #2, a combined emission limitation for VOCs was established to avoid a PSD review at the time of the project approved in 1995 to construct a new purified terephthalic acid (PTA) production process, designated as Cooper River #2. The limit was revised based on PSD review at the time of construction projects in 2000 and 2004. The maximum allowable VOC emission rate is 1825 tons per year; this limit incorporates all VOC limits from previous construction permits.
5.E.6	Emission Unit 03 06 The following shall apply to the HPVGTS on the units: The permittee shall operate the catalytic oxidizers (BR 1814 and DR 1814) in compliance with the requirements of SC Regulation 61 62.5, Standard No. 3. SC Regulation 61 62.5, Standard No. 3 establishes the maximum allowable emissions of PM of 0.5lb/10 ⁶ Btu to be emitted from the catalytic oxidizers and establishes the opacity limitation of 20%. The CR#2 HPVGTS shall be limited to less than 20 ppmv HAPs through its vent, per requirements in the HON. SC Regulation 61 62.1, Section II(H) requires a destruction and removal efficiency (DRE) of 95%; this requirement is satisfied by the HON limit, which is more stringent.

Condition Number	Conditions								
	The following emission points in units 03-04 are subject to 40 CFR 63, Subparts A, F, G and H: Emission Unit ID 03 Cooper River #1: Oxidation Unit								
	Equipment Equipment Description ID		Emission Point	Group Classification	Stack ID				
	BT-401	High Pressure Absorber (Recovery Device for Air Oxidation Reactors and Dehydration Tower)	Process Vent	Group 2; TRE>4	N/A				
	BT-702 BT-603	Dehydration Tower Scrubber (Recovery Device for Dehydration Tower)Low Pressure Absorber (Recovery device for Dehydration Tower system)	Process Vent	Group 2; 1 <tre<4< td=""><th>O 23O-2</th></tre<4<>	O 23 O-2				
5.E.7	N/A	Piping Equipment	Equipment Leak	N/A	N/A				
	For the Group 2 Process Vent at BT-401 (CR#1 High Pressure Absorber), which includes emissions from the Air Oxidation Reactors (BR-301 A-D) and Dehydration Tower (BT 701/BE 706)-Pursuant to 40 CFR 63.113 (e), the permittee shall maintain a TRE greater than 4.0. For the Group 2 Process Vent at BT-702 603 (CR#1 Dehydration Tower ScrubberLow Pressure Absorber), which includes emissions from Dehydration Tower System including the Dehydration Tower (BT-701/BE 706) and BT-750 Entrainer Tower-Pursuant to 40 CFR 63.113(d), the permittee shall maintain a TRE greater than 1.0. For purposes of determining process vent stream flow rate, total organic hazardous air pollutants or total organic carbon concentration or TRE index value, as specified under paragraph (b), (c), or (d) of δ63.115, the sampling site shall be after the last recovery device but prior to the inlet of any control device that is present prior to release to the atmosphere. To determine the TRE index value, the owner or operator shall conduct a TRE determination and calculate the TRE index value according to the procedures in paragraph (d)(1) or (d)(2) of δ63.115								
5.E.8	and the TRE equation in paragraph (d)(3) of 863.115. Emission Units 03-04 The permittee shall operate emission units 03 and 04 in compliance with the requirements of SC Regulation 61-62.5, Standard No. 4. SC Regulation 61-62.5, Standard No. 4 establishes the maximum allowable emissions of PM to be emitted from emission units 03 and 04 (combined) and establishes the opacity limitation for emission units 03 and 04. Actual PM emissions from emission units 03 and 04 (combined) shall be less than or equal to the maximum allowable emissions. For each point and fugitive source within emission unit 03 and 04, the opacity shall be limited to 20%.								
5.E.9	Regulation 61- maximum allow establishes the units 05 and 00	shall operate emission unit-62.5, Standard No. 4. wable emissions of PM to opacity limitation for emis (combined) shall be less fugitive source within emissions.	SC Regulation 61 be emitted from ension units 05 and than or equal to the second secon	1-62.5, Standard No mission units 05 and 06. Actual PM emis the maximum allowa	o. 4 establishes the d 06 (combined) and sions from emission able emissions. For				

The following emission points in emissions units 05-06 are subject to 40 CFR 63, Subparts A, F, G and H:

EMISSION Unit ID 05 Cooper River #2: Oxidation Unit

Equipment ID	Equipment Description	Emission Point	Group Classification	Stack ID
DT-111	High Pressure Absorber (Recovery Device for Air Oxidation Reactors and Dehydration Tower)	Process Vent	Group <u>+2:</u> TRE>4	N/A
DT-302	Low Pressure Absorber (Recovery device for Dehydration Tower System)	Process Vent	Group 2; 1 <tre<4< th=""><th><u>02-1</u></th></tre<4<>	<u>02-1</u>
N/A	Piping Equipment (in HAPs Service)	Equipment Leak	N/A	N/A

Per 63.113(d), the owner or operator of a Group 2 process vent having a flow rate greater than or equal to 0.005 standard cubic meter per minute, a HAP concentration greater than or equal to 50 parts per million by volume, and a TRE index value greater than 1.0 but less than or equal to 4.0 shall maintain a TRE index value greater than 1.0 and shall comply with the monitoring of recovery device parameters in §63.114(b) or (c) of this subpart, the TRE index calculations of §63.115 of this subpart, and the applicable reporting and recordkeeping provisions of §§63.117 and 63.118 of this subpart. Such owner or operator is not subject to any other provisions of §§63.114 through 63.118 of this subpart.

Per δ63.113(a)(2), the owner or operator of a Group 1 process vent shall reduce emissions of total organic hazardous air pollutants by 98 weight percent or to a concentration of 20 parts per million by volume, whichever is less stringent. For combustion devices, the emission reduction or concentration shall be calculated on a dry basis, corrected to 3 percent oxygen, and compliance can be determined by measuring either organic hazardous air pollutants or total organic carbon using the procedures in δ63.116 of Subpart G.

Per δ63.113(c)(1), if a combustion device is used to comply with δ63.113(a)(2) for a halogenated vent stream, then the vent stream exiting the combustion device shall be dueted to a halogen reduction device. The halogen reduction device shall reduce overall emissions of hydrogen halides and halogen, as defined in δ63.111, by 99 percent or shall reduce the outlet mass of total hydrogen halides and halogens to less than 0.45 kilogram per hour, whichever is less stringent.

The permittee shall operate the air oxidation reactors in compliance with the requirements of 40 CFR 60, Subpart III. However since the vent is also a HON Group 1 process vent, it is required to comply only with the provisions of 40 CFR 63 Subpart G.

The permittee shall operate the dehydration tower in compliance with the requirements of 40 CFR 60, Subpart NNN. However since the vent is also a HON Group 1 process vent, it is required to comply only with the provisions of 40 CFR 63 Subpart G.

The following emission points within emission units 05-06 are subject to the requirements of 40 CFR 60, Subparts A and VV:

Equip ID	Equipment Description	Emission Point	Group Classification	Stack ID
N/A	P iping Equipment (in VOC Service)	Equipment Leak	N/A	N/A

5.E.10

<u>5.E.10a</u>	The permittee shall operate the air oxidation reactors in compliance with the requirements of 40 CFR 60, Subpart III. Per 60.610 (c), each affected facility that has a total resource effectiveness (TRE) index value greater than 4.0 is exempt from all provisions of this subpart except for §§60.612, 60.614(f), 60.615(h), and 60.615(l). Per 60.612(c), maintain a TRE index value greater than 1.0 without use of VOC emission control devices. The permittee shall operate the dehydration tower in compliance with the requirements of 40 CFR 60, Per 60.660 (c)(4), each affected facility that has a total resource effectiveness (TRE) index value greater than 8.0 is exempt from all provisions of this subpart except for §§60.662; 60.664 (d), (e), and (f); and 60.665 (h) and (l). Per 60.662 (c), maintain a TRE index value greater than 1.0 without use of VOC emission control devices.						
5.E.11	Emission Units 07 The permittee shall operate emission unit 07 in compliance with the requirements of SC Regulation 61-62.5, Standard No. 4. SC Regulation 61-62.5, Standard No. 4 establishes the maximum allowable emissions of PM to be emitted from emission units 07 and establishes the opacity limitation for emission unit 07. Actual PM emissions from emission unit 07 shall be less than or equal to the maximum allowable emissions. For each point and fugitive source within emission unit 07, the opacity shall be limited to 20%. The permittee shall also comply with the synthetic minor emission limitation for PM ₁₀ that was established to avoid a PSD review at the time of the construction project approved in 2000 to debottleneck Cooper River #1 and Cooper River #2. The emission limitation is 1.08 lb/hr each for						
		A-E) and 0.48 lb/hr for			0.40 GDD 60		
	The following emission points within emission unit 12 are subject to the requirements of 40 CFR 63, Subparts A, F, G and H: Emission Unit ID 12- Tank Farm						
	Equip ID	Equipment Description	Emission Point	Group Classification	Stack ID		
	AF-101	Px Storage Tank (internal floating roof)	Storage Tank	Group 2	TK-1		
5.E.12	AF-102	Px Storage Tank (internal floating roof)	Storage Tank	Group 2	TK-2		
	AF-103	Px Storage Tank (Internal floating roof)	Storage Tank	Group 2	TK-6		
	N/A	Px Unloading Station-Piping Equipment	Equipment Leak	N/A	N/A		
	Subpart G, the	p 2 storage vessel that owner or operator shal is not required to comp	l comply with the reco	ord keeping requirem	ent in δ63.123(a) of		

The following emission points within emission unit 13 are subject to the requirements of 40 CFR 63, Subparts A, F, G, and H:

Emission Unit 13-Wastewater Treatment

5.E.13

Lillission Onit 13-W	astewater Treatmen	ι		
Equip ID	Equipment	Emission Point	Group	Stack ID
	Description		Classification	
AM-775	Anaerobic	N/A	Group 2	WT-11or U-1/U-
	Reactor			2 /U-11/U-12
AM-704A	Aerobic Basin	N/A	Group 2	N/A
AM-705A	Aerobic Basin	N/A	Group 2	N/A
AM-705B	Aerobic Basin	N/A	Group 2	N/A
AR-751	500,000 gallon	N/A	Group 2	WT-11or U-1/U-
	UASB Reactor			2/ U-11/U-12
AF-754	4,000 gallon	N/A	Group 2	N/A
	UASB Seed			
	Storage Tank			

Emission Unit 13-Wastewater Treatment-The process wastewater has been determined (at the point of determination) to be a Group 2 wastewater stream. No further controls are required on this stream. Records of this determination are maintained at the facility.

Emission Unit 11

The permittee shall operate each generator, compressor, and pump in compliance with the applicable requirements of 40 CFR 63 Subpart ZZZZ, National Emission Standards For Hazardous Air Pollutants For Stationary Reciprocating Internal Combustion Engines

The permittee shall operate each generator, compressor, and pump in compliance with the requirements of SC Regulation 61-62.5, Standard No. 4. SC Regulation 61-62.5, Standard No. 4 establishes the respective opacity limitations for these units. The opacity limitation for the generators, compressors, and pumps are summarized in the table below.

The allowable operating hours per year and fuel sulfur content (percent sulfur) for each generator, compressor, and pump is summarized in the table below.

Equip ID	Combustion Source	Opacity	PM/PM ₁₀	SO_2	NO _x	СО	VOC	No. 2 fuel oil Percent Sulfur	Hrs/yr
AM- 804	Emergency Generator #1	40%	N/A	N/A	N/A	N/A	N/A	<0.3%	No limits <100**
AC-402	Emergency Compressor #1	40%	N/A	N/A	N/A	N/A	N/A	<0.3%	No limits <100**
AG- 202B	Emergency Fire Water Pump	40% 20%	N/A	N/A	N/A	N/A	N/A	<0.3%	No limits <100**
AG-229	T-Head FW Pump	40% 20%	N/A	N/A	N/A	N/A	N/A	<0.3%	No limits <100**
AG- 202C	Emergency Fire Water Pump	20%	N/A	N/A	N/A	N/A	N/A	<0.05%	<250
AG- 202D	Emergency Fire Water Pump	20%	N/A	N/A	N/A	N/A	N/A	<0.05%	<250
BM- 1201	Emergency Generator #2 (CR#1)	40%	N/A	N/A	N/A	N/A	N/A	<0.3%	<250 <100**
DM- 135	Emergency Generator #3 (CR#2)	20%	0.368	0.355	5.2	0.20	0.175	<0.05%	<500
AC-404	Emergency Air Compressor #2 (Utility)	20%	0.175	1.165	14.265	0.65	0.60	<0.05%	<1,000 ≤500
AM- 838	IT Emergency Generator	20%	N/A	N/A	3.64	N/A	N/A	<0.05%	<500
L-1 and L-2	(Leased) Compressors #1 and #2	20%	7.884	13.14	15.33	3.286	2.322	<0.0 <u>01</u> 5% **	8760*

^{*} Total for both compressors

Emission Unit 12

The permittee shall operate emission unit 12 in compliance with the requirements of SC Regulation 61-62.5, Standard No. 4. SC Regulation 61-62.5, Standard No. 4 establishes the opacity limitation for emission unit 12. The opacity limitation for each point and fugitive emissions source within emission unit 12 is as follows:

5.E.15

5.E.14

Source Description	Stack ID. No.	Opacity Limitation
Px Storage Tank (internal	TK-1	20%
floating roof)		
Px Storage Tank (internal	TK-2	20%
floating roof)		
Px Storage Tank (internal	TK-6	20%
floating roof)		

^{**}Limit per 40 CFR 63 Subpart ZZZZ

	Emission Unit 13
5.E.16	The permittee shall operate emission unit 13 in compliance with the requirements of SC Regulation 61-62.5, Standard No. 4. SC Regulation 61-62.5, Standard No. 4 establishes the opacity limitation for emission unit 13. The opacity limitation for each point and fugitive emission source within emission unit 13 shall be limited to 20%.
	Conditions 5.E.15 and 5.E.16 Voided
5.E.17	When the "Net Volatile Organic Compound (VOC) Emissions Increase" for any new, modified or altered source exceeds 100 tons per year since June 25, 2004, Best Available Control technology shall be applied to the construction permit. The "Net Volatile Organic Compound (VOC) Emissions Increase" from this facility shall not exceed 100 tons since July 1, 1979. The "Net VOC Emissions Increase" includes any increases and decreases in the actual VOC emissions at the facility that have occurred since July 1, 1979 and are otherwise creditable. Increases in the VOC emissions from these existing sources may be subject to the applicability requirements of SC Regulation 61 62.5, Standard No. 5.1, Best Available Control Technology (BACT)/Lowest Achievable Emission Rate ("LAER") Applicable To Volatile Organic Compounds.
	The permittee shall operate Boiler No. 3 (AB-350A) and Boiler No. 4 (AB-350B) in compliance with the requirements of SC Regulation 61-62.5, Standard No. 1. In accordance with SC Regulation 61-62.5, Standard No. 1 - Emissions from Fuel Burning Operations, Section II - Particulate Matter Emissions, the allowable discharge of particulate matter resulting from the fuel burning operations is 0.6 lbs/10 ⁶ BTU input. In accordance with SC Regulation 61-62.5, Standard No. 1 - Emissions from Fuel Burning Operations, Section III - Sulfur Dioxide Emissions, the maximum allowable discharge of SO ₂ resulting from the fuel burning operations is 3.5 lbs/10 ⁶ BTU input. Boiler No. 3 and Boiler No. 4 are permitted to burn only natural gas, No. 2 VLSD (Very Low Sulfur Distillate) fuel oil, and biogas from the Anaerobic reactor or UASB and onsite spec used oil as a fuel. The No. 2 VLSD fuel oil, which is only to be burned during a natural gas supply curtailment, sulfur content shall be less than or equal to 0.5% by weight. The use of any other substances as fuel is
5.E.18	prohibited without prior written approval from the Bureau of Air Quality. In accordance with SC Regulation 61-62.5, Standard No. 1, Emissions from Fuel Burning Operations, Boiler No. 3 and Boiler No. 4 shall not discharge into the ambient air smoke which exceeds an opacity of 20%. The twenty (20) percent opacity limit may be exceeded for soot blowing, but may not be exceeded for more than six (6) minutes in a one hour period nor be exceeded for more than a total of twenty-four (24) minutes in a twenty-four (24) hour period. Emissions caused by soot blowing shall not exceed sixty (60) percent opacity. The opacity standards set forth above do not apply during startup or shutdown. The owner/operator shall, to the extent practicable, maintain and operate any source including associated air pollution control equipment in a manner consistent with good air pollution control practices for minimizing emissions. The owner/operator shall, for a period of at least five (5) years maintain a log of the time, magnitude, duration and any other pertinent information to determine periods of startup and shutdown and make these records available to a Department representative upon request. Also see condition 5.E.21 for the opacity requirements for the NSPS regulation.

1	D 1 1 1 1 1 1 1 1 1	10.10.1	0 1 11 1 11	
5.E.19	and on site generated spee used of fuel in case of a natural gas supply the definition of "very low sulfur content of 0.5 percent. Boile 18,675,0002,400,000 gallons of V to operating each boiler at a maximbe operated on natural gas for the in the boilers is subject to a limit of x106 SCF per year. The use of any the Bureau of Air Quality. The t	ii. They are also permitted to be interruption. The distillate fue of oil" contained in 40 CFR 60.4 or No. 3 and Boiler No. 4 LSD fuel oil per year. Based on num of 3,150 hours per year on remainder of the year. The or of 10,000 gallons per year. The or other substances is prohibited verm year in this condition refer x, and CO shall be calculated up	vVLSD fuel oil. Each boiler would site generated spec used oil burned a biogas is subject to a limit of 440 without prior written approval from rs to a rolling 12-month sum. The sing a 12-month rolling sum. The	
5.E.20	Boiler No. 3 and Boiler No. 4 are and Db, New Source Performanc Generating Units. The boilers are less than a 10% capacity factor.	e subject to the applicable require Standards for Industrial, Cogas boilers which will only burn	rements of 40 CFR 60 Subparts A mmercial, and Institutional Steam oil infrequently and are limited to	
5.E.21		This NSPS opacity standard of	o an opacity of 20% except for one does not apply during start-up and	
5.E.22	Per §60.48b(a)13(1)(2), the owner under §60.43b shall install, calib measuring the opacity of emissic system. that limits oil burning to	r or operator of an affected faci- orate, maintain, and operate a cons discharged to the atmosph o a 10% capacity factor and w approved alternative monitoring	continuous monitoring system for	
5.E.23	Per 40 CFR 60 Subpart Db, the N Btu (for high release rate).	NO_x limit is 0.10 lb/ 10^6 Btu (fo	or low release rate) and 0.20 lb/10 ⁶	
5.E.24	Boiler No. 3, and Boiler No. 4 and 2 HPVGTS heater DB-1813 shall be in compliance with 40 CFR 63 Subpart DDDDD, "National Emission Standards for Hazardous Air Pollutants for Industrial, Commercial, and Institutional Boilers and Process Heaters" upon start up of these units by the appropriate compliance date in the final regulation. The permittee must submit an Initial Notification not later than 120 days after becoming subject to this subpartand Notice of Compliance status containing the information listed in the regulation by the dates stated in the regulation. The Initial Notification must include the information required in §63.7545, as applicable. The permittee shall be in compliance with the emission limits and the work practice standards in this subpart at all			
5.E.25	only fossil fuels and other gases a and applicable work practice stan	process heaters in one of the land do not burn any residual oil idards shown below. The pernompliance with the emission lin	liquid fuel subcategories that burn l are subject to the emission limits nittee is not required to conduct a nits. The permittee is not required	
5.E.26	To demonstrate initial compliance the NOCS report required in §63 other than residual oils, either alon	8.7545(e) that indicates the faci	must include a signed statement in ility burns only liquid fossil fuels	
5.E.27			l be NO _x Budget units as they will design heat input greater than 250	

5.E.28	The facility is subject to the applicable requirements of 40 CFR 63 Subpart ZZZZ, National Emission Standards For Hazardous Air Pollutants For Stationary Reciprocating Internal Combustion Engines.				
5.E.29	The content of the on-site generated spec used oil shall meet the definition of used oil as defined by Section I, definition 83, of SC Regulation 61-62.1.				
	Conditions 5.E.28 and 5.E.29 Voided				
5.E.30	The facility shall implement a VOC LDAR (Leak Detection and Repair Program) equivalent to the requirements of 40 CFR 60 Subpart VV (per the regulation as of November 1, 2006) and submit to the Department before placing construction permit 0420 0029 CR into operation. The use of the LDAR program was voluntarily used for the purpose of a PSD offset.				
5.E.31	For Cooper River #2, emission limitations were established to avoid a PSD review for the project to construct Cooper River #2 that was approved in Construction Permit Nos. 0420-0029 CF. The maximum allowable VOC emission rate from the #2 OX and PTA units is 215.9 tpy and 49.3 lbs/hr.				
<u>5.E.32</u>		Limit 100 hrs/yr Minimize to a period needed for appropriate and safe loading of the engine, not to exceed 30 minutes Change oil & filter every 500 hours, Inspect air cleaner every 1,000 hours, Inspect/Replace as necessary hose & belt every 500 hours or do these annually; whichever comes sooner. Must operate and maintain according to the manufacturer's emission related written			
	Operate & maintain per plan	instructions or develop your own maintenance plan which must provide to the extent practicable for the maintenance and operation of the engine in a manner consistent with good air pollution control practice for minimizing emissions			

	Insignificant Activity Generators				
	The permittee shall operate generators AM-40 CFR 60 Subpart IIII. The respective req	-840 and AM-849 in compliance with the requirements of uirements are summarized below:			
	<u>Requirement</u>	<u>Limit</u>			
		HC - 1.0 g/HP-hr			
	AM-840 meet Table 1 standards in 40	NOx - 6.9 g/Hp-hr			
	<u>CFR 60 Subpart IIII</u>	$\underline{\text{CO} - 8.5 \text{ g/HP-hr}}$			
		<u>PM – 0.40 g/HP-hr</u>			
<u>5.E.33</u>	Hours of operation per year for maintenance checks and readiness testing	<u>100 hrs/yr</u>			
	Operate & maintain per plan	Operate and maintain the stationary CI internal combustion engine and control device according to the manufacturer's emission-related written instructions;			
	AM-849 meet Table 1 Tier 2 standards in 40 CFR 89.112	$\frac{\text{NMHC} + \text{NOx} - 7.5 \text{ g/KW-hr}}{\text{CO} - 5.0 \text{ g/KW-hr}}$ $\frac{\text{PM} - 0.40 \text{ g/KW-hr}}{\text{PM} - 0.40 \text{ g/KW-hr}}$			

PART 6.0 MONITORING AND REPORTING REQUIREMENTS [SC Regulation 61-62.1, Section II]; [SC Regulation 61-62.70.6(a)(3)(i)(B)]

MONITORING AND REPORTING A.

Table 6.1 contains summaries of the monitoring and reporting required of this facility.

	TABLE 6.1 MONITORING AND REPORTING					
Unit ID	Pollutant/ Parameter	Limit	Required Monitoring	Monitoring Frequency	Reporting Frequency	Condition Number
01-14 03-16	Record keeping	See Condition	N/A	N/A	See Condition	6.B.1
01-14 03-16	Reporting	See Condition	N/A	N/A	N/A	6.B.3
01-14 03-16	VOCs	100 TPY VOC Net Increase	See Condition	See Condition	See Condition	6.B.34
01-14 03-16	Source Testing	See Condition	See Condition	See Condition	See Condition	6.B.25
03	CR#1 Ox Unit Production	See Condition	See Condition	See Condition	Semiannual	6.B.7
03-14	Opacity	20%	Visual Inspection	Semiannual	Semiannual	6.B.2
03-06	PM Testing/ Operator Training	N/A	See Condition	See Condition	See Condition	6.B.35
03	Calculated delta T (CR#1- HPVGTS)	See Condition (CAM)	Record keeping	Continuously with daily average	Semiannual	6.B.21, 6.B.24

	TABLE 6.1 MONITORING AND REPORTING					
Unit ID	Pollutant/ Parameter	Limit	Required Monitoring	Monitoring Frequency	Reporting Frequency	Condition Number
03	Inlet temperature (CR#1- HPVGTS)	See Condition (CAM)	Record keeping	Continuously with daily average	Semiannual	6.B.21, 6.B.24
03	Liquid flow rate (Intermediate Storage Silo Scrubber BT- 501)	See Condition (CAM)	Record keeping	Continuously with daily average	Semiannual	6.B.20, 6.B.24
03	Water and Acetic Acid Scrubbing Flow Rates (DHT Scrubber)	See Condition	Record keeping	Continuously with daily average	Semiannual	6.B.6
03	Acetic Acid Scrubbing Liquid temperature (DHT Scrubber)	See Condition	Record keeping	Continuously with daily average	Semiannual	6.B.6
03	BT-603 LPA Top Temperature & scrubbing liquid flow	See Condition (CAM)	Record keeping	Continuously with daily average	Semiannual	6.B.20, 6.B.24
03	Condenser (BE-645)	See Condition	Record keeping	Daily	Semiannual	6.B.19
03	TRE Value (HPA)	> 4	Record keeping	See Condition	See Condition	6.B.8, 6.B.9
03	TRE Value (DHT Serubber Outlet LPA Outlet)	Greater than 1 and less than 4	Record keeping	See Condition	Semiannual	6.B.8, 6.B.9
03	(HPVGTS) VOCs, CO	See Condition	Stack test	Biennial	Biennial	6.B.25
03	LPA (VOCs, CO)	See Condition	Stack test	Biennial	Biennial	6.B.25
03	DHT Scrubber (VOCs, CO)	See Condition	Stack test	Biennial	Biennial	6.B.25
03	VOCs	LDAR	Record keeping	See Condition	Semiannual	6.B.56, 6.B.57
04	Pressure Crystallizer Vent Scrubber (CM-301)	See Condition (CAM)	Record keeping	At least once per day Daily	Semiannual	6.B.21, 6.B.24

	TABLE 6.1 MONITORING AND REPORTING					
Unit ID	Pollutant/ Parameter	Limit	Required Monitoring	Monitoring Frequency	Reporting Frequency	Condition Number
04	Pressure drop (Day Silo Bag Filters CM-603A & B)	See Condition	Record keeping	Daily	Semiannual	6.B.17
04	Pressure drop (Dust Collectors CM-608 A &B)	See Condition	Record keeping	Daily	Semiannual	6.B.17
05	Liquid flow rate (Intermediate Silos Vent Scrubber DT- 500)	See Condition	Record keeping	Daily	Semiannual	6.B.18
05	CR#2 Low Pressure Absorber (DT-302)	See Condition (CAM)	Record keeping	Continuously with daily average	Semiannual	6.B.22, 6.B.24
05	CR#2 CRU Evaporator Overhead Condenser (DE-416)	See Condition	Record keeping	Daily	Semiannual	6.B.19
06	Vent Header Flow (Crystallizer Vent Scrubber DM-601/DE- 601)	See Condition (CAM)	Record keeping	Continuously with daily average	Semiannual	6.B.23, 6.B.24
06	Pressure drop (Day Silo Dust Collectors DM-797 A/B)	See Condition	Record keeping	Daily	Semiannual	6.B.17
05-06	Inlet temperature (CR#2 HPVGTS)	See Condition (HON)	Record keeping	Continuously with daily average	Semiannual	6.B.10- 6.B.16
05-06	Calculated <u>AT (CR#2</u> <u>HPVGTS)</u>	See Condition (HON)	Record keeping	Continuously with daily average	Semiannual	6.B.10 6.B.16
05-06	(CR#2 HPVGTS) Effluent pH	See Condition (HON)	Record keeping	Continuously with daily average	Semiannual	6.B.10 6.B.16

TABLE 6.1 MONITORING AND REPORTING						
Unit ID	Pollutant/ Parameter	Limit	Required Monitoring	Monitoring Frequency	Reporting Frequency	Condition Number
05-06	Liquid to gas ratio (gallons/sef) (CR#2 HPVGTS)	See Condition (HON)	Record keeping	Continuously with daily average	<u>Semiannual</u>	6.B.10- 6.B.16
05-06	Calculated delta T (CR#2 HPVGTS)	CAM Presumptive Monitoring (HON)See condition CAM	See HON monitoring Recordkeeping	Continuously with daily average See HON monitoring	See HON monitoring Semiannual	6.B.22 <u>.</u> 6.B.24
<u>05</u>	Inlet temperature (CR#2- HPVGTS)	See Condition (CAM)	Record keeping	Continuously with daily average	Semiannual	6.B.22, 6.B.24
05	HPVGTS (VOCs)	See Condition	Record keeping	Biennial 36 months	Biennial 36 months	6.B.25
03-06	VOCs	Less than 1825 TPY	See Condition	See Condition	See Condition	6.B.26
05-06	VOCs	See Condition	See Condition	See Condition	See Condition	6.B.33
07	Pressure drop (Loading spout dust collectors CM-705A, B & C)	See Condition	Record keeping	Daily	Semiannual	6.B.17
07	Pressure drop (Truck Loading Dust collectors CM-722)	See Condition	Record keeping	Daily	Semiannual	6.B.17
07	Pressure drop (Shipping Storage Silo Dust collectors CM-701 A-E)	See Condition	Record keeping	Daily	Semiannual	6.B.17
07	Pressure drop (Shipping Storage Silo Dust collectors CM-720 A/B)	See Condition (CAM)	Record keeping	Continuously with daily average	Semiannual	6.B.23, 6.B.24
11	Hours of operation	See Condition	See Condition	See Condition	Semiannual	6.B.27, 6.B.28
11	Fuel sulfur content	See Condition	See Condition	See Condition	Semiannual	6.B.27, 6.B.28
<u>IAG</u>	Hours of operation	See Condition	See Condition	See Condition	<u>Semiannual</u>	6.B.27, 6.B.28

TABLE 6.1 MONITORING AND REPORTING						
Unit ID	Pollutant/ Parameter	Limit	Required Monitoring	Monitoring Frequency	Reporting Frequency	Condition Number
<u>IAG</u>	Fuel sulfur content	See Condition	See Condition	See Condition	Semiannual	6.B.27, 6.B.28
03-06, 12	HAPs	Per 40 CFR 63.112	Record keeping	See Condition	See Condition	6.B.29, 6.B.31- 6.B.34
13	HAPs	Per 40 CFR 63.112	Record keeping	See Condition	See Condition	6.B.30
15-16	Opacity	20%	COMS Source test (Based on NSPS Subpart Db)	Continuous Initial and annual RATA test	Quarterly within 30 days of test	6.B.39
15-16	PM (fuel oil consumption)	18,675,000 2,400,000 gallons per year each boiler	Record keeping	Daily	Semiannual	6.B.36
15-16	fuel oil sulfur content	0.5% sulfur by weight	Record keeping	Daily	Semiannual	6.B.36, 6.B.45, 6.B.46
15-16	PM	0.6 lb/10 ⁶ Btu of heat input each (3- hour average)	fuel supplier certification, and fuel oil consumption records will be maintained	Daily	Semiannual	6.B.36
15-16	<mark>₽M</mark>	50.9 TPY (for both boilers combined 12 month rolling sum)	Calculate a twelve month rolling sum using stack test data, sulfur content, and fuel consumption records.	Monthly	Semiannual	6.B.37
15-16	PM	50.9 TPY (for both boilers combined 12 month rolling sum)	Initial then biennial PM stack tests	Initial then biennial	Biennial	6.B.38
15-16	$\frac{\mathrm{PM}_{10}}{\mathrm{PM}_{10}}$	50.9 TPY (for both boilers combined 12 month rolling sum)	Initial then biennial PM stack tests	Initial then biennial	Biennial	6.B.38
15-16	<mark>₽M</mark>	0.03 lb/10 ⁶ Btu of heat input each (3 hr average)	Record keeping	Daily	NOCS submittal then Semiannual	6.B.47
15-16	SO_2	3.5 lb/10 ⁶ Btu of heat input each (24-hour average)	fuel supplier certification, and fuel oil consumption records will be maintained	Daily	Semiannual	6.B.36

	TABLE 6.1 MONITORING AND REPORTING						
Unit	Pollutant/	Limit	Required	Monitoring	Reporting	Condition	
1D 45 16	Parameter SO2	733.4 TPY (for both boilers combined-12 month rolling sum)	Monitoring An initial stack test only, fuel supplier certification, and fuel oil consumption records will be maintained	Frequency	Frequency Semiannual	Number 6.B.37, 6.B.38	
15-16	NO_x	0.10 lb/10 ⁶ Btu of heat input (30 day average)	Continuous nitrogen oxides monitor will be installed for NOx-SIP call these monitors can also be used to meet the NSPS requirements for NOx	Continuous (30 day average)	Quarterly	6.B.40, 6.B.41- 6.B.44	
15-16	NO_X	317.0 TPY for both boilers combined (12- month rolling sum)	Calculate a twelve-month rolling sum using stack test data	Monthly	Semiannual	6.B.37	
15-16	CO	299.6 TPY, for both boilers combined (12- month rolling sum)	Calculate a 12- month rolling sum using stack test or Continuous Emissions Monitoring System	Monthly	Semiannual	6.B.37	
15-16	CO	400 ppm by volume on a dry basis corrected to a 3% oxygen (30 day average)	CO continuous monitoring is required by the Boiler MACT Standard	Continuous (30 day average)	NOCS submittal then semiannual	6.B.49- 6.B.50	
15-16	Hydrogen Chloride	0.0005 lb/10 ⁶ Btu of heat input (30 day average)	Fuel mixture monitoring	Initial compliance demonstration and monthly monitoring	Semiannual	6.B.47 6.B.48	
15-16	NO _X , heat input, flow	As specified	CEMS	Continuous during control period	Quarterly	6.B.51- 6.B.54	
15-16	Used oil	See Condition	See Condition	Used oil analysis	Semiannual	6.B.4, 6.B.5	
Facility -wide	Temporary units	See condition	See Condition	See Condition	See Condition	6.B.55	

N/A = Not Applicable

B. MONITORING AND REPORTING CONDITIONS

Condition Number	Conditions			
6.B.1	Emission Unit 01-14 Unless otherwise specified in a more specific requirement, all monitoring shall be performed as follows: a. For control devices that have a monitoring frequency specified as "continuously with daily average", at least one data point shall be obtained each 15-minute period and all data points collected within a 24-hour period (during those times that the process or emissions generating equipment was being operated) shall be averaged together for a daily reading for comparison to an established monitoring range. b. For control devices that have a monitoring frequency specified as "daily reading", at least one reading will be taken in a 24-hour period (during a time that the process or emissions generating equipment was operating) for comparison to an established monitoring range. However, more than one reading may be taken in a 24-hour period (during a time that the process or emission generating equipment was operating) and all readings taken in the 24-hour period shall be averaged together for a daily reading for comparison to an established parameter.			
6.B.2	To assure compliance with the opacity limitations, the permittee shall comply with the following requirement: The permittee shall perform a visual inspection on a semiannual basis. Visual Inspection means a qualitative observation of opacity during daylight hours where the inspector records results in a log, noting color, duration, density (heavy or light), cause and corrective action taken for any abnormal emissions. The observer does not need to be certified to conduct valid visual inspections. However, at a minimum, the observer should be trained and knowledgeable about the effects on visibility of emissions caused by background contrast, ambient lighting, and observer position relative to lighting, wind, and the presence of uncombined water. No periodic monitoring for opacity will be required during periods of burning natural gas or propane only. Logs shall be kept to record all visual inspections, including cause and corrective action taken for any abnormal emissions and visual inspections from date of recording. The logs shall be maintained for a period of five (5) years and be made available to the Department upon request. The owner/operator shall submit semiannual reports to the Manager of the Technical Management Section, Bureau of Air Quality postmarked no later			
6.B.3	than 30 calendar days after the end of the reporting period. All records required under this Part 70 operating shall be maintained on site for a period of at least five (5) years and made available to Department personnel upon request. This permit contains compliance certification, testing, monitoring, reporting, and record keeping requirements sufficient to assure compliance with the terms and conditions of this permit. All submittals required by these conditions shall be sent to the South Carolina Department of Health and Environmental Control - Bureau of Air Quality (SC DHEC - BAQ) at the following address: SC DHEC - BAQ Technical Management Section 2600 Bull Street Columbia, SC 29201 The semi-annual monitoring reports required by this permit must be submitted within 60 days of the end of the monitoring period to the above address.			

Condition Number			Conditions			
6.B.4	Emission Unit 15-16 The content of the on-site generated spec used oil shall meet the definition of used oil as defined by Section I, definition 83, of SC Regulation 61-62.1. A sample of the used oil will be analyzed semiannually for specification used oil metals and sulfur content. A summary of these used oil analyses shall be submitted on an semiannual basis.					
6.B.5	Emission Unit 15-16 Because of the nature of the waste gas that is routed to the boilers stack testing will not be required for compliance with Standard No. 3 at this time. This is a State only enforceable requirement.					
6.B.6	for the first stage in liquid inlet tempera gauges shall be reactive, on ground leve (i.e., on ground leve (i.e., at least every Department personn (i.e., computerized Operational ranges assurance of complistack test data, vedemonstrate the prousing this procedure site for a period of Department personn including date and ties of the period of the pe	let (water), liquid flow ture gauge for the sec lily accessible for verification of the experiment of	meters for the second stage as apprication by operation by operation by operational stages and the second stages are also as a secompanied by place. Semianness of the second secompanied by place.	en established to provide a reasonable monitored parameters were derived from history and visual inspections, which pliance. These ranges may be updated monitoring data shall be maintained on enerated and shall be made available to eration outside these operational ranges, thall be recorded and kept on site for five		
6.B.7	12-month sum. The semi-annual basis. factors and/or contro annual (12-month re	se production records, The production rates, a of efficiencies and site of the sum of th	calculations, and clong with stack te specific factors w	e recorded and used to calculate a rolling calculation results will be submitted on a est data, other Bureau approved emission ill be used to calculate the CO and VOC GTS, and the DHT Scrubber.		
	Condition 6.B.7 Voi		h Dragging Alexa	where shall comply with the small of		
6.B.8		Control or Recovery Device CR#1 High Pressure Absorber (Recovery Device) CR#1 High Pressure Absorber (Recovery Device) CR#1 High Low Pressure Absorber (Recovery Device)		TRE Index Greater than 4.0 Greater than 4.0		

Condition Number	Conditions
	a. For the Group 2 Process Vent at BT-401 (CR#1 High Pressure Absorber), which includes emissions from the Air Oxidation Reactors (BR-301-A-D) and Dehydration Tower (BT 701/BE 706) - Pursuant to 40 CFR 63.113 (e), the permittee shall maintain a TRE greater than 4.0 and comply with the following requirements:
	 i. Provisions for calculating TRE index in 40 CFR 63.115. ii. Reporting and record keeping provisions in 40 CFR 63.117(b), 63.118(c), and 63.118(h).
	b. The owner or operator of a Group 2 process vent with a TRE index greater than 4.0 as specified in §63.113(e), shall maintain records of measurements, engineering assessments, and calculations performed to determine the TRE index value of the vent stream. Documentation of engineering assessments shall include all data, assumptions, and procedures used for the engineering assessments, as specified in §63.115(d)(1).
	c. The owner or operator who elects to demonstrate compliance with the TRE index value greater than 4.0 under §63.113(e) shall keep up-to-date, readily accessible records of:
	 i. Any process changes as defined in §63.115(e); and ii. Any recalculation of the TRE index value pursuant to §63.115(e).
6.B.9	d. Whenever a process change, as defined in §63.115(e), is made that causes a Group 2 process vent with a TRE greater than 4.0 to become a Group 2 process vent with a TRE less than 4.0, the owner or operator shall submit a report within 180 calendar days after the process change. The report may be submitted as part of the next periodic report. The report shall include:
	 i. A description of the process change, ii. The results of the recalculation of the TRE index value required under §63.115(e) and recorded under paragraph (c) of §63.118, and iii. A statement that the owner or operator will comply with the requirements specified in §63.113(d).
	iv. The owner or operator of a source subject to Subpart G shall submit Periodic Reports. Except as specified under paragraphs (c)(5) and (c)(6) of section §63.152, reports containing information in paragraphs 63.152(c)(2), (c)(3), and (c)(4) shall be submitted semi-annually no later than 60 calendar days after the end of each 6-month period.
	e. For the Group 2 Process Vent at BT-702_603 (CR#1 DHT ScrubberLow Pressure Absorber), which includes emissions from the Dehydration Tower (BT-701/BE-706) and Entrainer Tower (BT-750) - Pursuant to 40 CFR 63.113 (e), the permittee shall maintain a TRE between 1.0 and 4.0 and comply with the following requirements:
	 i. Provisions for calculating TRE index in 40 CFR 63.115. ii. Monitoring of recovery device parameters per provisions of 40 CFR 63.114(b) using the alternate parameters approved by DHEC in a letter of August 11, 2003. iii. Reporting and record keeping provisions in 40 CFR 63.117(b), 63.118(c), and 63.118(h)

Condition Number					litions		
	The Control Dev requirements of 4	ice CR#2 HP 0 CFR 63.	VGTS sh	<mark>all compl</mark>	y with the	monitoring,	, recordkeeping and reporting
	Equipment	Control	Control Device		Group Classification		Reduction Required
6.B.10	High Pressure Absorber		HPVGTS		<u> </u>		t % or to a concentration of 20 ppm by volume
	Dehydration Tower	HPV	, 		1		t % or to a concentration of 20 ppm by volume t % or to a concentration of
	Reactors DR 10 A/B 1st Crystallize				1		20 ppm by volume t % or to a concentration of
	DD201				1	2	2 0 ppm by volume
	40 CFR 63:	s a summary	or the mo	mitoring (ina reportif	ig required	for Emission Units 05-06 per
	Emission Unit			Monitoring Frequency		ging time	Condition
	05-06	Inlet emperature (HPVGTS exidizer)	Continuously D		aily	6.B.13-6.B.17	
	05-06	Calculated Delta T (HPVGTS exidizer)	a T GTS		Đ	<mark>aily</mark>	6.B.13-6.B.17
	05-06	Effluent pH (HPVGTS scrubber)	Contin	nuously	Đ	<mark>aily</mark>	6.B.13-6.B.17
6.B.11		iquid to gas ratio gallons/scf) (HPVGTS serubber)	Contin	nuously	D .	aily	6.B.13 6.B.17
	The owner or operator of a HON Group 1 process vent shall reduce emissions of total organic hazardous air pollutants by 98 weight percent or to a concentration of 20 parts per million by volume, whichever is less stringent. For combustion devices, the emission reduction or concentration shall be calculated on a dry basis, corrected to 3 percent oxygen, and compliance can be determined by measuring either organic hazardous air pollutants or total organic carbon using the procedures in §63.116 of Subpart G.						
	device) shall be of it is discharged to hydrogen halides	lucted to a ha o the atmosp and halogens	l <mark>logen red</mark> here. The s, as defin	uction de halogen ed in §63	vice, included reduction of the sub-	ling but not device shall part G, by	colled by combustion control thimited to a scrubber, before I reduce overall emissions of 99 percent or shall reduce the ogram per hour, whichever is

Non-Confidential

Condition Number	Conditions
	Each owner or operator of a HON Group 1 process vent that uses a combustion device to comply with the requirements in §63.113 (a)(2) of subpart G, shall install monitoring equipment specified below. All monitoring equipment shall be installed, calibrated, maintained, and operated according to manufacturer's specifications or other written procedures that provide adequate assurance that the equipment would reasonably be expected to monitor accurately.
	i) For the catalytic oxidizer (DR 1814), temperature monitoring devices shall be installed in the gas stream immediately before and after the catalyst bed.
	ii.) For the bromine scrubber (DT-1821), the following monitoring equipment is required for the scrubber:
(5.42	A.) A pH-monitoring device equipped with a continuous recorder shall be installed to monitor the pH of the scrubber effluent.
6.B.12	B.) A flow meter equipped with a continuous recorder shall be located at the scrubber influent for liquid flow. Gas stream flow shall be determined using one of the procedures specified as follows:
	1. The owner or operator may determine gas stream flow using the design blower capacity, with appropriate adjustments for pressure drop.
	2. The owner or operator may prepare and implement a gas stream flow determination plan that documents an appropriate method which will be used to determine the gas stream flow. The plan shall require determination of gas stream flow by a method which will at least provide a value for either a representative or the highest gas stream flow anticipated in the scrubber during representative operating conditions other than start ups, shutdowns, or malfunctions. The plan shall include a description of the methodology to be followed and an explanation of how the selected methodology will reliably determine the gas stream flow, and a description of the records that will be maintained to document the determination of gas stream flow. The owner or operator shall maintain the plan as specified in §63.103(c).
	The owner or operator of a process vent using a vent system that contains bypass lines that could divert a vent stream away from the control device used to comply with §63.113(a)(2) of subpart G shall comply with the paragraphs shown below. Equipment such as low leg drains, high point bleeds, analyzer vents, open ended valves or lines, and pressure relief valves needed for safety purposes are not subject to this paragraph.
6.B.13	i.) Properly install, maintain, and operate a flow indicator that takes a reading at least once every 15 minutes. Records shall be generated as specified in \$63.118(a)(3) of subpart G. The flow indicator shall be installed at the entrance to any bypass line that could divert the vent stream away from the control device to the atmosphere; or
0.B.13	ii.) Secure the bypass line valve in the non-diverting position with a car-seal or a lock-and-key type configuration. A visual inspection of the seal or closure mechanism shall be performed at least once every month to ensure that the valve is maintained in the non-diverting position and the vent stream is not diverted through the bypass line.
	iii.) Maintain a continuous record of valve (by pass valve) position as a means to determine a by-pass condition. The valves (by-pass valves) are either fully open or fully closed and are not designed to regulate or adjust flow. The positions of the valves (open or closed) can be confirmed on a continuous basis by limit switches via a Distributive Control System (DCS). These limit switches will be maintained and tested in accordance with the manufacturer's recommendations.

Condition Number	Conditions
	Each owner or operator subject to the control provisions for Group 1 vent shall keep an up to date, readily accessible record of the following data:
	i.) If any subsequent TRE determinations or performance tests are conducted after the Notification of Compliance Status (NCS) has been submitted, report the data in paragraphs (a)(4) through (a)(8) of §63.117 in the next Periodic Report as specified in §63.152(e) of this subpart.
	ii.) Record and report the following in the NCS when using a combustion device to achieve a 98 weight percent reduction in organic HAP or an organic HAP concentration of 20 parts per million by volume, as specified in §63.113(a)(2) of this subpart:
	A.) The parameter monitoring results for catalytic oxidizer (DR-1814) specified in Table 3 of subpart G, and averaged over the same time period of the performance testing.
6.B.14	B.) For an incinerator, the percent reduction of organic HAP or TOC achieved by the incinerator determined as specified in §63.116(c) of this subpart, or the concentration of organic HAP or TOC (parts per million by volume, by compound) determined as specified in §63.116(c) of this subpart at the outlet of the incinerator on a dry basis corrected to 3 percent oxygen.
	iii.) Record and report the following in the NCS when using a scrubber following a combustion device to control a halogenated process vent stream:
	A.) The percent reduction or scrubber outlet mass emission rate of total hydrogen halides and halogens as specified in §63.116(d) of Subpart G;
	B.) The pH of the scrubber effluent; and
	C.) The scrubber liquid to gas ratio; and
	iv.) Record and report in the NCS the halogen concentration in the process vent stream determined according to the procedures specified in \(\)663.115(d)(2)(v) of subpart G.

Condition Number	Conditions
	Each owner or operator using a control device to comply with §63.113 (a)(2) of subpart G shall keep the following records up to date and readily accessible:
	i.) Continuous records of the equipment operating parameters specified to be monitored under §63.114(a) of this subpart and listed in table 3 of this subpart or specified by the Administrator in accordance with §63.114(c) and §63.117(e) of this subpart.
	ii.) Records of the daily average value of each continuously monitored parameter for each operating day determined according to the procedures specified in §63.152(f).
	iii.) The daily average shall be calculated as the average of all values for a monitored parameter recorded during the operating day, except as provided in paragraph (a)(2)(ii) of §63.118. The average shall cover a 24 hour period if operation is continuous, or the number of hours of operation per operating day if operation is not continuous.
6.B.15	iv.) Monitoring data recorded during periods of monitoring system breakdowns, repairs, calibration checks, and zero (low level) and high level adjustments shall not be included in computing the hourly or daily averages. Records shall be kept of the times and durations of all such periods and any other periods of process or control device operation when monitors are not operating.
	v.) The operating day shall be the period from midnight to midnight.
	vi.) If all recorded values for a monitored parameter during an operating day are within the range established in this Part 70 operating permit, the owner or operator may record that all values were within the range rather than calculating and recording a daily average for that operating day.
	vii.) Hourly records of whether the flow indicator specified under §63.114(d)(1) of Subpart G was operating and whether flow was detected at any time under the hour, as well as records of the times and durations of all periods when the vent stream is diverted from the control device or the monitor is not operating.
	viii.) Where a seal mechanism is used to comply with §63.114(d)(2) of subpart G, hourly records of flow are not required. In such cases, the owner or operator shall record that the monthly visual inspection of the seals or closure mechanism has been done, and shall record the duration of all periods when the seal mechanism is broken, the bypass line valve position has changed, or the key for a lock and key type lock has been checked out, and records of any car seal that has broken.

Condition	Conditions					
Number						
	Each owner or operator who elects to comply with the requirements of §63.113 of this subpart shall submit to the Administrator Periodic Reports semi-annually no later than 60 calendar days after the end of each 6-month period of the following recorded information according to the schedule in §63.152 of this subpart:					
	i. Reports of daily average values of monitored parameters for all operating days when the daily average values recorded under paragraphs (a) and (b) of this section were outside the ranges established in this Part 70 operating permit.					
6.B.16	ii. For Group 1 points, reports of the duration of periods when monitoring data is not collected for each excursion caused by insufficient monitoring data as defined in §63.152(c)(2)(ii)(A) of subpart G.					
	Reports of the times and durations of all periods recorded under paragraph (a)(3) of §63.118 when the vent stream is diverted from the control device through a bypass line.					
	iv. Reports of all periods recorded under paragraph (a)(4) of §63.118 in which the seal mechanism is broken, the bypass line valve position has changed, or the key to unlock the bypass line valve was checked out					
	For 603 A &B, CM-608 A & B, DM-797 A/B, CM-705A, B & C, CM-722, and CM-701 A-E, the owner/operator shall continue to operate and maintain pressure drop gauge(s) on each module of the baghouse(s). Pressure drop readings shall be recorded daily during source operation.					
6.B.17	Operational ranges for the monitored parameters have been established to provide a reasonable assurance of compliance. These operational ranges for the monitored parameters were derived from stack test data, vendor certification, and/or operational history and visual inspections, which demonstrate the proper operation of the equipment in compliance. The facility shall maintain previously established operational ranges for these monitored parameters. The operating ranges may be updated using this procedure, following submittal to the Bureau.					
	For DT-500, the owner/operator shall continue to operate, and maintain liquid flow meters on each scrubber module. Each parameter shall be recorded daily during source operation.					
6.B.18	Operational ranges for the monitored parameters have been established to provide a reasonable assurance of compliance. These operational ranges for the monitored parameters were derived from stack test data, vendor certification, and/or operational history and visual inspections, which demonstrate the proper operation of the equipment in compliance. The facility shall maintain the established operational ranges for these monitored parameters. The operating ranges may be updated using this procedure, following submittal to the Bureau.					
	For Condenser BE 645 and CR#2 CRU Evaporator Overhead Condenser (DE 416), the owner/operator shall continue to operate and maintain outlet coolant temperature gauges on each condenser. Each parameter shall be recorded daily during source operation.					
6.B.19	Operational ranges for the monitored parameters have been established to provide a reasonable assurance of compliance. These operational ranges for the monitored parameters were derived from stack test data, vendor certification, and/or operational history and visual inspections, which demonstrate the proper operation of the equipment in compliance. The facility shall maintain the established operational ranges for these monitored parameters. The operating ranges may be updated using this procedure, following Bureau approval.					

Condition Number	Conditions						
	To meet the requirements of 40 CFR 64 the owner/operator shall install, operate and maintain indicators shown below as the measurement approach: Control Applicable Indicator Monitoring & Range Excursion QA/QC Device Requirement and Reporting Practices						
	(Emission Unit) CR#1 Low Pressure Absorber (BT-603)	SC Re. 61- 62.1, Sec II (H) (1825 TPY VOC) BACT LIMIT	Indicator Location Scrubbing fluid flow rate and absorber top temperature will be monitored with flow meter and thermocouple	Monitored continuously and recorded at least once per 15-minutes. A daily average will be calculated from all valid 15-minute monitoring periods and recorded.	> 3.5 gal/min (liquid flow) ≤ 125°F (top temperature)	Occurs when the daily average for the parameter is outside the approved monitoring range or when the number of valid monitoring periods for the parameter is less than 75% of the number of process operating	Preventative Maintenance including calibration once every three years
6.B.20	CR#1 Intermediate Storage Silo Scrubber (BT-501)	SC Reg. 61- 62.1, Sec. II (H) (2.16 lbs/hr of PM)	Liquid top and bottom flow rates will monitored with flow meters	Monitored continuously and recorded at least once per 15-minutes. A daily average will be calculated from all valid 15-minute monitoring periods and recorded.	Single Transfer > 18 gallons per minute (top water spray) > 120 gallons per minute (bottom water spray) Double Transfer > 90 gallons per minute (top water spray) > 95 gallons per minute (bottom water spray)	periods in a day. Occurs when the daily average for the parameter is outside the approved monitoring range or when the number of valid monitoring periods for the parameter is less than 75% of the number of process operating periods in a day.	Preventative Maintenance including calibration once every three years
	personnel a These oper	and Departme	nt personnel es for the m	shall be readily acc (i.e. on ground lev nonitored paramete the equipment in co	rel or easily ac	cessible roof level).

Condition Number	Conditions							
Number		To meet the requirements of 40 CFR 64 the owner/operator shall install, operate and maintain the indicators shown below as the measurement approach:						
	Control Device (Emission	Applicable Requirement	Indicator and Indicator Location	Monitoring & Reporting Frequency	Range	Excursion	QA/QC Practices	
	Unit 03) High Pressure Vent Gas Treatment System CR#1 (non-HON source)	SC Reg. 61-62.1 Section II (H) CO limit of 1452 lbs/hr and 375 TPY BACT limits	Inlet T and delta T across the catalytic oxidizer will be monitored with thermo- couples	Monitored continuously and recorded at least once per 15-minutes. A daily average will be calculated from all valid 15-minute monitoring periods and recorded.	Inlet temperature and Delta Temperature ¹	Occurs when the daily average for the parameter is outside the approved monitoring range or when the number of valid monitoring periods for the parameter is less than 75% of the number of process operating periods in a day.	Preventative Maintenance including calibration once every three years	
	CR#1 Crystallize r Vent Scrubber (CM-301)	SC Reg. 61- 62.1 Standard No. 4 (56.05 lbs/hr of PM for Emission Units 03-04)	Scrubber pressure will be monitored	Monitor at least once per day	<0.5 inches of water	Occurs when the parameter is outside the approved monitoring range	Preventative Maintenance including calibration once every three years	
6.B.21	High Pressure Vent Gas Treatment System CR#1 (non-HON source)	SC Reg. 61-62.1 Section II (H) 1825—TPY of VOC for Emission Units 03-06 & HPVGTS VOC limit of 85—lbs/hr and 80-TPY BACT Limits	Inlet T and delta T across the catalytic oxidizer will be monitored with thermo- couples	Monitored continuously and recorded at least once per 15-minutes. A daily average will be calculated from all valid 15-minute monitoring periods and recorded.	Inlet temperature and Delta Temperature ¹	Occurs when the daily average for the parameter is outside the approved monitoring range or when the number of valid monitoring periods for the parameter is less than 75% of the number of process operating periods in a day.	Preventative Maintenance including calibration once every three years	
	contempor catalyst, ar	aneous sourc	e test data.	erated within the Source testing sl onth period thereafte	hall be requir	red upon installation	on of a new	
	reports mu	st include ap	propriate inf	not apply during t formation regarding s information will r	g testing to ju	istify temperature a		
	shall be us	ed to determin	ne the accept	therwise comprom able temperature ra ith the testing frequ	inge. A new s	source test shall be		
				nts shall be readil (i.e. on ground lev				
				nonitored parameter the equipment in co		red from stack test	data, which	

Condition Number	Conditions									
		To meet the requirements of 40 CFR 64 the owner/operator shall install, operate and maintain the indicators shown below as the measurement approach:								
	Control Device (Emission Unit)	Applicable Requirement	Indicator and Indicator Location	Monitoring & Reporting Frequency	Range	Excursion	QA/QC Practices			
	CR#2 Low Pressure Absorber (DT-302)	SC Re. 61-62.1, Sec II (H) (1825 TPY VOC for Emission Units 03-06) BACT Limit	Scrubbing fluid flow top and bottom will be monitored with flow meters.	The top and bottom fluid flows will be monitored continuously and recorded at least once per 15-minutes. A daily average will be calculated from all valid 15-minute monitoring periods and recorded.	> 1 gpm (top water reflux) > 23 gpm (bottom acid reflux)	Occurs when the daily average for the parameter is outside the approved monitoring range or when the number of valid monitoring periods for the parameter is less than 75% of the number of process operating periods in a day.	Preventative Maintenance including calibration once every three years			
6.B.22	High Pressure Vent Gas Treatment System CR#2	SC Reg. 61- 62.1 Section II (H) 1825 TPY of VOC for Emission Units 03-06	Inlet T and delta T across the catalytic oxidizer will be monitored with thermocouples Presumptive CAM monitoring (HON)	Monitored continuously and recorded at least once per 15-minutes. A daily average will be calculated from all valid 15-minute monitoring periods and recorded. Presumptive CAM monitoring (HON)	Inlet temperature and Delta Temperature Presumptive CAM monitoring (HON)	Occurs when the daily average for the parameter is outside the approved monitoring range or when the number of valid monitoring periods for the parameter is less than 75% of the number of process operating periods in a day Presumptive CAM monitoring (HON)	Preventative Maintenance including calibration once every three yearsPresum ptive CAM monitoring (HON)			
				nts shall be readil (i.e. on ground lev						
				nonitored parameter the equipment in co		ved from stack test	data, which			

Condition Number	Conditions								
		To meet the requirements of 40 CFR 64 the owner/operator shall install, operate and maintain the indicators shown below as the measurement approach:							
	Control Device (Emission Unit)	Applicable Requirement	Indicator and Indicator Location	Monitoring & Reporting Frequency	Range	Excursion	QA/QC Practices		
	CR#2 Crystallize r Vent Scrubber (DM- 601/DE- 601)	SC Reg. 61- 62.5 Standard No. 4 (53.67 lbs/hr of PM for Emission Units 05-06)	Scrubber fluid flow rate will be monitored with a flow meter.	The fluid flow rates will be monitored continuously and recorded at least once per 15-minutes. A daily average will be calculated from all valid 15-minute monitoring periods and recorded.	> 180 gallons per minute	Occurs when the daily monitoring parameter is outside the approved monitoring range or when no valid monitoring value is recorded for either parameter when either A or B has been in operation for at least four hours that day.	Preventative Maintenance including calibration once every three years		
6.B.23	S & L Shipping Storage Silo Bag- houses (CM-720 A/B-F Silo))	SC Reg. 61-62.5 Standard No. 4 (56.25 lbs/hr of PM for Emission Unit 07	Pressure drop will be monitored with a differential pressure gauge on each baghouse	The pressure drop will be monitored continuously and recorded at least once per 15-minutes. A daily average will be calculated from all valid 15-minute monitoring periods and recorded.	0.2-10 in of water	Occurs when the daily average for the parameter is outside the approved monitoring range or when the number of valid monitoring periods for the parameter is less than 75% of the number of process operating periods in a day.	Preventative Maintenance including calibration once every three years		
	personnel a	and Departme	nt personnel	(i.e. on ground lev	el or easily ac	for verification lecessible roof level)			
				ionitored parameter the equipment in co		ved from stack test	data, which		

Condition Number			Conditions				
	Per 40 CFR 64, an excursion is defined as any operating condition where the indicator is outside of the approved range. Upon detecting an excursion, the owner or operator shall restore operation of the pollutant-specific emissions unit (including the control device and associated capture system) to its normal or usual manner of operation as expeditiously as practicable in accordance with good air pollution control practices for minimizing emissions. The response shall include minimizing any startup, shutdown or malfunction period and taking any necessary corrective actions to restore normal operation and prevent the likely recurrence of the cause of an excursion (other than those caused by excused startup and shutdown conditions). Any alternative method for monitoring control device performance must be preapproved by the Bureau and shall be incorporated into the permit as set forth in SC Regulation 61-62.70.7.						
(D 24	A semiannual report for monitoring shall include, at a minimum, the information required under § 70.6(a)(3)(iii) and the following information as applicable:						
6.B.24	 Summary information of the number, duration and cause (including unknown cause, if applicable) of excursions, as applicable, and the corrective actions taken; Summary information on the number, duration and cause (including unknown cause, if applicable) for monitor downtime incidents (other than downtime associated with zero span or other daily calibration checks, if applicable); If applicable, a description of the actions taken to implement a Quality Improvement Plan (QIP) during the reporting period as specified in §64.8. Upon completion of a QIP, the owner or operator shall include in the next summary report documentation that the implementation of the plan has been completed and reduced the likelihood of similar levels of excursions occurring. 						
	The owner or operator shall maintain records of monitoring data, monitor performance data, corrective action, and quality improvement plans. Records shall be maintained on site for a period of at least five (5) years from the date generated and shall be made available to Department personnel upon request.						
	The following source	s shall be stack tested	l at least every other ye	ear 36 months per the table below:			
	Emission Unit	Source	Pollutant	Testing Frequency			
	03	HPVGTS	VOC, CO	Once every 24-36 months			
6 D 25	03	LPA	VOC, CO	Once every 24-36 months			
6.B.25	03 05	DHT Scrubber HPVGTS	VOC, CO VOC	Once every 24 months Once every 2436 months			
	may be present. So	The Bureau must be notified at least two weeks prior to a source test so that a Bureau representative may be present. Source test methodology, to include testing at worst-case conditions, must be approved by the Bureau and comply with SC DHEC Regulation 61-62.1, Section IV-Source Testing.					

Condition Number	Conditions					
Number	To assure compliance with the VOC emission limitation, the permittee shall comply with the following requirements: a. Based on the daily production rates, process data (i.e., organic recording device), source test data, and the operation of all recovery and control equipment, the permittee shall calculate and record within fifteen days following a quarter basis the monthly emissions of VOCs and a twelve month rolling sum. The twelve month rolling sum shall not exceed 1825 TPV. The calculated values shall include					
6.B.26	the sum of VOC emissions from all uncontrolled and controlled fugitive (i.e. equipment leaks) and point sources plus uncontrolled VOC emission emitted during periods when performing maintenance on any control device. b. When bypassing any control device during periods of malfunctions, the permittee shall comply with permit condition 4 P.6 of this Part 70 energities permit. If					
	repetitive circumstances or causes of malfunctions are detected, a plan for improving the operations and maintenance of the control device shall be submitted to the Manager of the Technical Management Section, Bureau of Air Quality to address such causes.					
	c. The VOC calculated total shall be submitted on a semi-annual basis. The permittee shall comply with the following requirements:					
	a. The combustion sources included in Condition 6.B.31–28 are permitted to burn only #2 virgin fuel oil as a fuel. The sulfur content of the fuel oil burned in each combustion source shall be limited as shown in Condition 6.B.3128. The use of any other substances as fuel is prohibited without prior written approval from the Bureau of Air Quality. Fuel oil analysis (i.e. supplier certification sheet) shall be obtained for each batch of oil received and stored on site. The supplier certification shall be maintained on-site for five years.					
6.B.27	 b. The operating time of each combustion source shall be limited as shown in Condition 6.B.28 on a twelve-month rolling sum. Per combustion source, the permittee for each month must record the actual operating hour meter reading and the calculated twelve-month rolling sum. The records of actual operating hours shall be maintained on-site for a period of at least five (5) years. 					
	c. In regards to compressors L-1 and L-2, the total rated capacity of two or less diesel powered compressors shall be less than or equal to 5.98 million Btu/hr (2350 HP). The permittee shall maintain appropriate records which demonstrates compliance with this condition. These records shall include, but are not limited to, a copy of the manufacturer's information indicating the rated capacity of each compressor. These records shall be maintained on site for a period of at least five (5) years and shall be made available to a Department representative upon request. The permittee shall notify by phone the local EQC District Office at least a day before replacing and/or adding a compressor. A follow-up letter shall be mailed to the Bureau of Air Quality and the local EQC District Office postmarked at least 2 days after replacing and/or adding a compressor indicating the actual date of installation, the rated capacity of each compressor on site, and the total associated emissions of each criteria pollutant in terms of lbs/hr.					
	BP will prepare a semiannual report to summarize the fuel sulfur content and the hours of operation of the emergency generators, compressors, and pumps per Condition 6.B.3128.					

Condition Number	Conditions							
	pumps in Em	The operating hours and percent sulfur contents for the fuel- for the generators, compressors and pumps in Emission Unit 11 and the IAG Informational EU shall be limited as follows:						
	Equip ID	Combustion Source	No. 2 fuel oil Percent Sulfur	Hrs/yr (non-emergency operation)				
	AM-804	Emergency Generator #1	<0.3%15 ppm	No limits 100				
	AC-402	Emergency Compressor #1	<u>15 ppm</u> < 0.3%	100No limits				
	AG-202B	Emergency Fire Water Pump	<u>15 ppm</u> < 0.3%	100No limits				
	AG-229	T-Head FW Pump	<u>15 ppm</u> <0.3%	100No limits				
	AG-202C	Emergency Fire Water Pump	<0.05%	<250				
	AG-202D	Emergency Fire Water Pump	<0.05%	<250				
	BM-1201	Emergency Generator #2 (CR#1)	<u>15 ppm</u> <0.3%	<u>100</u> < 250				
	DM-135	Emergency Generator #3 (CR#2)	<u>15 ppm</u> < 0.05%	<500				
6.B.28	AC-404	Emergency Air Compressor #2 (Utility)	<u>15 ppm</u> < 0.05%	<1,000 <u><500</u>				
0.2.20	AM-838	IT Emergency Generator	<u>15 ppm</u> < 0.5%	<500				
	L-1 and L-2	(Leased) Compressors #1 and #2	<u>15 ppm</u> <0.05%	8760*				
	<u>AM-819</u>	Administration Building Emergency Generator	<u>15 ppm</u>	<u>100</u>				
	<u>AM-840</u>	PX Pump Emergency Generator	<u>15 ppm</u>	<u>100</u>				
	<u>AM-846</u>	Main Gate Emergency Generator	<u>15 ppm</u>	<u>100</u>				
	<u>AM-847</u>	Contractor Gate Emergency Generator	<u>15 ppm</u>	<u>100</u>				
	<u>AM-848</u>	T-Head Emergency Generator	<u>15 ppm</u>	100				
	AM-849	WWT Control Room Emergency Generator	<u>15 ppm</u>	<u>100</u>				
	Total for both compressors							
	Fuel oil analysis (i.e. supplier certification sheet) shall be obtained for each batch of oil received and stored on site. A seminannual report shall be prepared to summarize the fuel sulfur content and the hours of operation.							
6.B.29	Emission Unit No. 12 Each owner or operator of a Group 1 or Group 2 storage vessel shall keep readily accessible records showing the dimensions of a the storage vessel and an analysis showing the capacity of the storage vessel. This record shall be kept as long as the storage vessel retains Group 1 or Group 2 status and is in operation. For each Group 2 storage vessel, the owner or operator is not required to comply with any other provisions of §§63.119 through 63.123 of Subpart G other than those required by this paragraph unless such vessel is part of an emissions average as described in §63.150 of Subpart G.							
6.B.30	HON wastev must be kep	vater generated is all Group 2 wastewater. t available for inspection. If the status fication and capture/destruction system w	Records of the Gro of the wastewater	oup 2 status determinations changes to Group 1, the				

Condition Number	Conditions			
	Emission Units 03-06, 12 The owner /operator of these units is subject to 40 CFR 63 Subpart H, National Emiss Standards for Organic Hazardous Air Pollutants for Equipment Leaks. In accordance w 40 CFR 63, Subparts A & H, the owner /operator shall comply with the requirements of applicable provisions of these subparts. The table below lists equipment categories sub to the provisions of this subpart and the method used to show compliance. All VOC will considered as a HAP for purposes of determining the components requiring a monitor program.			
	Emissio Unit	Equipment/Components	Method of Compliance from 40 CFR 63, Subpart H Provisions	
6.B.31		Valves in Gas Vapor or Light Liquid Service	§63.168(b), §63.168(f)	
	#1 Ox	Connectors/ Flanges in Light Liquid Service	§63.174(a), §63.174(d)	
	#1 OX	Pumps in Light Liquid Service	§63.163(b), §63.163(c)	
	#2 Ox OSBL	Agitators	§63.173(a), §63.173(b), §63.173(c)	
		Relief Valves	§63.169	
		Valves in Gas Vapor or Light Liquid Service	§63.168(b), §63.168(f)	
		Connectors/ Flanges in Light Liquid Service	§63.174(a), §63.174(d)	
		Pumps in Light Liquid Service	§63.163(b), §63.163(c)	
		Agitators	§63.173(a), §63.173(b), §63.173(c)	
		Relief Valves	§63.169	
		Valves	§63.168(b), §63.168(f)	
		Connectors/ Flanges	§63.174(a), §63.174(d)	
		Pumps in Light Liquid Service	§63.163(b), §63.163(c)	
		Relief Valves	§63.169	

Condition Number	Conditions			
	Emission Units 03-06, 12 Pumps in Light Liquid Service Each pump shall be checked by visual inspection each calendar week for indicators of liquids dripping from the pump seal. If there are indications of liquids dripping from the pump seal, a leak is detected.			
	A first attempt at repair shall be made no later than 5 calendar days after the detected. First attempts at repair include, but are not limited to, the following pr where practicable:			
	i. Tightening of the packing gland nuts.			
	ii. Ensuring that the seal flush is operated at design pressure and temperature. Valves in gas/vapor service and in light liquid service			
	When a leak is detected, it shall be repaired as soon as practicable, but no later than 15 calendar days after the leak is detected, except as provided in §63.171.			
	A first attempt to repair shall be made no later than 5 calendar days after each leak is detected. When a leak has been repaired, the valve shall be monitored at least once within the first 3 months after its repair. The monitoring shall be conducted as specified in §63.180b and c as appropriate to determine whether the valve has resumed leaking.			
	Pumps, valves, connectors, and agitators in heavy liquid service; instrumentation systems and pressure relief devices in liquid service			
6.B.32	a. Pumps, valves, connectors, and agitators in heavy liquid service, pressure relief devices in light liquid or heavy liquid service, and instrumentation systems shall be monitored within 5 calendar days by the method specified in §63.180(b) if any evidence of a potential leak to the atmosphere is found by visual, audible, olfactory, or any other detection method. If such a potential leak is repaired as required in paragraphs (c) and (d) of this section, it is not necessary to monitor the system for leaks by the method specified in §63.180(b).			
	b. If an instrument reading of 10,000 parts per million or greater for agitators, 5,000 parts per million or greater for pumps handling polymerizing monomers, 2,000 parts per million or greater for pumps in food/medical service or pumps subject to §63.163(b)(iii)(C), or 500 parts per million or greater for valves, connectors, instrumentation systems, and pressure relief devices is measured, a leak is detected.			
	c. When a leak is detected, it shall be repaired as soon as practicable, but not later than 15 calendar days after it is detected, except as provided in §63.171. The first attempt at repair shall be made no later than 5 calendar days after each leak is detected.			
	For equipment identified in paragraph (a) of this section that is not monitored by the method specified in §63.180(b), repaired shall mean that the visual, audible, olfactory, or other indications of a leak to the atmosphere have been eliminated; that no bubbles are observed at potential leak sites during a leak check using soap solution; or that the system will hold a test pressure.			
	d. First attempts at repair include, but are not limited to, the practices described under §§63.163(c)(2) and 63.168(g), for pumps and valves, respectively <i>Non-Confidential</i>			

Condition Number	Conditions			
	Emission Unit 05-06 The owner /operator of these units is subject to 40 CFR-60 Subpart VV, Standards of Performance for Equipment Leaks of VOC in the Synthetic Organic Chemicals Manufacturing Industry. In accordance with 40 CFR-60, Subparts A & VV, the owner /operator shall comply with the requirements of all applicable provisions of these subparts. The table below lists equipment categories subject to the provisions of this subpart and the method used to show compliance.			
6.B.33	Emission Unit Equipment/Components Valves Connectors/ Flanges Pumps in Light Liquid Service Agitators Relief Valves (gas/vapor) Relief Valves (Liquid) Compressors			
	Per 40 CFR 60. 487(c) All semiannual reports to the Administrator shall include the following information, summarized from the information in §60.486: (e)(1) Process unit identification. (e)(2) For each month during the semiannual reporting period, (e)(2)(i) Number of valves for which leaks were detected as described in §60.482(7)(b) or \$60.483.2			
	(c)(2)(ii) Number of valves for which leaks were not repaired as required in §60.482-7(d)(1), (c)(2)(iii) Number of pumps for which leaks were detected as described in §60.482-2(b) and (d)(6)(i),			
	(c)(2)(iv) Number of pumps for which leaks were not repaired as required in §60.482-2(c)(1) and (d)(6)(ii), (c)(2)(v) Number of compressors for which leaks were detected as described in §60.482-3(f),			
	(c)(2)(vi) Number of compressors for which leaks were not repaired as required in §60.482-3(g)(1), and (c)(2)(vii) The facts that explain each delay of repair and, where appropriate, why a process unit shutdown was technically infeasible. Non-Confidential			
	(c)(3) Dates of process unit shutdowns which occurred within the semiannual reporting			

Condition Number	Conditions		
6.B.34	Emission Units 01-14 Per Standard 5.1, the permittee shall review all new, modified, or altered sources to determine if they would increase net Volatile Organic Compounds (VOC) emissions by more than 100 tpy. If they would increase net Volatile Organic Compounds (VOC) emissions by more than 100 tpy. If they would increase net Volatile Organic Compounds (VOC) emissions by more than 100 tpy. If they applied to construction or modifications permitted before June 25, 2004. Best Available Control Technology shall be applied to any new construction permit issued on or after June 25, 2004, when the net VOC emissions increase exceeds 100 tpy. To assure non exceedance of the LAER net increase above 2831 TPY, as defined by SC Regulation 62.5, Standard No. 5.1, the permittee shall use the information required under this Part 70 operating permit, and other applicable information (e.g., emission factors) to calculate and record the actual VOC emissions from the facility on a monthly basis. The emission calculations shall include emissions from, but not be limited to, fugitive sources, process vents, equipment leaks, transfer racks (unloading and loading operations), storage tanks working, filling and breathing losses, combustion sources, and wastewater collection and treatment equipment. Reports including a summary of all recorded parameter values used in the calculations and calculated values shall be submitted to the Manager of the Technical Management Section, Bureau of Air Quality postmarked no later than 30 calendar days after the end of the reporting period. Record keeping and reporting periods shall be as follows: a. For actual emissions greater than 50 tons/year but less than 75 tons/year of net increase above 2831 TPY as defined by SC Regulation 62.5, Standard No. 5.1, the reporting shall be on an annual basis. b. For actual emissions greater than 50 tons/year but less than 50 tons/year of net increase above 2831 TPY as defined by SC Regulation 62.5, Standard No. 5.1, the reporting shall be on an annual basis.		
6.B.35	Emission Units 03-06 The Department shall waive the periodic particulate matter testing requirements per SC Regulation 61-62.5, Std. 3, Section VIII and the Operator training requirements per SC Regulation 61-62.5, Std. 3, Section IX.		

Condition Number	Conditions			
	Boilers AB-350 A/B (Boiler Nos. 3 and 4 respectively) combined are each_permitted to burn 18,675,0002,400,000 gallons per year of VLSD fuel oil. The owner/operator must record fuel oil consumption daily and calculate yearly fuel oil consumption on a twelve-month rolling sum. Fuel oil sulfur content shall be less than or equal to 0.5 percent by weight. Acceptable fuel oil certification can be ensured by following Department guidance entitled "Guidance For Fuel Oil Certifications" issued on May 19, 2000 and any subsequent revisions. Fuel oil supplier certification shall be obtained for each batch of oil received and stored on site. Records of fuel oil consumption and fuel oil certification shall be maintained on site for a period of at least five (5) years from the date generated and shall be made available to a Department representative upon request.			
6.B.36	To assure compliance with SC Regulation 61-62.1 Sec II(H) for the 2005 project adding the new boilers, the permittee shall monitor and record the following information: 1. The daily VLSD fuel oil consumption and calculate the rolling twelve month sum 2. The daily natural gas consumption 3. The daily used oil consumption and calculate the rolling twelve month sum 4.3. The daily biogas consumption and calculate the rolling twelve month sum 5.4. VLSD fuel oil sulfur content shall be ≤ 0.5%. The Fuel oil supplier certification shall be obtained for each batch of oil received and stored on site. The above information shall be included in the semi-annual reports. Semiannual reports including fuel oil certification, fuel oil consumption, and all recorded parameters and calculated values shall be submitted to the Manager of the Technical Management Section,			
6.B.37	Bureau of Air Quality postmarked no later than 30 calendar days after the end of the reporting period. The owner/operator shall calculate SO ₂ , NO _x , CO, PM, PM ₁₀ and VOC emissions from Boilers AB-350A/B on a twelve-month rolling sum. The calculations shall include—sulfur content, fuel consumption and Bureau approved emission factors from stack test data, where available. SO ₂ , NO _x , CO, PM, and PM ₁₀ , emissions are listed in Section II A, "Emission Limitations" of this construction permit. The twelve month rolling sum will be included in the semiannual report.			
6.B.38	Source tests for PM, PM ₁₀ , and SO ₂ on Boilers AB 350A/B will be required. The tests shall be performed within 60 days after achieving maximum production but not later than 180 days after initial start up. The Bureau must be notified at least two weeks prior to a source test so that a Bureau representative may be present. Source test methodology, to include testing at worst case conditions, must be approved by the Bureau and comply with SC DHEC Regulation 61-62.1, Section IV-Source Testing. Source testing for PM and PM ₁₀ on Boilers AB 350A/B will be required on a biennial basis after the initial source test. An initial source test will be required for SO ₂ . RATA testing for the NOx and CO CEM systems will be conducted annually. The Continuous Opacity monitor requires an initial certification per 40 CFR 60 Subpart Db.			

Condition Number	Conditions			
6.B.39	Emission Unit 15-16 (Boilers AB-350 A/B) Per §60.48b(a), the owner or operator of an affected facility subject to the opacity standard under §60.43b shall install, calibrate, maintain, and operate a continuous monitoring system for measuring the opacity (COMs) of emissions discharged to the atmosphere and record the output of the system. However under 60.13(i)(2), if #2 fuel oil is used "infrequently", then an alternative monitoring plan can be approved as specified. The permittee will submit a request for an alternative monitoring plan. Logs shall be kept to record all periods of excess emissions, periods when 6 minute opacity exceeds the opacity standard, including cause, corrective action taken and preventative actions adopted. The logs shall be maintained for a period of five (5) years and be made available to the Department upon request. The owner/operator shall submit semiannual excess emissions reports within 30 days after the end of the monitoring period. The permittee will provide a COMs on the AB 350 A/B boilers and will not be required to do any			
6.B.40	Per §60.48b(b), the owner or operator of an affected facility subject to the NOx standard under §60.44b shall install, calibrate, maintain, and operate a continuous monitoring system for measuring the NOx (CEMs) emissions discharged to the atmosphere and record the output of the system.			
6.B.41	Per §40.46b(e)(1), for the initial compliance test, nitrogen oxides from the steam generating unit ar monitored for 30 successive steam generating unit operating days and the 30-day average emission rates used to determine compliance with the nitrogen oxides emissions standards under §60.44b. The 30-day average emission rate is calculated as the average of all hourly emissions data recorder by the monitoring system during the 30-day test period.			
6.B.42	§60.48 states that if the owner or operator has installed a nitrogen oxides emission rate continuous emission monitoring system (CEMS) to meet the requirements of 40 CFR 75 and will continue to meet the ongoing requirements of part 75, that CEMS may be used to meet the requirements of §60.48b, except the permittee shall meet the requirements of §60.49b. S.C. Regulation 61-96.70 states that owners and operators shall comply with the monitoring and reporting requirements as provided in Subpart H Monitoring and Reporting of the NOx Budget Trading Program and in Subpart H of 40 CFR part 75. Data reported to meet the requirements of §60.49b shall not include data substituted using the missing data procedures in subpart D of part 75, nor shall the data have bias adjusted according to the procedures of part 75. The permittee has stated in the permit application that it will operate CEMS in accordance with the Part 75 provisions to measure NO _x emissions discharged from the proposed boilers. RATA testing for the NOx CEM system will be conducted annually.			
6.B.43	Per §60.48b(c), the continuous monitoring required shall be operated and data recorded during all period of operation of the affected facility except for continuous monitoring system breakdowns and repairs. Data shall be recorded during calibration checks, and zero and span adjustments.			
6.B.44	Per §60.48b(e), the procedures under §60.13 shall be followed for installation, evaluation, and operation of the continuous monitoring systems.			
6.B.45	For SO ₂ , the permittee has elected to maintain records to demonstrate that the affected facility combusts only VLSD oil under §60.42b(j)(2). The permittee shall obtain and maintain at the affected facility fuel receipts from the fuel supplier which certify that the oil meets the definition of distillate oil as defined in §60.41b. Reports shall be submitted semiannually certifying that only VLSD oil meeting this definition was combusted in the affected facility during the reporting period.			
6.B.46	Reports for units subject to 40 CFR 60 Subpart Db shall be submitted in accordance with §60.49b Reporting And Recordkeeping Requirements. As stated in §60.49b, the permittee must submit reports on a semiannual basis. The semiannual reports shall be submitted to the Manager of the Technical Management Section, Bureau of Air Quality postmarked no later than 30 days after the end of the reporting period. The reports may be included in the Title V semi-annual reports.			

Condition Number	Conditions
6.B.47	To demonstrate initial compliance for PM and HCl for 40 CFR 63 Subpart DDDDD, the permittee must include a signed statement in the NOCS report required in §63.7545(e) that indicates the facility burns only liquid fossil fuels other than residual oils, either alone or in combination with gaseous fuels. To demonstrate continuous compliance with the applicable PM and HCl emission limits, the permittee must also keep records that demonstrate that the facility burns only liquid fossil fuels other than residual oils, either alone or in combination with gaseous fuels. For each boiler or process heater subject to an emission limit, the permittee must also keep the records in paragraphs(d)(1) through (5), where applicable of §63.7555.
	Section 1 of §63.7555states that the permittee must keep records of monthly fuel use by each boiler or process heater, including the type(s) of fuel and amount(s) used.
6.B.48	§63.7550 that indicates that the facility burned only liquid fossil fuels other than residual oils, either alone or in combination with gaseous fuels.
6.B.49	Since the facility has an applicable work practice standard for CO and boilers that will be in the large liquid fuel subcategory, a CEMS for CO must be installed, operated, and maintained according to the procedures in paragraphs (a)(1) through (6) of \$63.7525 by the compliance date specified in \$63.7495. (1) Each CEMS must be installed, operated, and maintained according to Performance Specification (PS) 4A of 40 CFR part 60, appendix B, and according to the site specific monitoring plan developed according to \$63.7505(d). (2) The owner/operator must conduct a performance evaluation of each CEMS according to the requirements in \$63.8 and according to PS 4A of 40 CFR part 60, appendix B. (3) Each CEMS must complete a minimum of one cycle of operation (sampling, analyzing, and data recording) for each successive 15 minute period. (4) The CEMS data must be reduced as specified in \$63.8(g)(2). (5) The owner/operator must calculate and record a 30 day rolling average emission rate on a daily basis. A new 30 day rolling average emission rate is calculated as the average of all of the hourly CO emission data for the preceding 30 operating days. (6) For purposes of calculating data averages, the owner/operator must not use data recorded during periods of monitoring malfunctions, associated repairs, out of control periods, required quality assurance or control activities, or when the boiler or process heater is operating at less than 50 percent of its rated capacity. The owner/operator must use all the data collected during all other periods in assessing compliance. Logs shall be kept to record all periods of deviation/excess emissions, periods when CEM value averaged over appropriate period exceeds the standard, including cause, corrective action taken and preventative actions adopted. The logs shall be maintained for a period of two (2) years and be made available to the Department upon request. The owner/operator shall submit semiannual deviation/excess emissions reports within 30 days after the end of the mo
	Any period for which the monitoring system is out of control and data are not available for required calculations constitutes a deviation from the monitoring requirements. Conditions 6.B.47, 6.B.48 and 6.B.49 Voided
6.B.50	Per 40 CFR 63 Subpart DDDDD, the facility will comply with the SSM plan requirements as applicable. 40 CFR 63 Subpart DDDDD As stated in §63.7550, the permittee must submit reports on a semiannual basis according to the requirements in §63.7550(b). The semiannual reports shall be submitted to the Manager of the Technical Management Section, Bureau of Air Quality postmarked no later than 30 days after the end of the reporting period.

Condition Number	Conditions		
6.B.51	Emission Unit 15-16 (Boilers AB-350 A/B) Per S.C. Regulation 61-62.96, Boilers AB-350 A/B will be NO _x Budget units and the permittee to the extent applicable shall comply with the monitoring and reporting requirements as provided in subpart H of SC Regulation 61-62.96 and in subpart H of 40 CFR part 75. The NO _x authorized account representative shall comply with all record keeping and reporting requirements in SC Regulation 61-62.96.74 and with the requirements of SC Regulation 61-62.96.10(e). Quarterly reports, as specified in SC Regulation 61-62.96.74(d), shall be sent to EPA and to SC DHEC Bureau of Air Quality's Technical Management Section at the addresses listed in Section 1 of this permit. Unless otherwise provided, the owners and operators of the NO _x Budget source and each NO _x Budget unit at the source shall keep on site at the source each of the following documents for a period of 5 years from the date the document is created. This period may be extended for cause, at any time prior to the end of 5 years, in writing by the Department or the EPA. (i) The account certificate of representation for the NO _x authorized account representative for the source and each NO _x Budget unit at the source and all documents that demonstrate the truth of the statements in the account certificate of representation, in accordance with Section 96.13; provided that the certificate and documents shall be retained on site at the source beyond such 5-year period until such documents are superseded because of the submission of a new account certificate of representation changing the NO _x authorized account representative. (ii) All emissions monitoring information, in accordance with subpart H of this regulation; provided that to the extent that subpart H of this regulation provides for a 3-year period for record keeping, the 3-year period shall apply. (iii) Copies of all reports, compliance certifications, and other submissions and all records made or required under the NO _x Budget Trading Program. (iv) Copi		
6.B.52	Per S.C. Regulation 61-62.96, the NO _X authorized account representative of each NO _X Budget source required to have a federally enforceable permit and each NO _X Budget unit required to have a federally enforceable permit at the source shall: (i) Submit to the Department a complete NO _X Budget permit application under Section 96.22 in accordance with the deadlines specified in Section 96.21(b) and (c); (ii) Submit in a timely manner any supplemental information that the Department determines is necessary in order to review a NO _X Budget permit application and issue or deny a NO _X Budget permit.		

Condition Number	Conditions		
Number	This source is subject to SC Regulation 61-62.96, Nitrogen Oxides (NO _x) Budget Trading Program, and shall comply with all applicable provisions.		
	The owners and operators, and to the extent applicable, the NO _x authorized account representative of a NO _x Budget unit, shall comply with the monitoring and reporting requirements as provided in subpart H of SC Regulation 61-62.96 and in subpart H of 40 CFR part 75. For purposes of complying with such requirements, the definitions in SC Regulation 61-62.96.2 and in 40 CFR part 72 section 72.2 shall apply, and the terms "affected unit," "designated representative," and "continuous emission monitoring system" (or "CEMS") in 40 CFR part 75 shall be replaced by the terms "NO _x Budget unit," "NO _x authorized account representative," and "continuous emission monitoring system" (or "CEMS"), respectively, as defined in SC Regulation 61-62.96.2.		
6.B.53	The NO _x authorized account representative shall comply with all record keeping and reporting requirements in SC Regulation 61-62.96.74 and with the requirements of SC Regulation 61-62.96.10(e). Quarterly reports, as specified in SC Regulation 61-62.96.74(d), shall be sent to EPA and to SC DHEC, Bureau of Air Quality's Technical Management Section at the addresses listed below.		
	US EPA, Region 4 SC DHEC - BAQ Air Enforcement Branch Technical Management Section 61 Forsyth Street 2600 Bull Street Atlanta, GA 30303 Columbia, SC 29201		
	If the NO _x authorized account representative for a NO _x Budget unit subject to an Acid Rain Emission limitation who signed and certified any submission that is made under subpart F or G of 40 CFR part 75 and which includes data and information required under this subpart or subpart H of 40 CFR part 75 is not the same person as the designated representative or the alternative designated representative for the unit under 40 CFR part 72, the submission must also be signed by the designated representative or the alternative designated representative.		
6.B.54	Unless otherwise provided, the owners and operators of the NO _x Budget source and each NO _x Budget unit at the source shall keep on site at the source each of the following documents for a period of 5 years from the date the document is created. This period may be extended for cause, at any time prior to the end of 5 years, in writing by the Department or the EPA. (i) The account certificate of representation for the NO _x authorized account representative for the source and each NO _x Budget unit at the source and all documents that demonstrate the truth of the statements in the account certificate of representation, in accordance with Section 96.13; provided that the certificate and documents shall be retained on site at the source beyond such 5-year period until such documents are superseded because of the submission of a new account certificate of representation changing the NO _x authorized account representative. (ii) All emissions monitoring information, in accordance with subpart H of this regulation; provided that to the extent that subpart H of this regulation provides for a 3-year period for record keeping, the 3-year period shall apply. (iii) Copies of all reports, compliance certifications, and other submissions and all records made or required under the NO _x Budget Trading Program. (iv) Copies of all documents used to complete a NO _x Budget permit application and other submission under the NO _x Budget Trading Program or to demonstrate		
	compliance with the requirements of the NO _x Budget Trading Program.		

Condition Number	Conditions			
6.B.55	This facility shall be allowed to operate temporary units such as generators, compressors, and other diesel-driven portable units for emergency, overhaul, maintenance, or similar activities that will have a duration of six months or less. These units shall be equipped with hour meter indicators or other method for recording actual hours of use. Emissions from the use of such equipment must be added to the facility wide totals, if applicable. The owner/operator shall, record for each unit: 1) the size of unit, 2) the date the unit brought on site, 3) the date of first use, 4) the total hours operated, 5) the purpose served by unit, 6) the date unit was removed from site, and 7) the emissions from use. The facility shall not be required to notify the Bureau prior to operating these units. Permanent units, including emergency equipment, shall require prior notification and approval by the Bureau and will be shown in the facility's operating permit as permitted, insignificant, or exempt sources. Units used for peak shaving or load reductions cannot be considered emergency generators.			
6.B.56	Emission Unit 03 The facility shall implement a VOC LDAR (Leak Detection and Repair Program) equivalent to the requirements of 40 CFR 60 Subpart VV (per the regulation as of November 1, 2006) and submit to the Department before placing construction permit 0420 0029 CR into operation. The use of the LDAR program was voluntarily used for the purpose of a PSD offset. The owner/operator of these units shall comply with 40 CFR 60 Subpart VV (per regulation as of November 1, 2006), Standards of Performance for Equipment Leaks of VOC in the Synthetic Organic Chemicals Manufacturing Industry. In accordance with 40 CFR 60, Subparts A & VV, the owner /operator shall comply with the requirements of all applicable provisions of these subparts. The table below lists equipment categories subject to the provisions of this subpart and the method used to show compliance.			
	Emission Unit Equipment/Components CFR 60, Subpart VV Provisions			
	Valves Connectors/ Flanges Pumps in Light Liquid Service #1 Ox Agitators Relief Valves (gas/vapor) Relief Valves (Liquid) Compressors			

ATTACHMENT B

Insignificant Activities

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The following table contains a list of activities which are considered insignificant pursuant to SC Regulation 61-62.70.5(c). Sources listed below are not exempt from any otherwise applicable state or federal requirements including, but not limited to, opacity standards, ambient air quality standards, and air toxic standards.

Equip ID	Source Description	Installation Date/ Modification Date	Basis
IA-5	Facility Maintenance-Process Vessel and Tank Cleaning	N/A	Emissions total < 5 TPY of VOC Emission total < .5 TPY of HAP
IA-6	Facility Maintenance-Purging of Natural Gas Lines	N/A	Emissions total < 5 TPY of VOC Emission total < .5 TPY of HAP
IA-8	Facility Maintenance – General Vehicle Maintenance and Service Activities including but not limited to Railcars	N/A	Emissions total < 5 TPY of VOC Emission total < .5 TPY of HAP
IA-9	Facility Maintenance- Vehicle fueling (diesel & gasoline)	N/A	Emissions total < 5 TPY of VOC Emission total < .5 TPY of HAP
IA-10	Facility Maintenance-Metals machining solvents including cutting oils	N/A	Emissions total < 5 TPY of VOC Emission total < .5 TPY of HAP
IA-11	Facility Maintenance-Grinding activities	N/A	Emissions total < 5 TPY of PM Emission total < .5 TPY of HAP
IA-12	Facility Maintenance-Catalyst change out/unit turnarounds	N/A	Emissions total < 5 TPY of VOC Emission total < 5 TPY of PM Emission total < .5 TPY of HAP
IA-13	Facility Maintenance-Insulation work	N/A	Emission total < 5 TPY of PM
IA-14	Facility Maintenance-Filter change out	N/A	Emissions total < 5 TPY of VOC Emission total < .5 TPY of HAP
IA-19	Wastewater & Stormwater Management- Filter pressing	N/A	Emissions total < 5 TPY of VOC Emission total < .5 TPY of HAP
IA-21	Remediation-Vacuum Truck Operations	N/A	Emissions total < 5 TPY of VOC Emission total < .5 TPY of HAP
IA-23	Remediation-Stockpiled contaminated soils	N/A	Emissions total < 5 TPY of VOC Emission total < .5 TPY of HAP
IA-24	Remediation-Groundwater sampling and level monitoring	N/A	Emissions total < 5 TPY of VOC Emission total < .5 TPY of HAP
IA-25	Remediation-Soil Coring	N/A	Emissions total < 5 TPY of VOC Emission total < .5 TPY of HAP

IA-26 Remediation-Asbestos Abatement N/A Emissions total < 5 TPY of PM Emission total < 5 TPY	Equip ID	Source Description	Installation Date/ Modification Date	Basis
Lime Storage, Spent Lime, and Clay Handling activities N/A Emission stotal < 5 TPY of PM Emissions total < 5 TPY of PM Emission total < 5 TPY of VOC Emission total < 5 TPY of PM Emission to	IA 26	Damadiation Ashastas Abatament	NI/A	Emissions total < 5 TPY of PM
Lime Storage, Spent Lime, and Clay Handling activities N/A Emissions total < 5 TPY of VOC Emission total < 5 TPY of VO	1A-20	Remediation-Aspestos Abatement	IN/A	
Handling activities		Lime Storage Spent Lime and Clay		
LA-44 Fuel Oil and Paraxylene Separators 1977 Emission total < 5 TPY of VOC Emission total < 5 TPY of VOC Emission total < 5 TPY of VAPA	IA-43		N/A	
1974		Č		
1.4.48	IA-44	Fuel Oil and Paraxylene Separators	1977	
IA-48	IA-47			
IA-57				
A-S8		Herbicide and Insecticide Application	NT/A	
AF-1001	IA-5/		N/A	Emission total < .5 TPY of HAP
AF-1001	TA -58			Should not be listed In Title V
AF-1010	171-50			permit since on IA list Section A #5
AP-206A Utilities-<2,000 gallon Cooling Tower Additive Tank Insignificant Activity B.3 AP-206B Utilities-<2,000 gallon Cooling Tower Additive Tank Insignificant Activity B.3 AF-211 Utilities-6300 gallon Water Coagulant Tk Insignificant Activity B.3 AF-306 Utilities-1000 gallon Boiler Water Additive Insignificant Activity B.3 AF-307 Utilities-1000 gallon Boiler Water Additive Insignificant Activity B.3 AF-309 Utilities-1000 gallon Boiler Water Additive Insignificant Activity B.3 AF-313 Utilities-1000 gallon Polymer Additive Insignificant Activity B.3 DF-901 Utilities-1000 gallon Polymer Additive Insignificant Activity B.3 AF-313 Utilities-1000 gallon Polymer Additive Insignificant Activity B.3 AF-314 Utilities-1000 gallon Polymer Additive Insignificant Activity B.3 AF-315 Utilities-1000 gallon Polymer Additive Insignificant Activity B.3 AF-316 Utilities-1000 gallon Polymer Additive Insignificant Activity B.3 AF-317 Utilities-1000 gallon Polymer Additive Insignificant Activity B.3 AF-318 Utilities-1000 gallon Polymer Additive Insignificant Activity B.3 AF-319 Utilities-1000 gallon Cooling Tower Additive Insignificant Activity B.3 AF-320 Utilities-1000 gallon Cooling Tower Additive Insignificant Activity B.3 AF-320 Utilities-1000 gallon Polymer Insignificant Activity B.3 AF-320 Utilities-1000 gallon Polymer Insignificant Activity B.3 AF-320 Utilities-1000 gallon Polymer Insignificant Activity B.3 BD-100 Sol gallon Cooling Tower Insignificant Activity B.3 BD-101 Sol gallon Cooling Tower Insignificant Activity B.3 BD-102 Sol gallon Steam Condensate Chemical Storage Insignificant Activity B.3 BD-910 Sol gallon Steam Condensate Chemical Storage Insignificant Activity B.3 BD-911 Sol gallon Steam Condensate Chemical Storage Insignificant Activity B.3 BD-912 Sol gallon Steam Condensate Chemical Storage Insignificant Activity B.3 BD-913 Insignificant Activity B.3 BD-914 Sol gallon Steam Condensate Chemical Storage Insignificant Activity B.3 BD-915 Cooling Tower Condensate Chemical Storage Insign	AF-1001	Tank	1992	Insignificant Activity B.3
AD-206A Utilities-<2,000 gallon Cooling Tower Additive Tank 2009 Insignificant Activity B.3 AD-206B Utilities-<2,000 gallon Cooling Tower Additive Tank 2009 Insignificant Activity B.3 AF-211 Utilities-6300 gallon Water Coagulant Tk Insignificant Activity B.3 AF-306 Utilities-1000 gallon Boiler Water Additive Tk Insignificant Activity B.3 AF-307 Utilities-1000 gallon Boiler Water Additive Insignificant Activity B.3 AF-308 Utilities-1000 gallon Boiler Water Additive Insignificant Activity B.3 AF-309 Utilities-1000 gallon Boiler Water Additive Insignificant Activity B.3 AF-313 Utilities-<1000 gallon Polymer Additive Insignificant Activity B.3 DF-901 Utilities-1000 gallon Polymer Additive Insignificant Activity B.3 AF-3120 Utilities-1000 gallon Cooling Tower Additive Tank Insignificant Activity B.3 AF-803 #2 VLSD Fuel Oil Day Storage Tank (TK-5) 1977 Emissions total < 5 TPY of VOC Emission total < 5 TPY of HAP Insignificant Activity B.3 AF-803 #2 VLSD Fuel Oil Day Storage Tank (TK-5) 1977 Insignificant Activity A.20 AT-201 #1 Cooling Tower 1977 Insignificant Activity A.20 AT-202 #2 Cooling Tower 1977 Insignificant Activity A.20 BD-100 230 gallon Chiller Expansion Tank 1989 Insignificant Activity B.3 BD-102 50 gallon Injection Tank 1984 Insignificant Activity B.3 BD-910 So0 gallon Steam Condensate Chemical 1996 Insignificant Activity B.3 BD-911 560 gallon Steam Condensate Chemical 1993 Insignificant Activity B.3 BD-912 560 gallon Steam Condensate Chemical 1979 Insignificant Activity B.3 BD-913 100 gallon Chemical Mix (Steam System Tank) 1997 Insignificant Activity B.3 BD-913 2,000 gallon Steam Condensate Chemical 1997 Insignificant Activity B.3 BD-915 2,000 gallon Steam Condensate Chemical 1997 Insignificant Activity B.3 BD-916 Chemical Mix (Steam System Tank) 1997 Insignificant Activity B.3 BD-917 Chemical Mix (Steam System Tank) 1997 Insignificant Activity B.3 BD-918 2,000 gallon Chemical Mix (Steam System Tank) 1997 Insignificant Activity B.3 BD-916 Chemical Mix (Steam System Tank) 1997 I	AF-1000		1992	Insignificant Activity B 3
AD-2068 Utilities-<2,000 gallon Cooling Tower Additive Tank AF-211 Utilities-6300 gallon Water Coagulant Tk AF-306 Utilities-1000 gal Steam Additive Tk AF-307 Utilities-1000 gallon Boiler Water Additive AF-309 Utilities-1000 gallon Boiler Water Additive AF-309 Utilities-1000 gallon Boiler Water Additive AF-300 Utilities-1000 gallon Polymer Additive AF-313 Utilities-1000 gallon Polymer Additive AF-313 Utilities-1000 gallon Polymer Additive AF-314 Insignificant Activity B.3 AF-315 Utilities-1000 gallon Polymer Additive AF-316 Insignificant Activity B.3 AF-317 Insignificant Activity B.3 AF-318 Insignificant Activity B.3 AF-319 Utilities-1000 gallon Polymer Additive AF-310 Insignificant Activity B.3 AF-310 Insignificant Activity A.20 BD-100 Insignificant Activity B.3 BD-101 Insignificant Activity B.3 BD-102 Insignificant Activity B.3 BD-103 Insignificant Activity B.3 BD-104 Insignificant Activity B.3 BD-105 Insignificant Activity B.3 BD-106 Insignificant Activity B.3 BD-107 Insignificant Activity B.3 BD-108 Insignificant Activity B.3 BD-109 Insignificant Activity B.3 BD-109 Insignificant Activity B.3 BD-110 Insignificant Activity B.3 BD-110 Insignificant Activity B.3 BD-111 Insignificant Activity B.3 BD-112 Insignificant Activity B.3 BD-113 Insignificant Activity B.3 BD-114 Insignificant Activity B.3 BD-115 Insignificant Activity B.3 BD-116 Insignificant Activity B.3 BD-117 Insignificant Activity B.3 BD-118 Insignificant Activity B.3 BD-119 Insignificant Activity B.3 BD-110 Insignificant Activity B.3 BD-111 Insignificant Activity B.3 BD-111 Insignificant Activity B.3 BD-112 Insignificant Activity B.3 BD-113 Insignificant Activity B.3 BD-114 Insignificant Activity B.3 BD-115 Insign	711 1000		17,72	marginiteum recevity B.5
AF-2008	AD-206A	Additive Tank	2009	Insignificant Activity B.3
AF-306 Utilities-1000 gallon Boiler Water Additive AF-307 Utilities-1000 gallon Boiler Water Additive AF-309 Utilities-1000 gallon Boiler Water Additive AF-313 Utilities-<1000 gallon Polymer Additive Tank DF-901 Utilities-<1000 gallon Polymer Additive Tank AF-313 Utilities-<1000 gallon Polymer Additive Tank DF-901 Utilities-<1000 gallon Polymer Additive Tank AF-320 Utilities-1000 gallon Cooling Tower Additive Tank AF-803 #2 VLSD Fuel Oil Day Storage Tank (TK-5) AF-803 #2 VLSD Fuel Oil Day Storage Tank (TK-5) AF-803 #2 VLSD Fuel Oil Day Storage Tank (TK-5) BD-100 230 gallon Chiller Expansion Tank BD-102 50 gallon Injection Tank BD-102 50 gallon DHT Waste Condensate BD-910 Storage BD-910 Storage BD-910 Storage BD-911 560 gallon Steam Condensate Chemical Storage BD-912 560 gallon Steam Condensate Chemical Storage BD-913 100 gallon Chemical Mix (Steam System Tank) BD-915 2,000 gallon Liquid Catalyst Tank BF-1402 95,000 gallon Liquid Catalyst Tank BF-1404 6,600 gallon Hydrobromic Acid (HBr) BF-1404 6,600 gallon Hydrobromic Acid (HBr) DI tilities-1000 gallon Injection Tank Insignificant Activity B.3 Insignif	AD-206B		2009	Insignificant Activity B.3
AF-307 Utilities-1000 gallon Boiler Water Additive AF-309 Utilities-1000 gallon Boiler Water Additive AF-313 Utilities-(1000 gallon Polymer Additive Tank DF-901 Utilities-(1000 gallon Polymer Additive Tank DF-901 Utilities-(1000 gallon Polymer Additive Tank AF-1320 Utilities-(1000 gallon Polymer Additive Tank AF-1320 Utilities-(1000 gallon Polymer Additive Tank AF-803 #2 VLSD Fuel Oil Day Storage Tank (TK-5) AF-803 #2 VLSD Fuel Oil Day Storage Tank (TK-5) AF-201 #1 Cooling Tower AT-202 #2 Cooling Tower AT-202 #2 Cooling Tower AT-203 BD-100 230 gallon Chiller Expansion Tank BD-102 S0 gallon Injection Tank BD-102 S0 gallon DHT Waste Condensate BD-910 \$500 gallon DHT Waste Condensate BD-910 \$500 gallon Steam Condensate Chemical Storage BD-911 \$600 gallon Steam Condensate Chemical Storage BD-912 \$1000 gallon Steam Condensate Chemical Storage BD-913 \$1000 gallon Steam Condensate Chemical Storage BD-914 \$2,0000 gallon Steam Condensate Chemical Storage BD-915 \$2,0000 gallon Steam Condensate Chemical Storage BD-916 \$2,0000 gallon Steam Condensate Chemical Storage BD-917 \$2,0000 gallon Steam Condensate Chemical Storage BD-918 \$2,0000 gallon Steam Condensate Chemical Storage BD-919 \$2,0000 gallon Steam Condensate Chemical Storage BD-910 \$2,0000 gallon Steam Condensate Chemical Storage BD-911 \$2,0000 gallon Steam Condensate Chemical Storage BD-912 \$2,0000 gallon Steam Condensate Chemical Storage BD-913 \$1000 gallon Steam Condensate Chemical Storage BD-914 \$2,0000 gallon Steam Condensate Chemical Storage BD-915 \$2,0000 gallon Steam Condensate Chemical Storage BD-916 \$2,0000 gallon Steam Condensate Chemical Storage BD-917 \$2,0000 gallon Steam Condensate Chemical Storage BD-918 \$2,0000 gallon Steam Condensate Chemical Storage BD-919 \$2,0000 gallon Steam Condensate Chemical Storage BD-910 \$2,0000 g	AF-211	Utilities-6300 gallon Water Coagulant Tk		Insignificant Activity B.3
AF-309 Utilities-1000 gallon Boiler Water Additive AF-313 Utilities-<1000 gallon Polymer Additive Tank DF-901 Utilities-<1000 gallon Polymer Additive Tank AF-1320 Utilities-1000 gallon Cooling Tower Additive Tank AF-803 #2 VLSD Fuel Oil Day Storage Tank (TK-5) AT-201 #1 Cooling Tower AT-202 #2 Cooling Tower BD-100 230 gallon Chiller Expansion Tank BD-125 1500 gallon DHT Waste Condensate BD-910 Storage BD-910 Storage BD-911 560 gallon Steam Condensate Chemical BD-912 Storage BD-913 100 gallon Chemical Mix (Steam System Tank) BD-915 2,000 gallon Liquid Catalyst Tank BF-1402 95,000 gallon Liquid Catalyst Tank BF-1404 6,600 gallon Hydrobromic Acid (HBr) DISSIPPTICAL TACTIVITY B.3 Insignificant Activity B.3 Insi	AF-306	Utilities-1000 gal Steam Additive Tk		Insignificant Activity B.3
DF-901 Utilities-<1000 gallon Polymer Additive Tank 1998 Insignificant Activity B.3	AF-307	Utilities-1000 gallon Boiler Water Additive		Insignificant Activity B.3
DF-901 Utilities-<1000 gallon Polymer Additive Tank AF-1320 Utilities-1000 gallon Cooling Tower Additive Tank AF-803 #2 VLSD Fuel Oil Day Storage Tank (TK-5) AT-201 #1 Cooling Tower AT-202 #2 Cooling Tower AD-100 230 gallon Chemical Mix (Steam System BD-910 560 gallon Steam Condensate Chemical Storage BD-913 100 gallon Chemical Mix (Steam System Tank) BD-915 2,000 gallon Liquid Catalyst Tank DI Utilities-<1000 gallon Polymer Additive Tank 1998 Insignificant Activity B.3	AF-309	Utilities-1000 gallon Boiler Water Additive		Insignificant Activity B.3
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BM-1201 Shouldn't be listed in Title V permit	BF-1404	6,600 gallon Hydrobromic Acid (HBr)	2004	
	BM-1201			* *

Equip ID	Source Description	Installation Date/ Modification Date	Basis	
SO-100			since on IA list Section A #18	
BF-713	1050 gallon Lube Oil Reservoir Tank (LPVGT)	1995	Insignificant Activity B.3	
CD-501	32,100 gallon Recycle Solvent Drum (Process Water)	1979	Emissions total < 5 TPY of VOC Emission total < .5 TPY of HAP	
CF-401A			Shouldn't be listed in Title V permit	
CF-401B			since on IA list Section A #18	
CF=401C			since on 1A list Section A #18	
DF-901	100 gallon Polymer Additive Tk	2008	Insignificant Activity B.3	
DF-902	400 gallon Steam Condensate Chemical	2008	Insignificant Activity B.3	
DD-913	100 gallon Chemical Mix (Steam System Tank)	1996	Insignificant Activity B.3	
AM-840	PX Pump Emergency Generator (230 KW)	07/2006	Insignificant Activity B.2.b	
AM-846	Main Gate Emergency Generator (50 KW)	5/2005	Insignificant Activity B.2.a	
AM-847	Contractor Gate Emergency Generator (20 KW)	5/2005	Insignificant Activity B.2.a	
AM-848	T-Head Emergency Generator (50 KW)	5/2205	Insignificant Activity B.2.a	
AM-849	WWT Control Room Emergency Generator (60 KW)	12/2007	Insignificant Activity B.2.a	
AM-819	Administration Building Emergency Generator (50 KW)	04/2005	Insignificant Activity B.2.a	

N/A = Not Applicable

Appendix F Federal Land Manager Reply

Doerner, Michael

From: Collins, Catherine <catherine_collins@fws.gov>

Sent: Tuesday, March 12, 2013 2:44 PM

To: Doerner, Michael

Subject: Re: FW: BP Cooper River PSD Permit Application

Thank you for sending the information regarding the project near the Cape Romain National Wildlife Refuge. Based on the emission changes identified in the document and distance from the Class I area(s) listed below, the Fish and Wildlife Service anticipates that modeling would not show any significant additional impacts to air quality related values (AQRV) at the Class I area(s) administered by the FWS. Therefore, we are not requesting that a Class I AQRV analysis be included in the PSD permit application. Our screening of this analysis does not indicate agreement with any AQRV analysis protocols or conclusions applicants may make independent of Federal Land Manager review. Please note that we are specifically addressing the need for an AQRV analysis for Class I areas managed by the Fish and Wildlife Service.

Class I Area:

Cape Romain NWR

Distance to Facility in kilometers

21.6 km

Annual Emissions (based on short term maximum emission rates adjusted to an annual emission rate) in tons per year (tpy)

- + 27.4 Nitrogen Oxides
- + 0.3 Sulfur Oxides
- + 4.7 Total Fine particulate matter
- + 72.6 Volatile organic compounds
- + 439.6 Carbon Monoxide

The state and/or EPA may have a different opinion regarding the need for a Class I increment analysis. Should the emissions or the nature of the project change significantly, please contact me, so that we might re-evaluate the revised proposed project.

Thank you for keeping us informed and involving the Fish and Wildlife Service in the project review.

Catherine Collins, Environmental Engineer U.S. Fish and Wildlife Service Air Quality Branch 7333 W. Jefferson Ave., Suite 375 Lakewood, CO 80235-2034

Appendix G Air Modeling Information

The air modeling information is provided in the attached compact disc.		

Appendix H USEPA Control Technology Fact Sheet – Incinerators



Air Pollution Control Technology Fact Sheet

See Bottom of page 3

Name of Technology: Thermal Incinerator

This type of incinerator is also referred to as a direct flame incinerator, thermal oxidizer, or afterburner. However, the term afterburner is generally appropriate only to describe a thermal oxidizer used to control gases coming from a process where combustion is incomplete.

Type of Technology: Destruction by thermal oxidation

Applicable Pollutants: Primarily volatile organic compounds (VOC). Some particulate matter (PM), commonly composed as soot (particles formed as a result of incomplete combustion of hydrocarbons (HC), coke, or carbon residue) will also be destroyed in various degrees.

Achievable Emission Limits/Reductions:

VOC destruction efficiency depends upon design criteria (i.e., chamber temperature, residence time, inlet VOC concentration, compound type, and degree of mixing) (EPA, 1992). Typical thermal incinerator design efficiencies range from 98 to 99.99% and above, depending on system requirements and characteristics of the contaminated stream (EPA, 1992; EPA, 1996a). The typical design conditions needed to meet 98% or greater control or a 20 parts per million by volume (ppmv) compound exit concentration are: 870°C (1600°F) combustion temperature, 0.75 second residence time, and proper mixing. For halogenated VOC streams, 1100°C (2000°F) combustion temperature, 1.0 second residence time, and use of an acid gas scrubber on the outlet is recommended (EPA, 1992).

For vent streams with VOC concentration below approximately 2000 ppmv, reaction rates decrease, maximum VOC destruction efficiency decreases, and an incinerator outlet VOC concentration of 20 ppmv, or lower may be achieved (EPA, 1992).

Controlled emissions and/or efficiency test data for PM in incinerators are not generally available in the literature. Emission factors for PM in phthalic anhydride processes with incinerators are available, however. The PM control efficiencies for these processes were found to vary from 79 to 96% (EPA, 1998). In EPA's 1990 National Inventory, incinerators used as control devices for PM were reported as achieving 25 to 99% control efficiency of particulate matter 10 microns or less in aerodynamic diameter (PM₁₀) at point source facilities (EPA, 1998). Table 1 presents a breakdown of the PM₁₀ control efficiency ranges by industry for recuperative incinerators (EPA, 1996b). The VOC control efficiency reported for these devices ranged from 0 to 99.9%. These ranges of control efficiencies are large because they include facilities that do not have VOC emissions and control only PM, as well as facilities which have low PM emissions and are primarily concerned with controlling VOC (EPA, 1998).

Table 1. Thermal Incinerator PM_{10} Destruction Efficiencies by Industry (EPA, 1996b)

	PM ₁₀ Control
Industry/Types of Sources	Efficiency (%)
Petroleum and Coal Products	25 - 99.9
asphalt roofing processes (blowing, felt saturation); mineral	
calcining; petroleum refinery processes (asphalt blowing,	
catalytic cracking, coke calcining, sludge converter); sulfur	
manufacturing	
Chemical and Allied Products	50 - 99.9
carbon black manufacturing (mfg); charcoal mfg; liquid waste	
disposal; miscellaneous chemical mfg processes; pesticide mfg;	
phthalic anhydride mfg (xylene oxidation); plastics/synthetic	
organic fiber mfg; solid waste incineration (industrial)	
Primary Metals Industries	70 - 99.9
by-product coke processes (coal unloading, oven charging and	
pushing, quenching); gray iron cupola and other miscellaneous	
processes; secondary aluminum processes (burning/drying,	
smelting furnace); secondary copper processes (scrap drying,	
scrap cupola, and miscellaneous processes); steel foundry	
miscellaneous processes; surface coating oven	
Electronic and Other Electric Equipment	70 - 99.9
chemical mfg miscellaneous processes; electrical equipment	
bake furnace; fixed roof tank; mineral production miscellaneous	
processes; secondary aluminum roll/draw extruding; solid waste	
incineration (industrial)	
Electric, Gas, and Sanitary Services	90 - 98
internal combustion engines; solid waste incineration (industrial,	
commercial/ institutional)	
Stone, Clay, and Glass Products	50 - 95
barium processing kiln; coal cleaning thermal dryer; fabricated	
plastics machinery; wool fiberglass mfg	
Food and Kindred Products	70 - 98
charcoal processing, miscellaneous;	
corn processing, miscellaneous,	
fugitive processing, miscellaneous;	
soybean processing, miscellaneous	
Mining	70 - 99.6
asphalt concrete rotary dryer; organic chemical air oxidation	
units, sulfur production	
National Security and International Affairs	70
solid waste incineration (commercial/institutional and	
municipal)	
Textile Mill Products	88 - 95
plastics/synthetic organic fiber (miscellaneous processes)	
Industrial Machinery and Equipment	88 -98
secondary aluminum processes (burning/drying, smelt furnace)	
Lumber and Wood Products	70
solid waste incineration (industrial)	
Transportation Equipment	70 - 95
solid waste incineration (industrial)	, , , , , ,
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Applicable Source Type: Point

Typical Industrial Applications:

Thermal incinerators can be used to reduce emissions from almost all VOC sources, including reactor vents, distillation vents, solvent operations, and operations performed in ovens, dryers, and kilns. They can handle minor fluctuations in flow, however, excess fluctuations require the use of a flare (EPA, 1992). Their fuel consumption is high, so thermal units are best suited for smaller process applications with moderate-to-high VOC loadings.

Incinerators are used to control VOC from a wide variety of industrial processes, including, but not limited to the following (EPA, 1992):

- Storing and loading/unloading of petroleum products and other volatile organic liquids;
- Vessel cleaning (rail tank cars and tank trucks, barges);
- Process vents in the synthetic organic chemical manufacturing industry (SOCMI);
- Paint manufacturing;
- Rubber products and polymer manufacturing;
- Plywood manufacturing;
- Surface coating operations:

Appliances, magnetic wire, automobiles, cans, metal coils, paper, film and foil, pressure sensitive tapes and labels, magnetic tape, fabric coating and printing, metal furniture, wood furniture, flatwood paneling, aircraft, miscellaneous metal products;

- Flexible vinyl and urethane coating;
- · Graphic arts industry; and
- Hazardous waste treatment storage, and disposal facilities (TSDFs).

Emission Stream Characteristics:

- a. Air Flow: Typical gas flow rates for thermal incinerators are 0.24 to 24 standard cubic meters per second (sm³/sec) (500 to 50,000 standard cubic feet per minute (scfm)) (EPA, 1996a).
- b. Temperature: Most incinerators operate at higher temperatures than the ignition temperature, which is a minimum temperature. Thermal destruction of most organic compounds occurs between 590°C and 650°C (1100°F and 1200°F). Most hazardous waste incinerators are operated at 980°C to 1200°C (1800°F to 2200°F) to ensure nearly complete destruction of the organics in the waste (AWMA, 1992).
- a. Pollutant Loading: Thermal incinerators can be used over a fairly wide range of organic vapor concentrations. For safety considerations, the concentration of the organics in the waste gas must be substantially below the lower flammable level (lower explosive limit, or LEL) of the specific compound being controlled. As a rule, a safety factor of four (i.e., 25% of the LEL) is used (EPA, 1991, AWMA, 1992). The waste gas may be diluted with ambient air, if necessary, to lower the concentration. Considering economic factors, thermal incinerators perform best at inlet concentrations of around 1500 to 3000 ppmv, because the heat of combustion of hydrocarbon gases is sufficient to sustain the high temperatures required without addition of expensive auxiliary fuel (EPA, 1995).
- d. Other Considerations: Incinerators are not generally recommended for controlling gases containing halogen- or sulfur-containing compounds, because of the formation of hydrogen chloride, hydrogen fluoride gas, sulfur dioxide, and other highly corrosive acid gases. It may be necessary to install a post-oxidation acid gas treatment system in such cases, depending on the outlet concentration. This would likely make incineration an uneconomical option. (EPA, 1996a). Thermal

incinerators are also not generally cost-effective for low-concentration, high-flow organic vapor streams (EPA, 1995).

Emission Stream Pretreatment Requirements:

Typically, no pretreatment is required, however, in some cases, a concentrator (e.g., carbon or zeolite adsorption) may be used to reduce the total gas volume to be treated by the more expensive incinerator.

Cost Information:

The following are cost ranges (expressed in 2002 dollars) for packaged thermal incinerators of conventional design under typical operating conditions, developed using EPA cost-estimating spreadsheets (EPA, 1996a) and referenced to the volumetric flow rate of the waste stream treated. The costs do not include costs for a post-oxidation acid gas treatment system. Costs can be substantially higher than in the ranges shown when used for low to moderate VOC concentration streams (less than around 1000 to 1500 ppmv). As a rule, smaller units controlling a low concentration waste stream will be much more expensive (per unit volumetric flow rate) than a large unit cleaning a high pollutant load flow. Operating and Maintenance (O & M) Costs, Annualized Cost, and Cost Effectiveness are dominated by the cost of supplemental fuel required.

- a. Capital Cost: \$53,000 to \$190,000 per sm³/sec (\$25 to \$90 per scfm)
- b. O & M Cost: \$11,000 to \$160,000 per sm³/sec (\$5 to \$75 per scfm), annually
- c. Annualized Cost: \$17,000 to \$208,000 per sm³/sec (\$8 to \$98 per scfm), annually
- d. Cost Effectiveness: \$440 to \$3,600 per metric ton (\$400 to \$3,300 per short ton), annualized cost per ton per year of pollutant controlled

Theory of Operation:

Incineration, or thermal oxidation is the process of oxidizing combustible materials by raising the temperature of the material above its auto-ignition point in the presence of oxygen, and maintaining it at high temperature for sufficient time to complete combustion to carbon dioxide and water. Time, temperature, turbulence (for mixing), and the availability of oxygen all affect the rate and efficiency of the combustion process. These factors provide the basic design parameters for VOC oxidation systems (ICAC, 1999).

A straight thermal incinerator is comprised of a combustion chamber and does not include any heat recovery of exhaust air by a heat exchanger (this type of incinerator is referred to as a recuperative incinerator).

The heart of the thermal incinerator is a nozzle-stabilized flame maintained by a combination of auxiliary fuel, waste gas compounds, and supplemental air added when necessary. Upon passing through the flame, the waste gas is heated from its preheated inlet temperature to its ignition temperature. The ignition temperature varies for different compounds and is usually determined empirically. It is the temperature at which the combustion reaction rate exceeds the rate of heat losses, thereby raising the temperature of the gases to some higher value. Thus, any organic/air mixture will ignite if its temperature is raised to a sufficiently high level (EPA, 1996a).

The required level of VOC control of the waste gas that must be achieved within the time that it spends in the thermal combustion chamber dictates the reactor temperature. The shorter the residence time, the higher the reactor temperature must be. The nominal residence time of the reacting waste gas in the combustion chamber is defined as the combustion chamber volume divided by the volumetric flow rate of the gas. Most thermal units are designed to provide no more than 1 second of residence time to the waste gas with typical temperatures of 650 to 1100°C (1200 to 2000°F). Once the unit is designed and built, the residence time is

not easily changed, so that the required reaction temperature becomes a function of the particular gaseous species and the desired level of control (EPA, 1996a).

Studies based on actual field test data, show that commercial incinerators should generally be run at 870°C (1600°F) with a nominal residence time of 0.75 seconds to ensure 98% destruction of non-halogenated organics (EPA, 1992).

Advantages:

Incinerators are one of the most positive and proven methods for destroying VOC, with efficiencies up to 99.9999% possible. Thermal incinerators are often the best choice when high efficiencies are needed and the waste gas is above 20% of the LEL.

Disadvantages:

Thermal incinerator operating costs are relatively high due to supplemental fuel costs.

Thermal incinerators are not well suited to streams with highly variable flow because of the reduced residence time and poor mixing during increased flow conditions which decreases the completeness of combustion. This causes the combustion chamber temperature to fall, thus decreasing the destruction efficiency (EPA, 1991).

Incinerators, in general, are not recommended for controlling gases containing halogen- or sulfur-containing compounds because of the formation of highly corrosive acid gases. It may be necessary to install a post-oxidation acid gas treatment system in such cases, depending on the outlet concentration (EPA, 1996a). Thermal incinerators are also not generally cost-effective for low-concentration, high-flow organic vapor streams (EPA, 1995).

Other Considerations:

Thermal incinerators are not usually as economical, on an annualized basis, as recuperative or regenerative incinerators because they do not recover waste heat energy from the exhaust gases. This heat can be used to preheat incoming air, thus reducing the amount of supplemental fuel required. If there is additional heat energy available, it can be used for other process heating needs.

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